

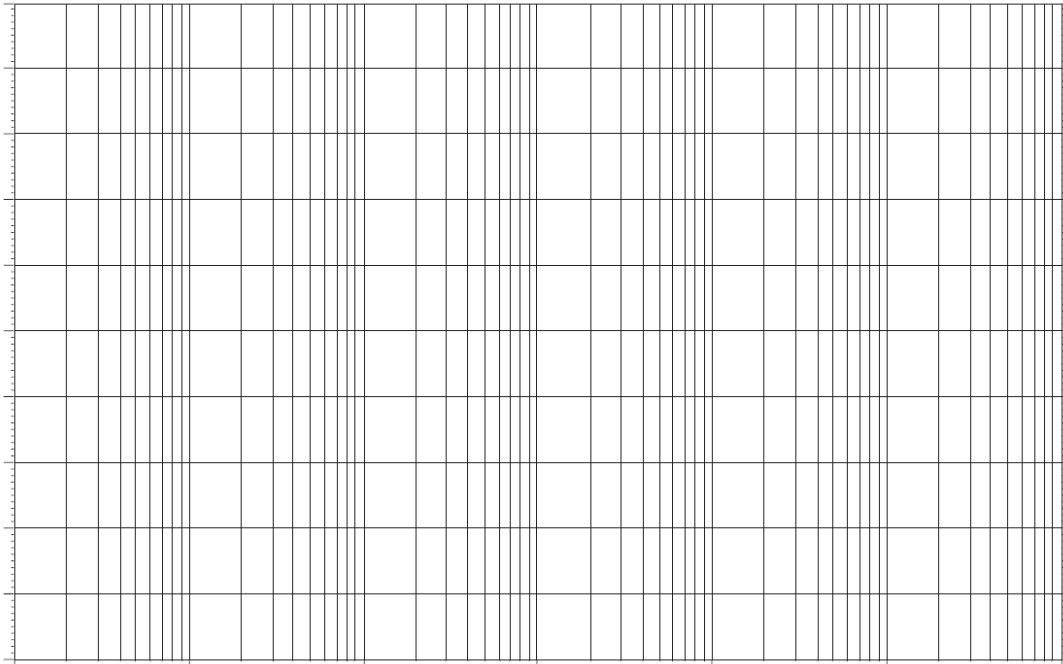
# Plotting a Single Pole Response



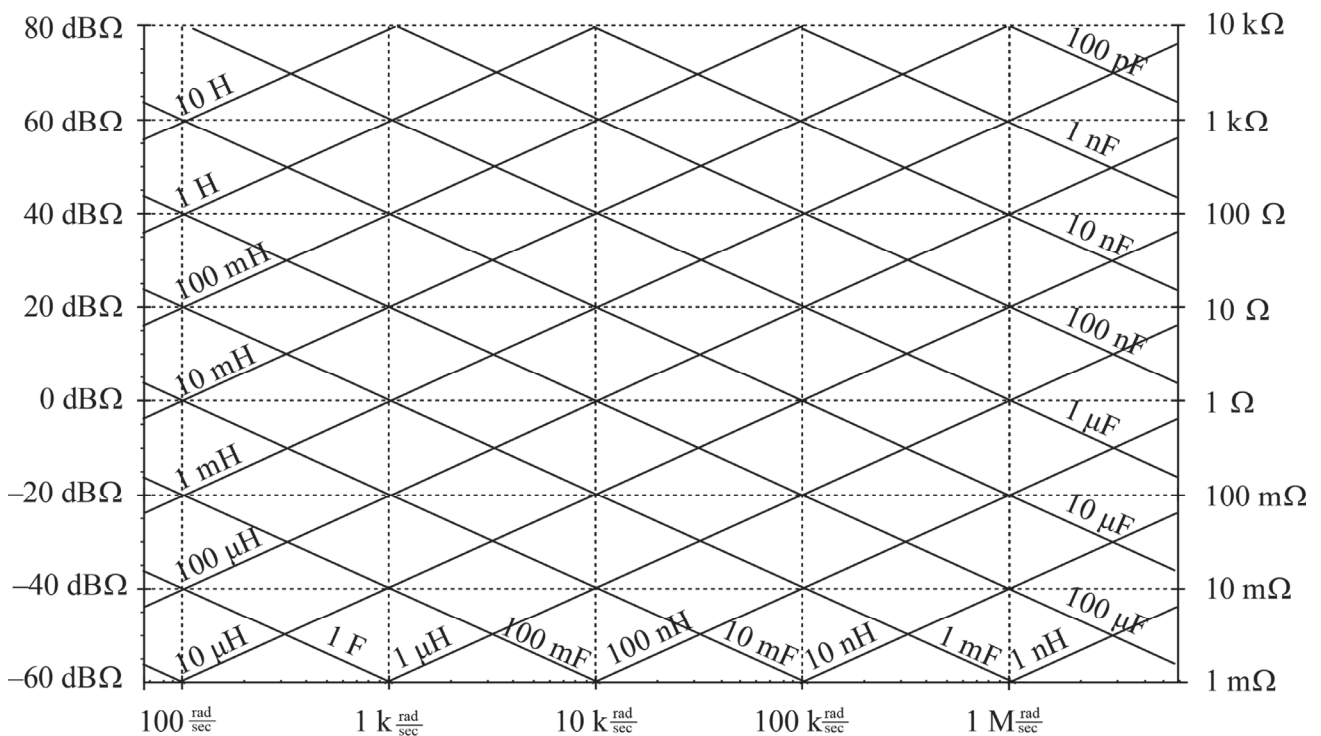
$R = 10\text{k}\Omega$   
 $C = 10\text{nF}$

## Graphical Construction of Bode Plots

# Log Paper



# Reactance Paper



## 8.1.6 Resonant Poles

Example

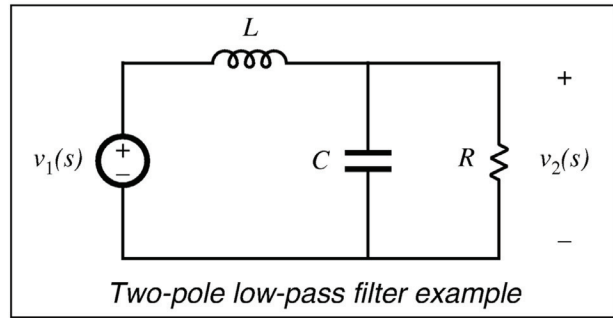
$$G(s) = \frac{v_2(s)}{v_1(s)} = \frac{1}{1 + s\frac{L}{R} + s^2LC}$$

Second-order denominator, of the form

$$G(s) = \frac{1}{1 + a_1s + a_2s^2}$$

with  $a_1 = L/R$  and  $a_2 = LC$

How should we construct the Bode diagram?



## Standard Form for Complex Poles

$$G(s) = \frac{1}{1 + 2\zeta \frac{s}{\omega_0} + \left(\frac{s}{\omega_0}\right)^2} \quad \text{or} \quad G(s) = \frac{1}{1 + \frac{s}{Q\omega_0} + \left(\frac{s}{\omega_0}\right)^2}$$

- When the coefficients of  $s$  are real and positive, then the parameters  $\zeta$ ,  $\omega_0$ , and  $Q$  are also real and positive
- The parameters  $\zeta$ ,  $\omega_0$ , and  $Q$  are found by equating the coefficients of  $s$
- The parameter  $\omega_0$  is the angular corner frequency, and we can define  $f_0 = \omega_0/2\pi$
- The parameter  $\zeta$  is called the *damping factor*.  $\zeta$  controls the shape of the exact curve in the vicinity of  $f = f_0$ . The roots are complex when  $\zeta < 1$ .
- In the alternative form, the parameter  $Q$  is called the *quality factor*.  $Q$  also controls the shape of the exact curve in the vicinity of  $f = f_0$ . The roots are complex when  $Q > 0.5$ .

# The Q Factor

In a second-order system,  $\zeta$  and  $Q$  are related according to

$$Q = \frac{1}{2\zeta}$$

$Q$  is a measure of the dissipation in the system. A more general definition of  $Q$ , for sinusoidal excitation of a passive element or system is

$$Q = 2\pi \frac{\text{(peak stored energy)}}{\text{(energy dissipated per cycle)}}$$

For a second-order passive system, the two equations above are equivalent. We will see that  $Q$  has a simple interpretation in the Bode diagrams of second-order transfer functions.

## Magnitude Asymptotes

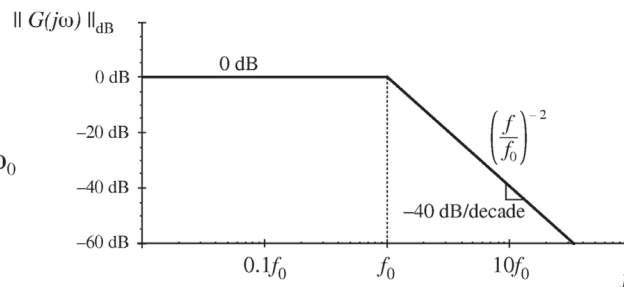
In the form 
$$G(s) = \frac{1}{1 + \frac{s}{Q\omega_0} + \left(\frac{s}{\omega_0}\right)^2}$$

let  $s = j\omega$  and find magnitude: 
$$\|G(j\omega)\| = \frac{1}{\sqrt{\left(1 - \left(\frac{\omega}{\omega_0}\right)^2\right)^2 + \frac{1}{Q^2} \left(\frac{\omega}{\omega_0}\right)^2}}$$

Asymptotes are

$$\|G\| \rightarrow 1 \quad \text{for } \omega \ll \omega_0$$

$$\|G\| \rightarrow \left(\frac{f}{f_0}\right)^{-2} \quad \text{for } \omega \gg \omega_0$$



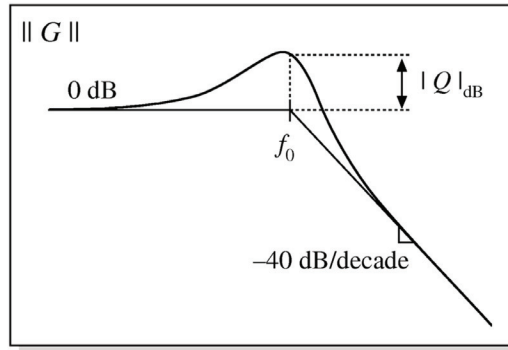
# Exact Magnitude Curve

$$\|G(j\omega)\| = \frac{1}{\sqrt{\left(1 - \left(\frac{\omega}{\omega_0}\right)^2\right)^2 + \frac{1}{Q^2} \left(\frac{\omega}{\omega_0}\right)^2}}$$

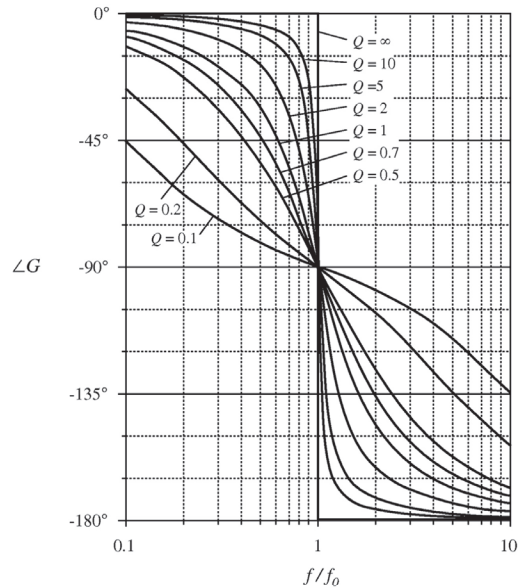
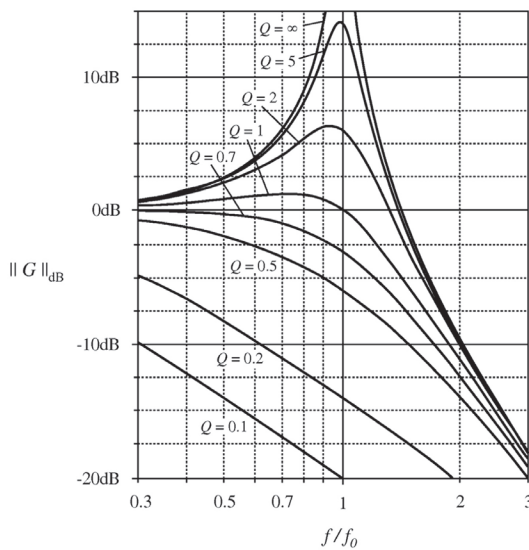
At  $\omega = \omega_0$ , the exact magnitude is

$$\|G(j\omega_0)\| = Q \quad \text{or, in dB:} \quad \|G(j\omega_0)\|_{\text{dB}} = |Q|_{\text{dB}}$$

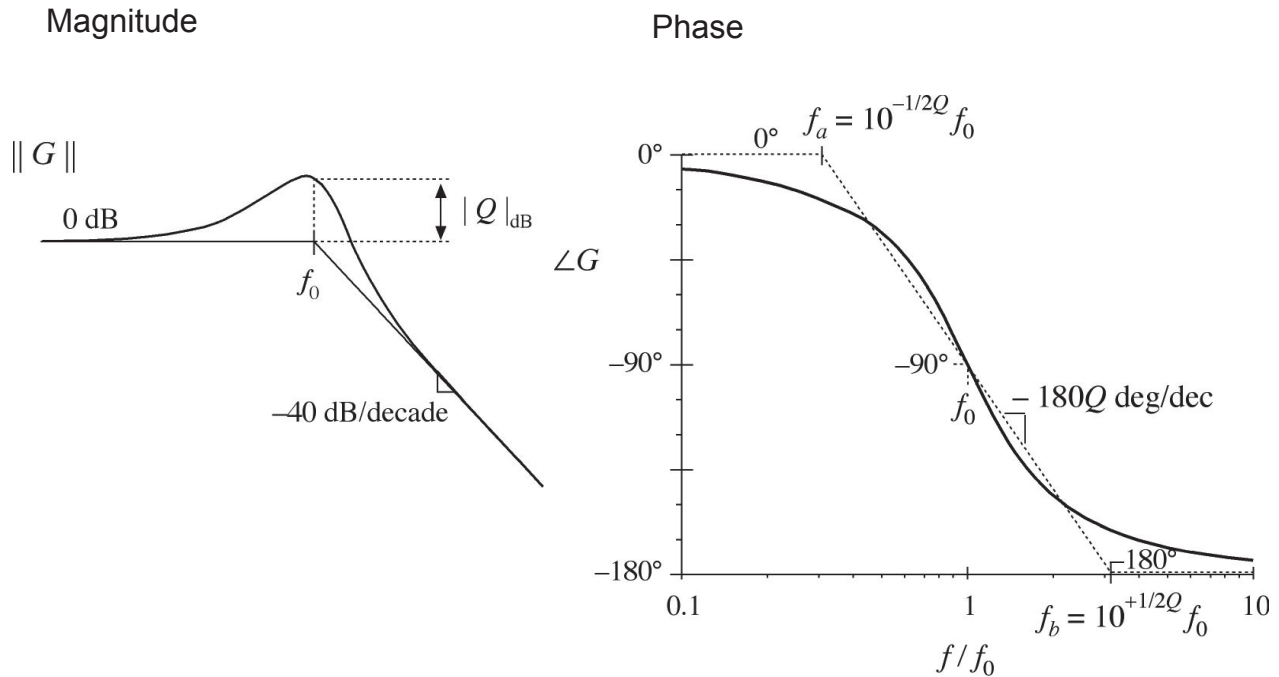
The exact curve has magnitude  $Q$  at  $f = f_0$ . The deviation of the exact curve from the asymptotes is  $|Q|_{\text{dB}}$



# Curves for Varying Q



# Asymptotes for Complex Poles, $Q > 0.5$



## The Low Q Approximation

Given a second-order denominator polynomial, of the form

$$G(s) = \frac{1}{1 + a_1 s + a_2 s^2} \quad \text{or} \quad G(s) = \frac{1}{1 + \frac{s}{Q\omega_0} + \left(\frac{s}{\omega_0}\right)^2}$$

When the roots are real, i.e., when  $Q < 0.5$ , then we can factor the denominator, and construct the Bode diagram using the asymptotes for real poles. We would then use the following normalized form:

$$G(s) = \frac{1}{\left(1 + \frac{s}{\omega_1}\right)\left(1 + \frac{s}{\omega_2}\right)}$$

This is a particularly desirable approach when  $Q \ll 0.5$ , i.e., when the corner frequencies  $\omega_1$  and  $\omega_2$  are well separated.

# Derivation of Low-Q Approximation

Given

$$G(s) = \frac{1}{1 + \frac{s}{Q\omega_0} + \left(\frac{s}{\omega_0}\right)^2}$$

Use quadratic formula to express corner frequencies  $\omega_1$  and  $\omega_2$  in terms of  $Q$  and  $\omega_0$  as:

$$\omega_1 = \frac{\omega_0}{Q} \frac{1 - \sqrt{1 - 4Q^2}}{2} \quad \omega_2 = \frac{\omega_0}{Q} \frac{1 + \sqrt{1 - 4Q^2}}{2}$$

## Corner Frequency $\omega_1$

$$\omega_1 = \frac{\omega_0}{Q} \frac{1 - \sqrt{1 - 4Q^2}}{2}$$

can be written in the form

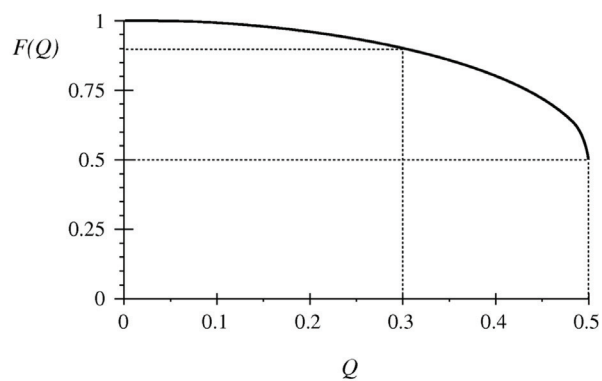
$$\omega_1 = \frac{Q \omega_0}{F(Q)}$$

where

$$F(Q) = \frac{1}{2} \left( 1 + \sqrt{1 - 4Q^2} \right)$$

For small  $Q$ ,  $F(Q)$  tends to 1.  
We then obtain

$$\omega_1 \approx Q \omega_0 \quad \text{for } Q \ll \frac{1}{2}$$



For  $Q < 0.3$ , the approximation  $F(Q) = 1$  is within 10% of the exact value.

# Corner Frequency $\omega_2$

$$\omega_2 = \frac{\omega_0}{Q} \frac{1 + \sqrt{1 - 4Q^2}}{2}$$

can be written in the form

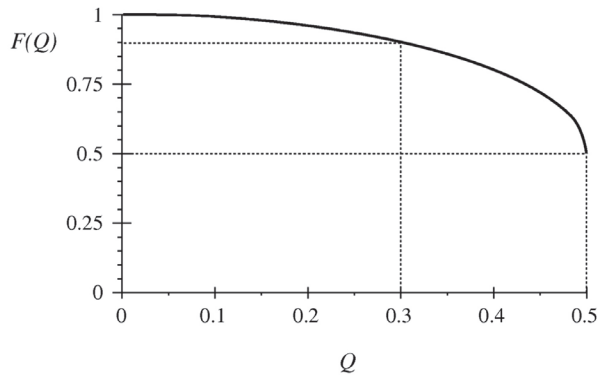
$$\omega_2 = \frac{\omega_0}{Q} F(Q)$$

where

$$F(Q) = \frac{1}{2} (1 + \sqrt{1 - 4Q^2})$$

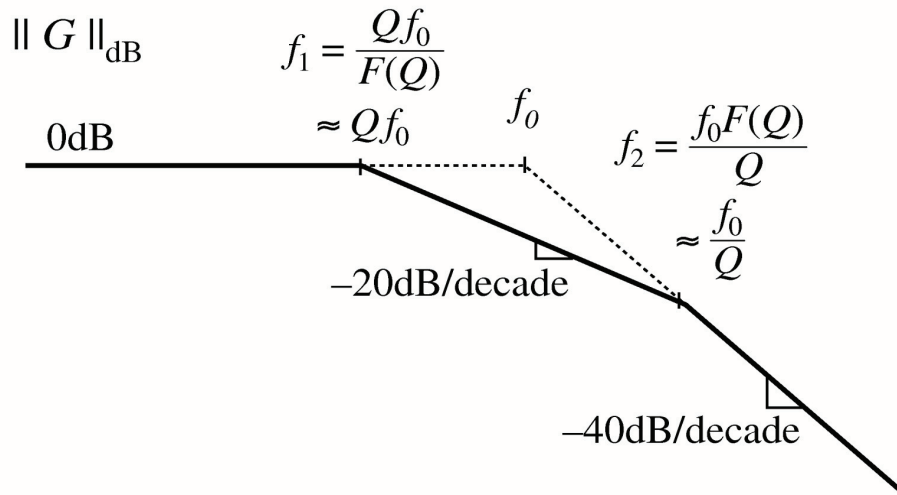
For small  $Q$ ,  $F(Q)$  tends to 1.  
We then obtain

$$\omega_2 \approx \frac{\omega_0}{Q} \quad \text{for } Q \ll \frac{1}{2}$$



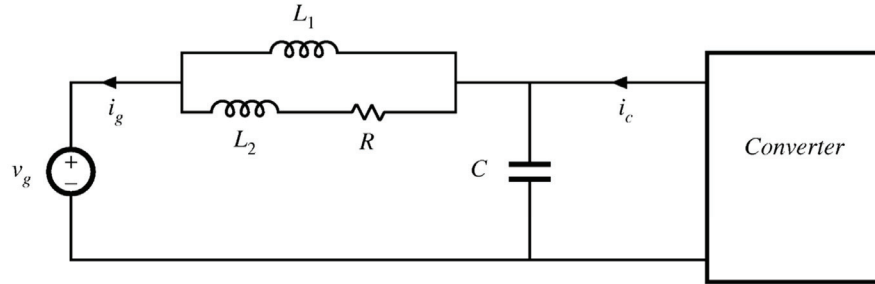
For  $Q < 0.3$ , the approximation  $F(Q) = 1$  is within 10% of the exact value.

## The Low-Q Approximation





# Example: Damped Input EMI Filter



$$G(s) = \frac{i_g(s)}{i_c(s)} = \frac{1 + s \frac{L_1 + L_2}{R}}{1 + s \frac{L_1 + L_2}{R} + s^2 L_1 C + s^3 \frac{L_1 L_2 C}{R}}$$

## 8.1.8: Approximate Roots of a Polynomial

Generalize the low- $Q$  approximation to obtain approximate factorization of the  $n^{\text{th}}$ -order polynomial

$$P(s) = 1 + a_1 s + a_2 s^2 + \dots + a_n s^n$$

It is desired to factor this polynomial in the form

$$P(s) = (1 + \tau_1 s)(1 + \tau_2 s) \dots (1 + \tau_n s)$$

When the roots are real and well separated in value, then approximate analytical expressions for the time constants  $\tau_1, \tau_2, \dots, \tau_n$  can be found, that typically are simple functions of the circuit element values.

**Objective:** find a general method for deriving such expressions. Include the case of complex root pairs.

# Derivation of the Approximation

Multiply out factored form of polynomial, then equate to original form (equate like powers of  $s$ ):

$$\begin{aligned}a_1 &= \tau_1 + \tau_2 + \dots + \tau_n \\a_2 &= \tau_1(\tau_2 + \dots + \tau_n) + \tau_2(\tau_3 + \dots + \tau_n) + \dots \\a_3 &= \tau_1\tau_2(\tau_3 + \dots + \tau_n) + \tau_2\tau_3(\tau_4 + \dots + \tau_n) + \dots \\&\vdots \\a_n &= \tau_1\tau_2\tau_3\cdots\tau_n\end{aligned}$$

- Exact system of equations relating roots to original coefficients
- Exact general solution is hopeless
- Under what conditions can solution for time constants be easily approximated?

## Case When All Roots Separate

*System of equations:*  
(from previous slide)

$$\begin{aligned}a_1 &= \tau_1 + \tau_2 + \dots + \tau_n \\a_2 &= \tau_1(\tau_2 + \dots + \tau_n) + \tau_2(\tau_3 + \dots + \tau_n) + \dots \\a_3 &= \tau_1\tau_2(\tau_3 + \dots + \tau_n) + \tau_2\tau_3(\tau_4 + \dots + \tau_n) + \dots \\&\vdots \\a_n &= \tau_1\tau_2\tau_3\cdots\tau_n\end{aligned}$$

Suppose that roots are real and well-separated, and are arranged in decreasing order of magnitude:

$$|\tau_1| \gg |\tau_2| \gg \dots \gg |\tau_n|$$

Then the first term of each equation is dominant

⇒ Neglect second and following terms in each equation above

# Approximation When Roots are Well Separated

*System of equations:*

(only first term in each equation is included)

$$\begin{aligned}a_1 &\approx \tau_1 \\a_2 &\approx \tau_1 \tau_2 \\a_3 &\approx \tau_1 \tau_2 \tau_3 \\&\vdots \\a_n &= \tau_1 \tau_2 \tau_3 \cdots \tau_n\end{aligned}$$

*Solve for the time constants:*

$$\begin{aligned}\tau_1 &\approx a_1 \\ \tau_2 &\approx \frac{a_2}{a_1} \\ \tau_3 &\approx \frac{a_3}{a_2} \\ &\vdots \\ \tau_n &\approx \frac{a_n}{a_{n-1}}\end{aligned}$$

## Results

If the following inequalities are satisfied

$$\left| a_1 \right| \gg \left| \frac{a_2}{a_1} \right| \gg \left| \frac{a_3}{a_2} \right| \gg \dots \gg \left| \frac{a_n}{a_{n-1}} \right|$$

Then the polynomial  $P(s)$  has the following approximate factorization

$$P(s) \approx \left( 1 + a_1 s \right) \left( 1 + \frac{a_2}{a_1} s \right) \left( 1 + \frac{a_3}{a_2} s \right) \cdots \left( 1 + \frac{a_n}{a_{n-1}} s \right)$$

- If the  $a_n$  coefficients are simple analytical functions of the element values  $L$ ,  $C$ , etc., then the roots are similar simple analytical functions of  $L$ ,  $C$ , etc.
- Numerical values are used to justify the approximation, but analytical expressions for the roots are obtained

# Quadratic Roots: Not Well Separated

Suppose inequality  $k$  is not satisfied:

$$|a_1| \gg \left| \frac{a_2}{a_1} \right| \gg \dots \gg \left| \frac{a_k}{a_{k-1}} \right| \not\gg \left| \frac{a_{k+1}}{a_k} \right| \gg \dots \gg \left| \frac{a_n}{a_{n-1}} \right|$$

↑  
not  
satisfied

Then leave the terms corresponding to roots  $k$  and  $(k + 1)$  in quadratic form, as follows:

$$P(s) \approx \left(1 + a_1 s\right) \left(1 + \frac{a_2}{a_1} s\right) \dots \left(1 + \frac{a_k}{a_{k-1}} s + \frac{a_{k+1}}{a_{k-1}} s^2\right) \dots \left(1 + \frac{a_n}{a_{n-1}} s\right)$$

This approximation is accurate provided

$$|a_1| \gg \left| \frac{a_2}{a_1} \right| \gg \dots \gg \left| \frac{a_k}{a_{k-1}} \right| \gg \left| \frac{a_{k-2} a_{k+1}}{a_{k-1}^2} \right| \gg \left| \frac{a_{k+2}}{a_{k+1}} \right| \gg \dots \gg \left| \frac{a_n}{a_{n-1}} \right|$$

## First Inequality Violated

When inequality 1 is not satisfied:

$$|a_1| \not\gg \left| \frac{a_2}{a_1} \right| \gg \left| \frac{a_3}{a_2} \right| \gg \dots \gg \left| \frac{a_n}{a_{n-1}} \right|$$

↑  
not  
satisfied

Then leave the first two roots in quadratic form, as follows:

$$P(s) \approx \left(1 + a_1 s + a_2 s^2\right) \left(1 + \frac{a_3}{a_2} s\right) \dots \left(1 + \frac{a_n}{a_{n-1}} s\right)$$

This approximation is justified provided

$$\left| \frac{a_2^2}{a_3} \right| \gg |a_1| \gg \left| \frac{a_3}{a_2} \right| \gg \left| \frac{a_4}{a_3} \right| \gg \dots \gg \left| \frac{a_n}{a_{n-1}} \right|$$

# Other Cases

- Several nonadjacent inequalities violated
  - Apply same process multiple times
- Multiple adjacent inequalities violated
  - More than two roots close in value
  - Must use 3<sup>rd</sup> order or higher polynomial