



Converter Loss Analysis

ECE 482 Lecture 4
January 17, 2014



Announcements

- Finish Experiment 1: report due Monday, 1/27
- This week: Experiment 2
 - Boost open-loop construction and modeling
 - Prelab: Inductor design and switch selection
- Component kits available in circuits store
 - \$80 *per group* for components for Labs 2 and 3
 - Plan to spend additional <\$5.00 on resistors

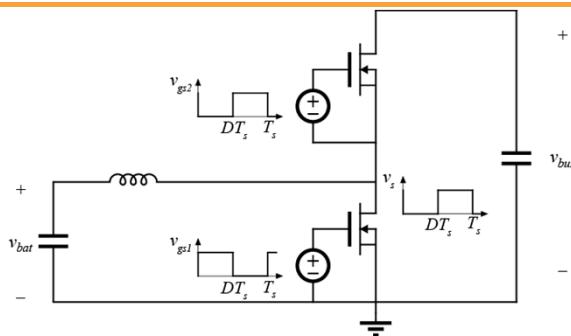


Analytical Loss Modeling

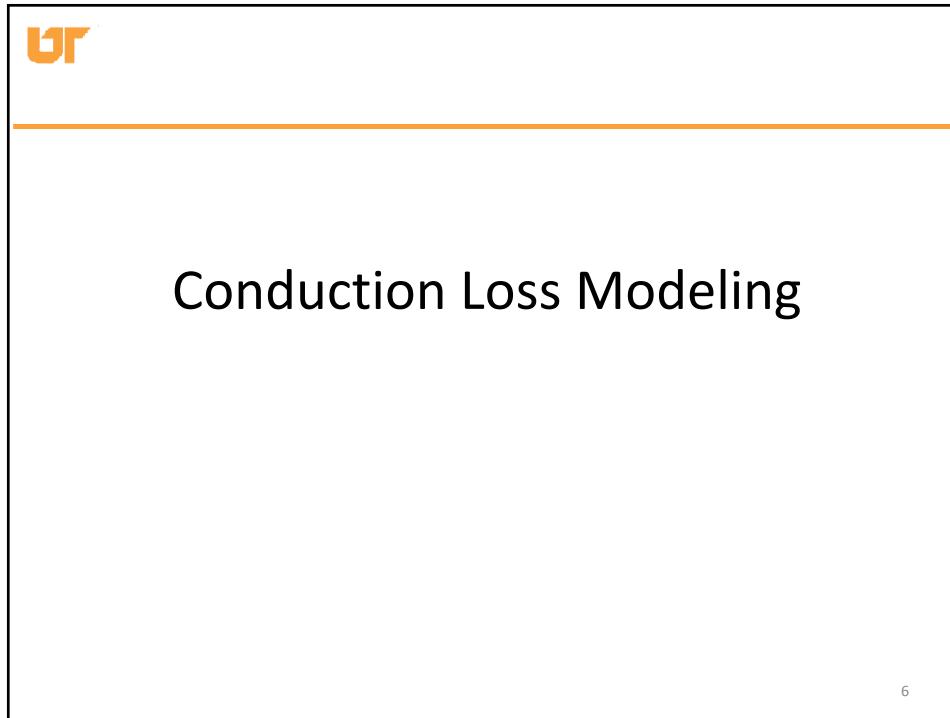
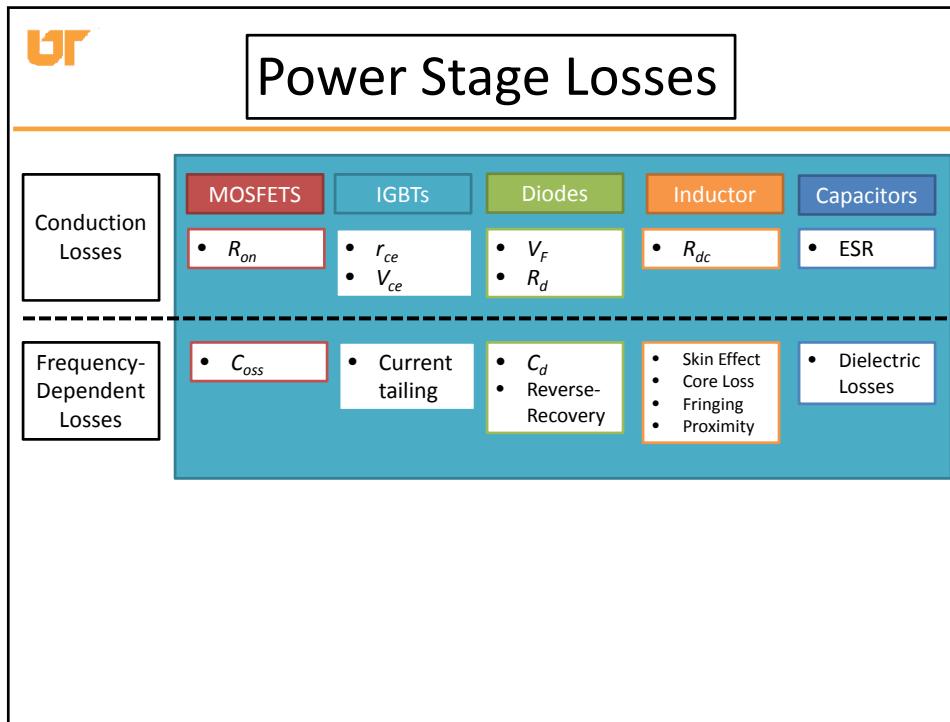
- High efficiency approximation is acceptable for hand calculations, as long as it is justified
 - Solve waveforms of lossless converter, then calculate losses
- Alternate approach: average circuit
 - Uses average, rather than RMS currents
 - Difficult to include losses other than conduction
- Argue which losses need to be included, and which may be neglected



Boost Converter Loss Analysis

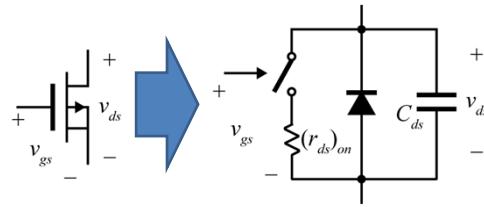


- Begin by solving important waveforms throughout converter assuming lossless operation





MOSFET Equivalent Circuit

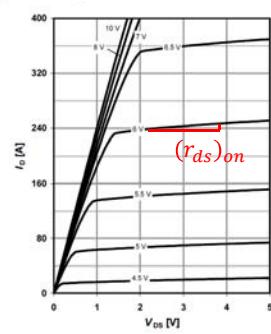


- Considering only power stage losses (gate drive neglected)
- MOSFET operated as power switch
- Intrinsic body diode behaviors considered using normal diode analysis

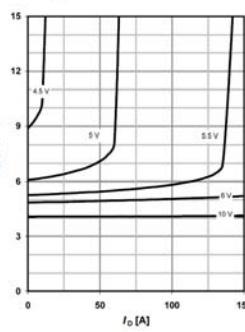


MOSFET On Resistance

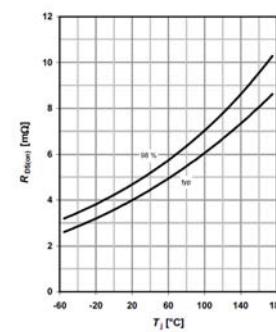
5 Typ. output characteristics
 $I_D=f(V_{DS})$; $T_J=25^\circ\text{C}$
parameter: V_{GS}



6 Typ. drain-source on resistance
 $R_{DS(on)}=f(I_D)$; $T_J=25^\circ\text{C}$
parameter: V_{GS}



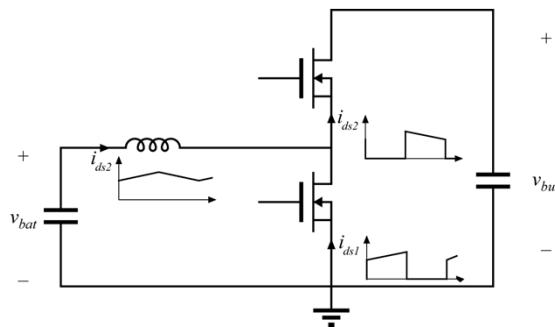
9 Drain-source on-state resistance
 $R_{DS(on)}=f(T_J)$; $I_D=100\text{ A}$; $V_{GS}=10\text{ V}$



- On resistance extracted from datasheet waveforms
- Significantly dependent on V_{GS} amplitude, temperature



Boost Converter RMS Currents



- MOSFET conduction losses due to $(r_{ds})_{on}$ depend given as

$$P_{cond,FET} = I_{d,rms}^2 (r_{ds})_{on}$$



MOSFET Conduction Losses

Pulsating waveform with linear ripple, Fig. A.6:

$$rms = I \sqrt{D} \sqrt{1 + \frac{1}{3} \left(\frac{\Delta i}{I} \right)^2} \quad (A.6)$$

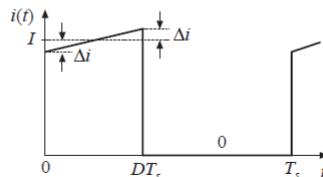
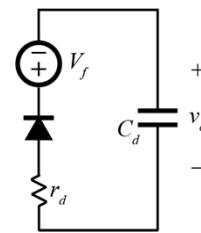


Fig. A.6

- RMS values of commonly observed waveforms appendix from Power Book



Diode Loss Model



- Example loss model includes resistance and forward voltage drop extracted from datasheet

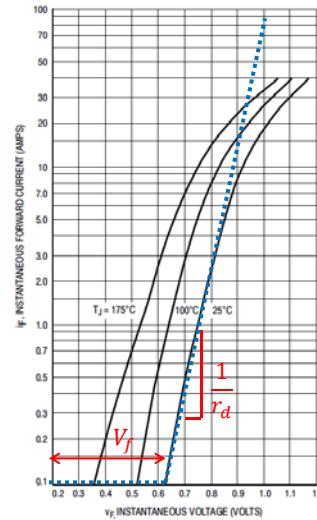
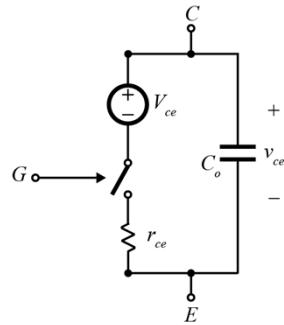


Figure 1. Typical Forward Voltage

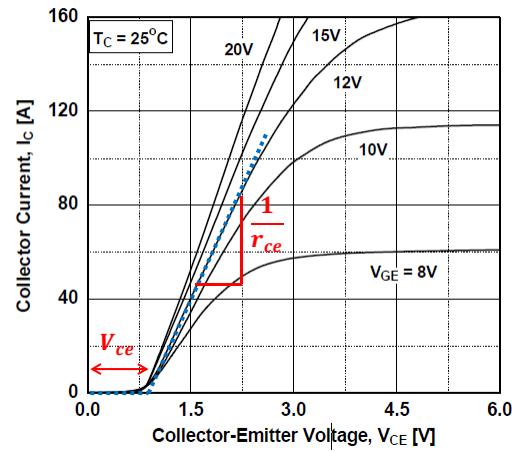


IGBT Loss Model



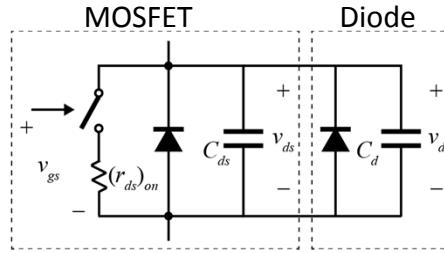
$$P_{cond} = I_{c,rms}^2 r_{ce} + V_{ce} I_{c,avg}$$

Figure 1. Typical Output Characteristics





Semiconductor Switch Conduction Loss



- Equivalent circuit of MOSFET with external antiparallel diode has two, non-ideal diodes
- Diodes, even when matched, will not share current equally, but $v_d = v_{ds}$ must remain true
- Silicon rectifier diodes are minority carrier devices
 - Concentration of minority carriers depends heavily on temperature



Diode Parallelizing

12 Forward characteristics of reverse diode

$$I_F = f(V_{SD})$$

parameter: T_j

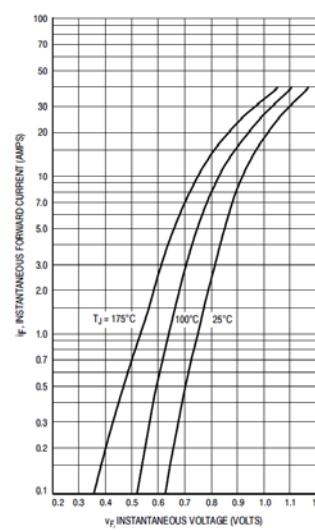
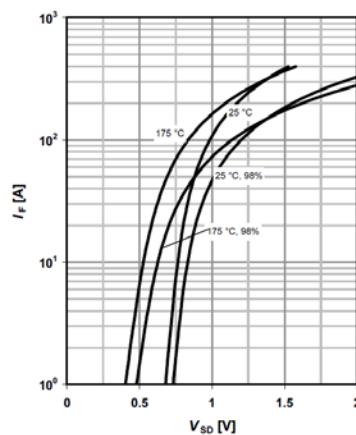
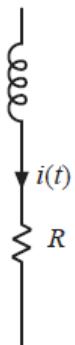


Figure 1. Typical Forward Voltage



DC Inductor Resistance



- DC Resistance given by

$$R_{DC} = \rho \frac{l_b}{A_w}$$

- At room temp, $\rho = 1.724 \cdot 10^{-6} \Omega\text{-cm}$
- At 100°C, $\rho = 2.3 \cdot 10^{-6} \Omega\text{-cm}$
- Losses due to DC current:

$$P_{cu,DC} = I_{L,rms}^2 R_{DC}$$



Inductor Conduction Losses

DC plus linear ripple, Fig. A.2:

$$rms = I \sqrt{1 + \frac{1}{3} \left(\frac{\Delta i}{I} \right)^2} \quad (\text{A.2})$$

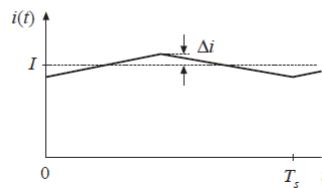
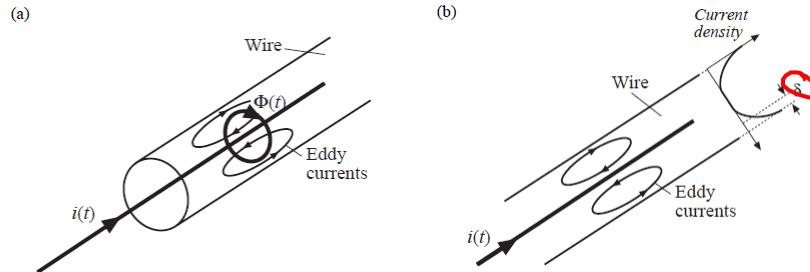


Fig. A.2

- Conduction losses dependent on RMS current through inductor



Skin Effect in Copper Wire



- Current profile at high frequency is exponential function of distance from center with characteristic length δ



Skin Depth

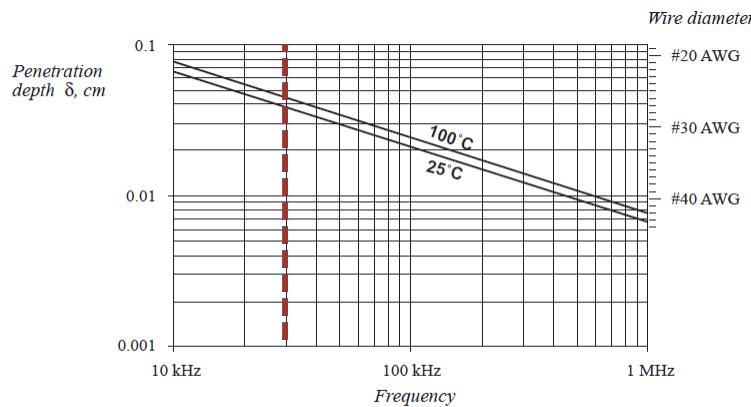
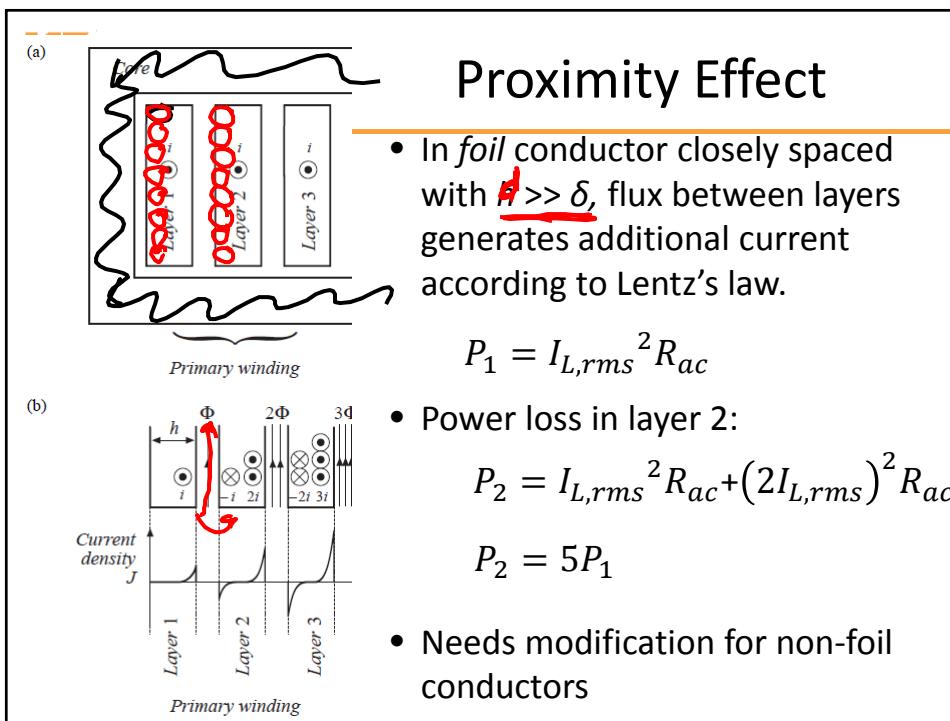
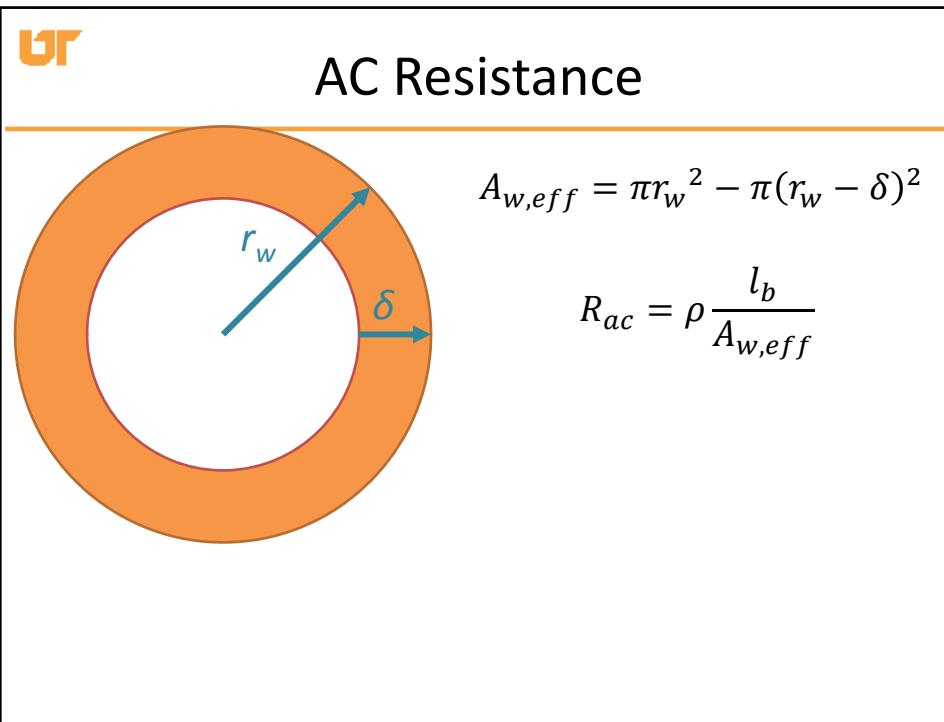
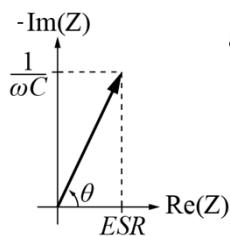
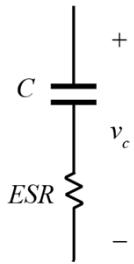


Fig. 13.23 Penetration depth δ , as a function of frequency f , for copper wire.





Capacitor Loss Model



- Operation well below resonance
- All loss mechanisms in a capacitor are generally lumped into an empirical loss model
- Equivalent Series Resistance (ESR) is *highly* frequency dependent
- Datasheets may give effective impedance at a frequency, or loss factor:

$$\delta = \frac{\pi}{2} - \theta$$

$$D = \tan(\delta)$$



Capacitor ESR Extraction



WV (Vdc)	Cap (μ F)	Case size ϕ D×L(mm)	Impedance (Ω max/100kHz)		Rated ripple current (mAmps/ 105°C, 100kHz)	Part No.
			20°C	-10°C		
6.8	5×11	1.4	5.6	125	EKZE101E□□6R8ME11D	
15	6.3×11	0.57	2.3	205	EKZE101E□□150MF11D	
27	8×11.5	0.36	1.4	355	EKZE101E□□270MHBS5D	
39	8×15	0.25	1.0	450	EKZE101E□□390MH15D	
47	10×12.5	0.17	0.66	480	EKZE101E□□470MJC5S	
56	8×20	0.19	0.76	565	EKZE101E□□560MH20D	
68	10×16	0.11	0.47	600	EKZE101E□□680MJ16S	
82	10×20	0.084	0.34	800	EKZE101E□□820MJ20S	
100	12.5×16	0.11	0.34	750	EKZE101E□□101MK16S	
120	10×25	0.069	0.28	900	EKZE101E□□121MJ25S	
150	12.5×20	0.062	0.18	1,100	EKZE101E□□151MK20S	
220	12.5×25	0.047	0.14	1,250	EKZE101E□□221MK25S	
220	16×20	0.048	0.15	1,350	EKZE101E□□221ML20S	
270	12.5×30	0.042	0.13	1,500	EKZE101E□□271MK30S	



Dissipation Factor: 1% Max. (25 °C, 1kHz)

Dissipation Factor ($\tan\delta$)	Rated voltage (Vdc)	6.3V	10V	16V	25V	35V	50V	63V	80V	100V
		tan δ (Max.)	0.22	0.19	0.16	0.14	0.12	0.10	0.09	0.08
When nominal capacitance exceeds 1,000 μ F, add 0.02 to the value above for each 1,000 μ F increase.										

(at 20°C, 120Hz)

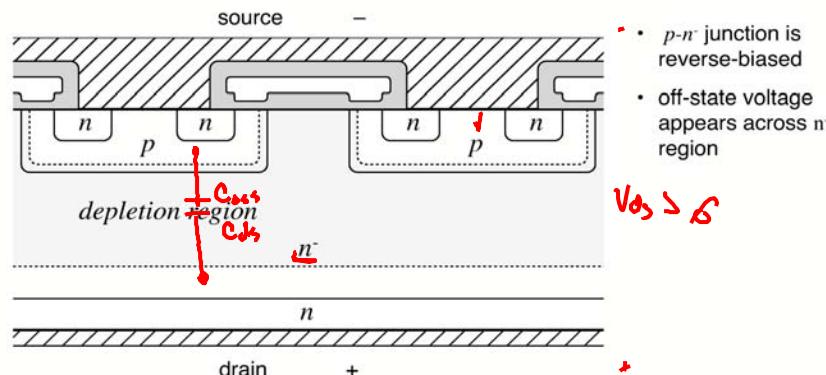


Switching Loss Modeling

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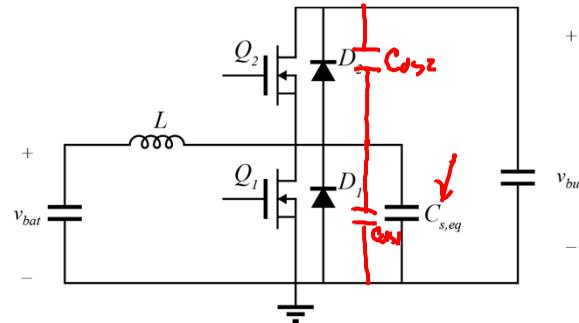


MOSFET Parasitic Capacitances





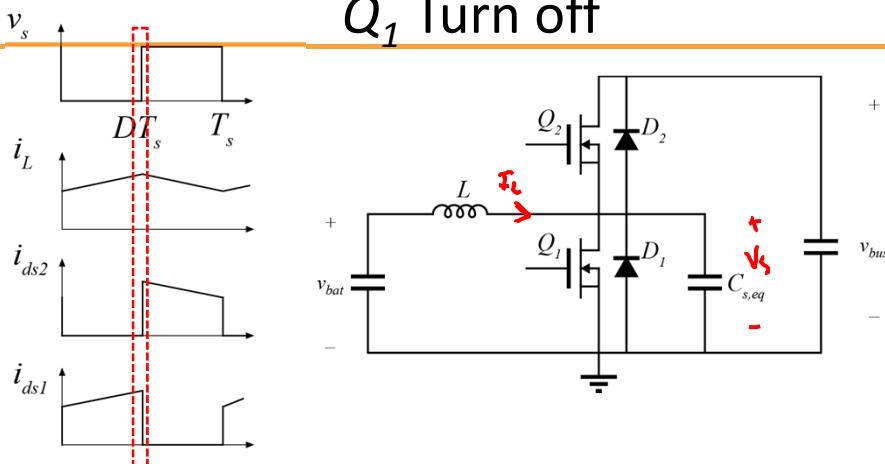
Lump Switched Node Capacitance

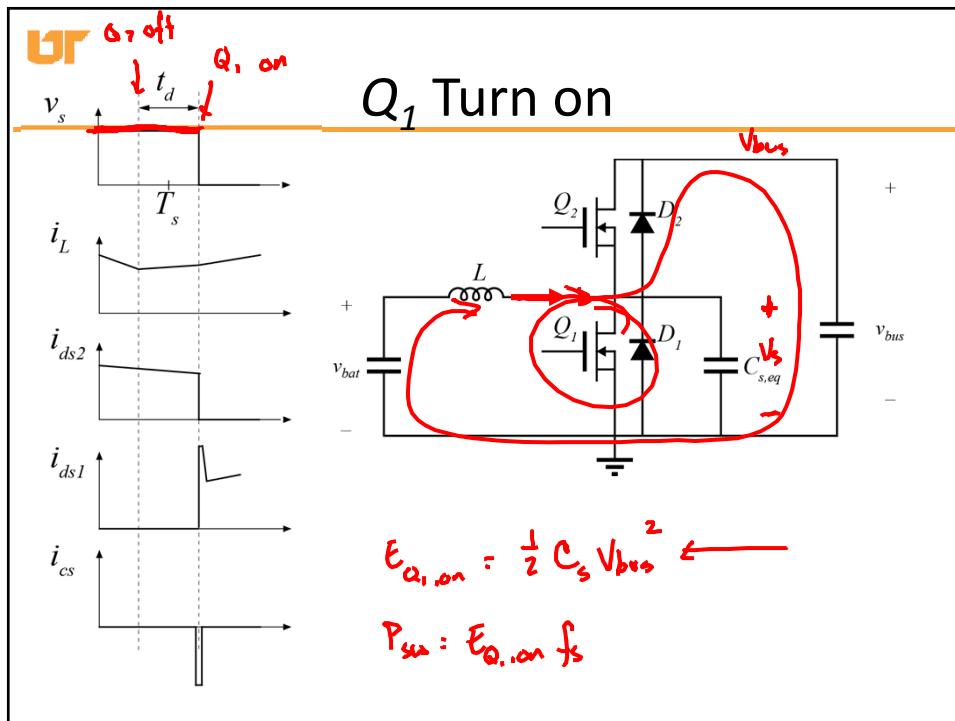
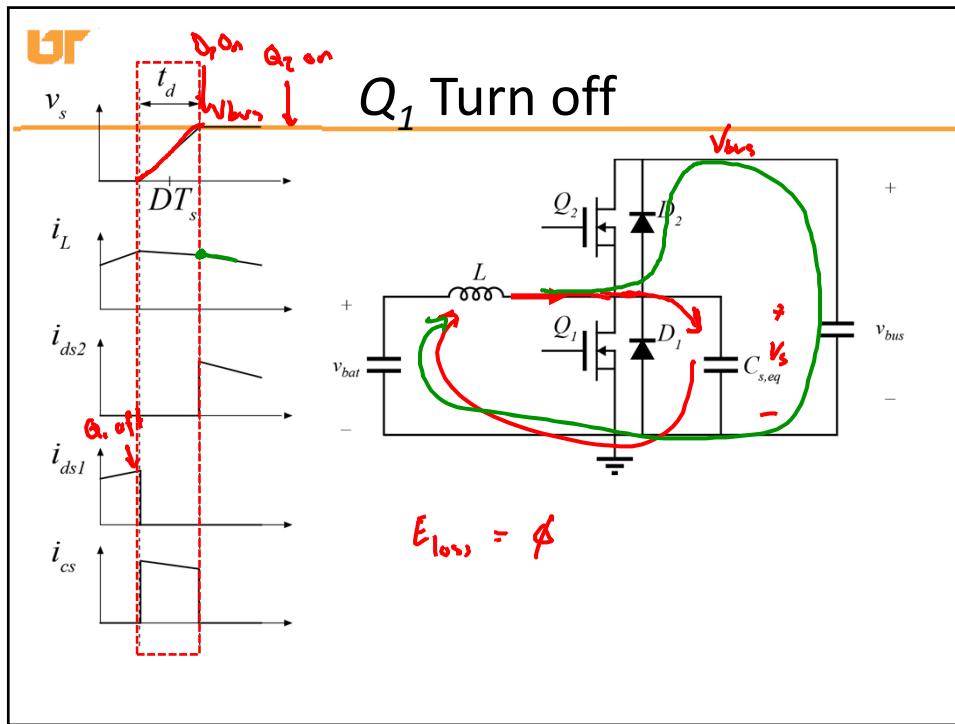


- Consider a single equivalent capacitor at switched node which combines energy storage due to all four semiconductor devices



Q_1 Turn off







Device Output Capacitances

11 Typ. capacitances

$C = f(V_{DS})$; $V_{GS} = 0$ V; $f = 1$ MHz

MUR810G, MUR815G, MUR820G, MUR840G, MUF SUR8820G, SUR8840G

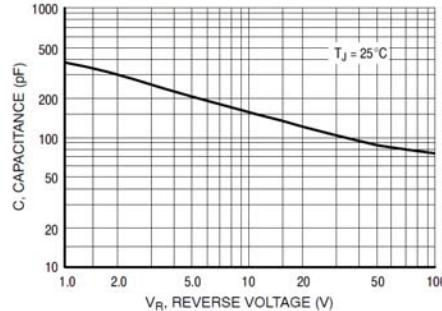
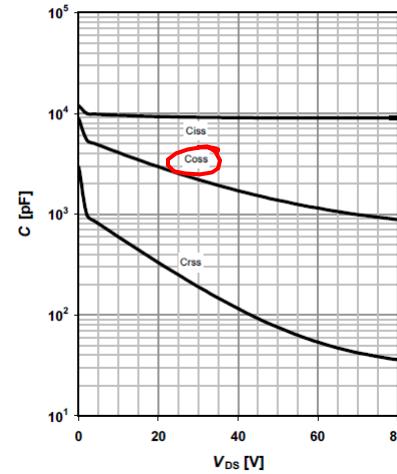


Figure 19. Typical Capacitance



Energy Equivalent Capacitor

- Measurements are small-signal
- At any voltage:

$$\hat{i}_{ds} = C_{oss} \Big|_{V_{ds}} \frac{d\hat{v}_{ds}}{dt}$$

- Total energy is then:

$$E_{ds}(V) = \int_0^t \hat{i}_{ds}(\tau) \hat{v}_{ds}(\tau) d\tau$$

$$E_{ds}(V) = \int_0^t C_{oss} \Big|_{\hat{v}_{ds}(\tau)} \frac{d\hat{v}_{ds}(\tau)}{d\tau} \hat{v}_{ds}(\tau) d\tau$$

$$E_{ds}(V) = \int_0^V v_{ds} C_{ds}(v_{ds}) dv_{ds}$$

$$C_{eq,E}(V) = \frac{2E_{ds}(V)}{V^2}$$

11 Typ. capacitances

$C = f(V_{DS})$; $V_{GS} = 0$ V; $f = 1$ MHz

