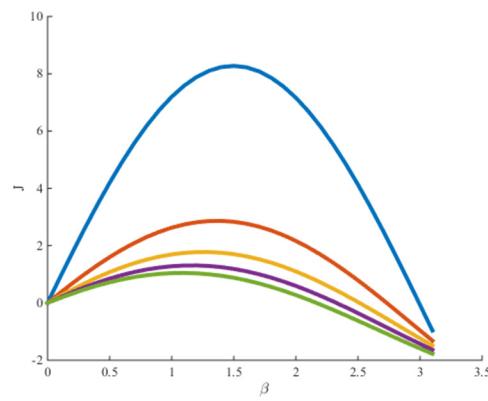


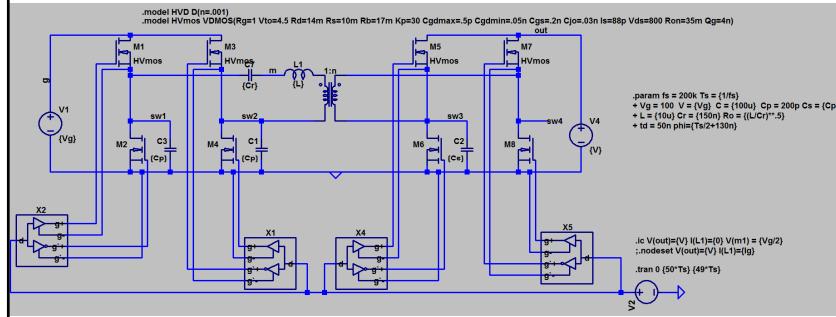
## Simplification



## SRC Control Trajectory

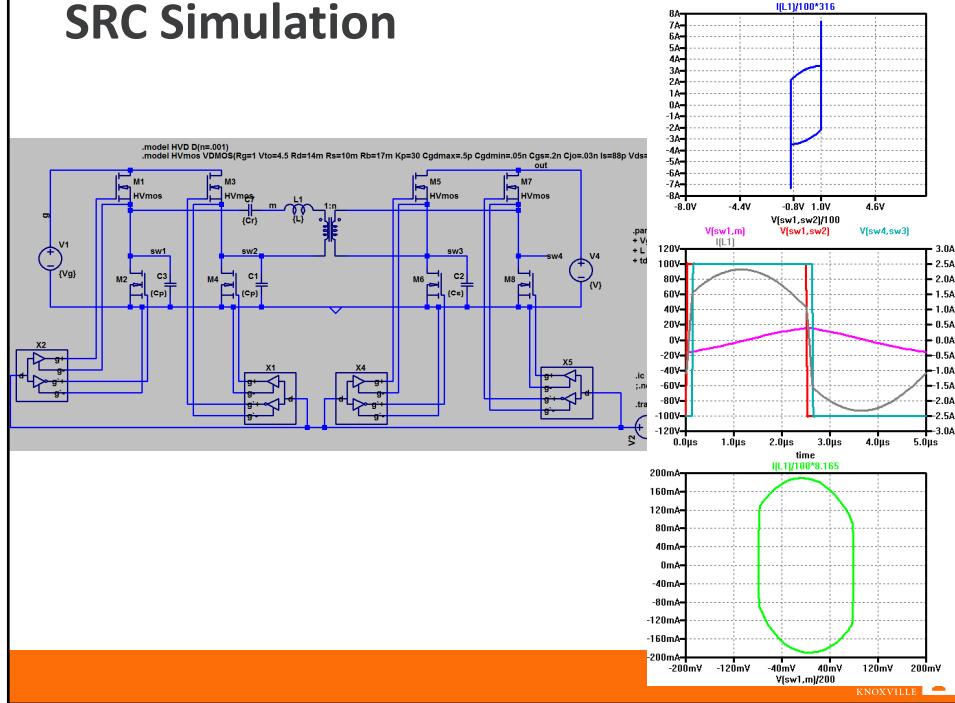


## SRC Simulation

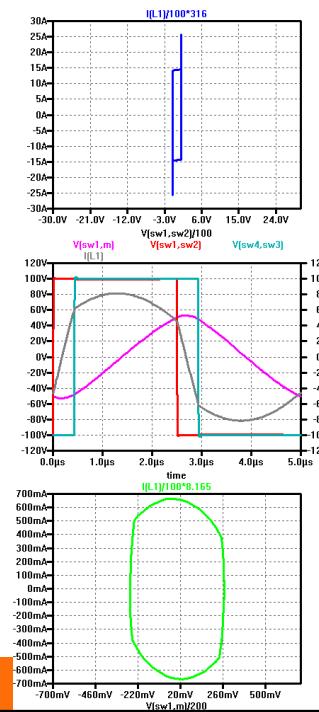


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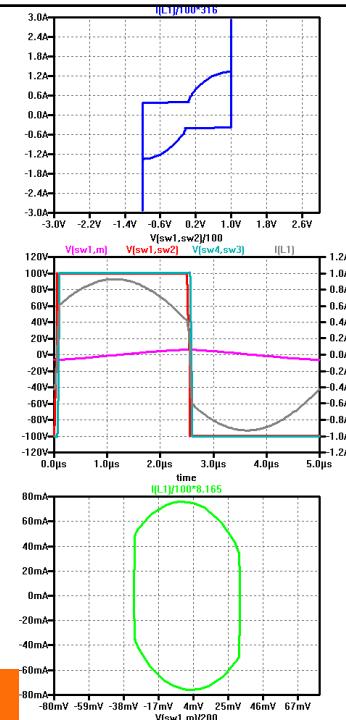
## SRC Simulation



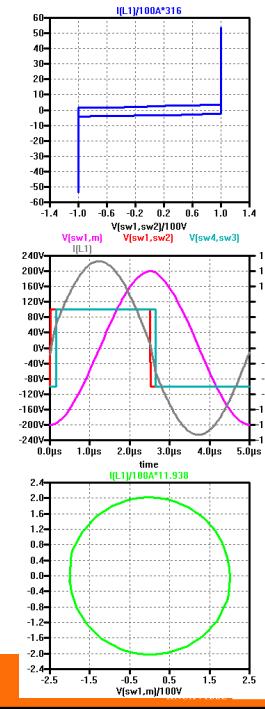
## SRC – Heavy Load



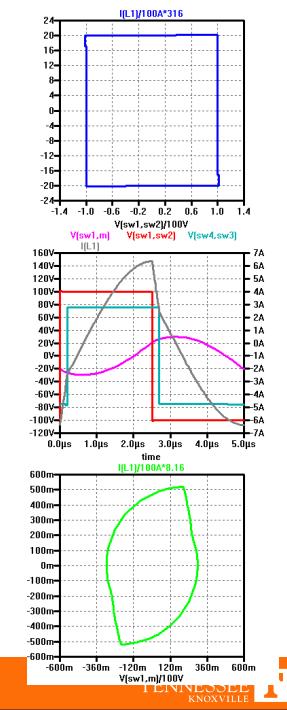
## SRC – Light Load



## SRC Near Resonance

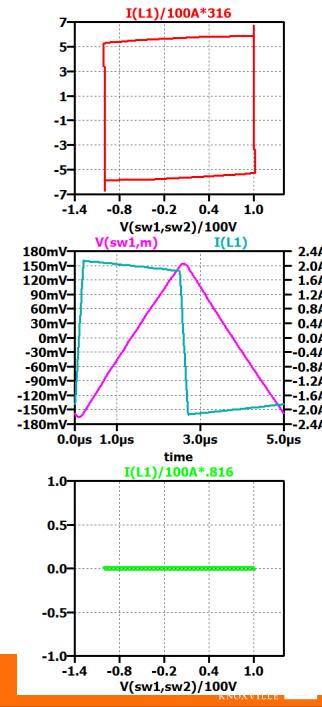


## SRC – Low $V_{out}$

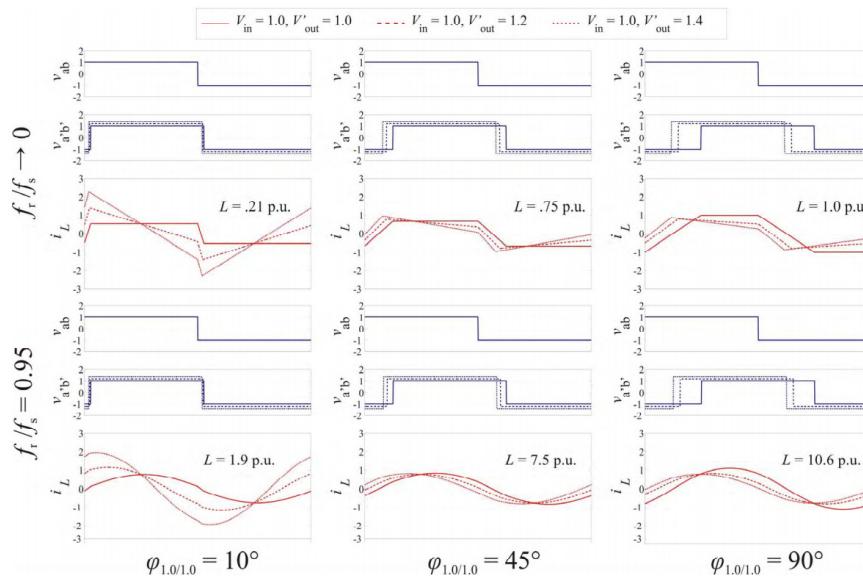


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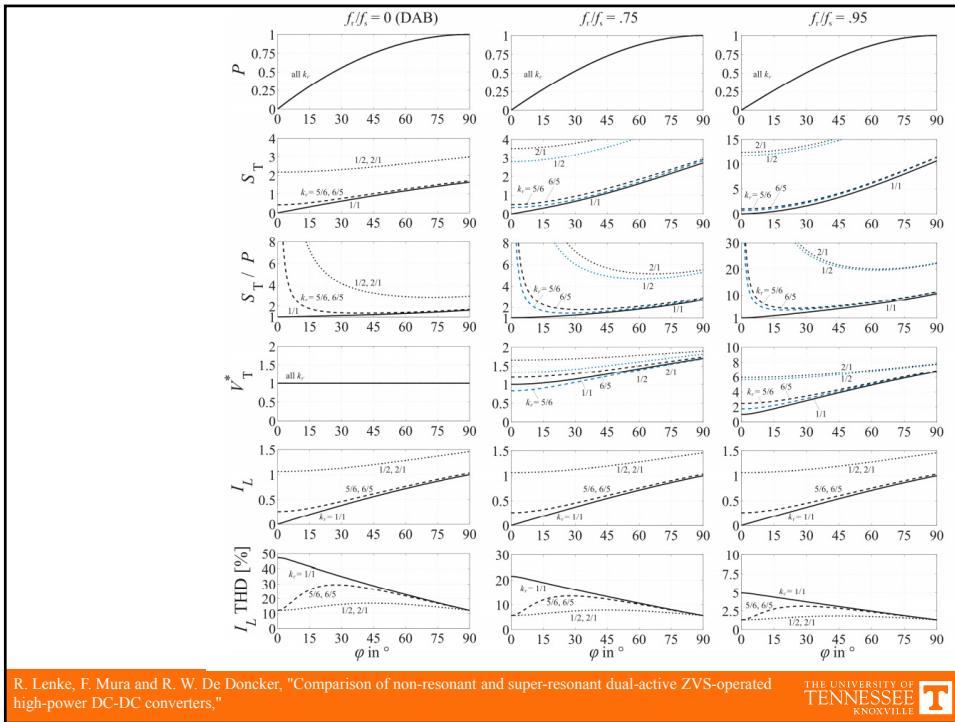
## SRC – F>>1



## DAB vs SRC



R. Lenke, F. Mura and R. W. De Doncker, "Comparison of non-resonant and super-resonant dual-active ZVS-operated high-power DC-DC converters,"



R. Lenke, F. Mura and R. W. De Doncker, "Comparison of non-resonant and super-resonant dual-active ZVS-operated high-power DC-DC converters."

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## DAB vs SRC: Conclusions

### DAB

- + Smaller resonant tank
- + Smaller RMS currents
- + Wider Soft-switching range

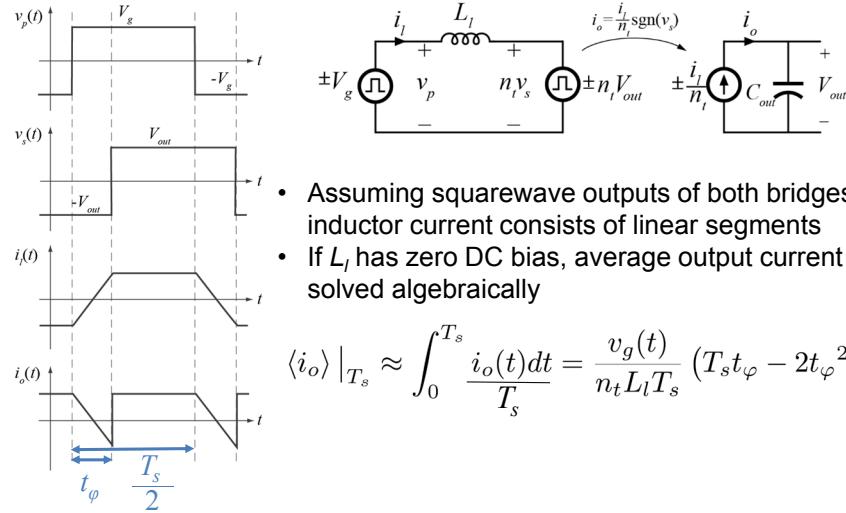
### SRC

- + Can be designed with larger XF inductance
- + Lower AC winding losses
- + Reduced device turn-off losses

R. Lenke, F. Mura and R. W. De Doncker, "Comparison of non-resonant and super-resonant dual-active ZVS-operated high-power DC-DC converters."

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## Linear Averaged Modeling of DAB



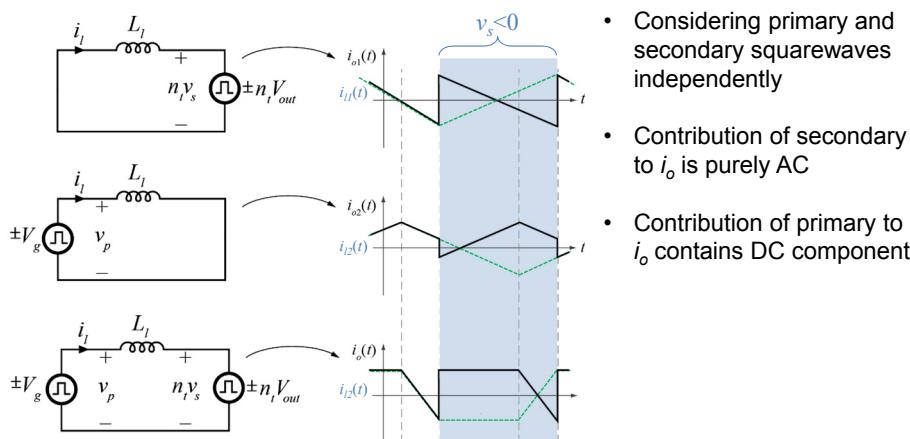
- Assuming squarewave outputs of both bridges, inductor current consists of linear segments
- If  $L_L$  has zero DC bias, average output current solved algebraically

$$\langle i_o \rangle |_{T_s} \approx \int_0^{T_s} \frac{i_o(t) dt}{T_s} = \frac{v_g(t)}{n_t L L T_s} (T_s t_\varphi - 2t_\varphi^2)$$

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## Superposition of Output Current

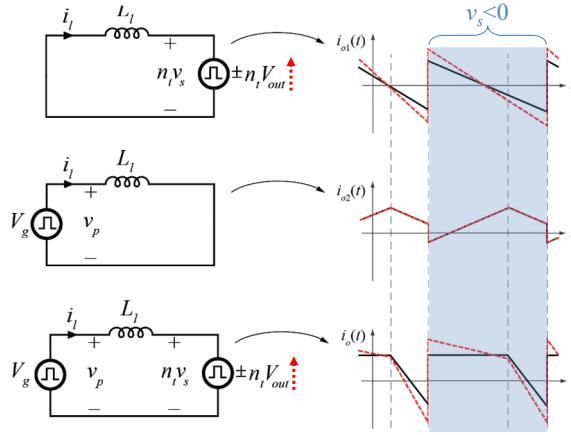


- Considering primary and secondary squarewaves independently
- Contribution of secondary to  $i_o$  is purely AC
- Contribution of primary to  $i_o$  contains DC component

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## Superposition of Output Current



- Considering primary and secondary squarewaves independently
- Contribution of secondary to  $i_o$  is purely AC
- Contribution of primary to  $i_o$  contains DC component
- As  $V_{out}$  increases, only AC component from secondary is increased
- Average current unaffected