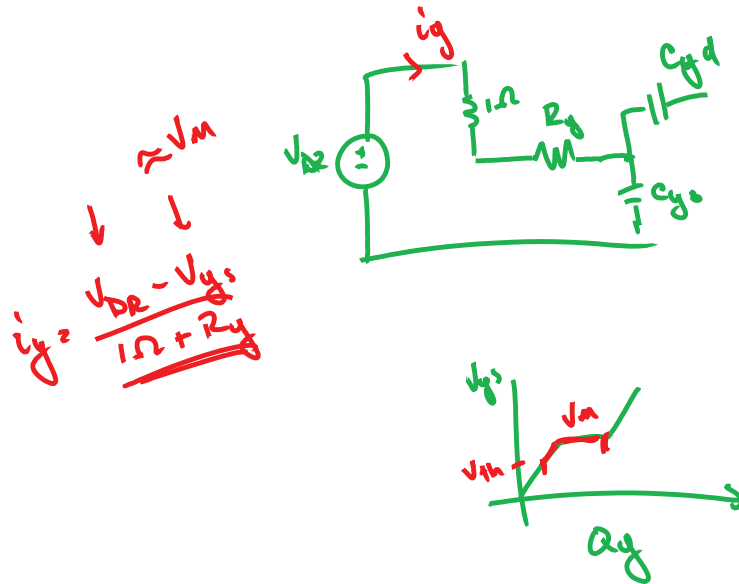
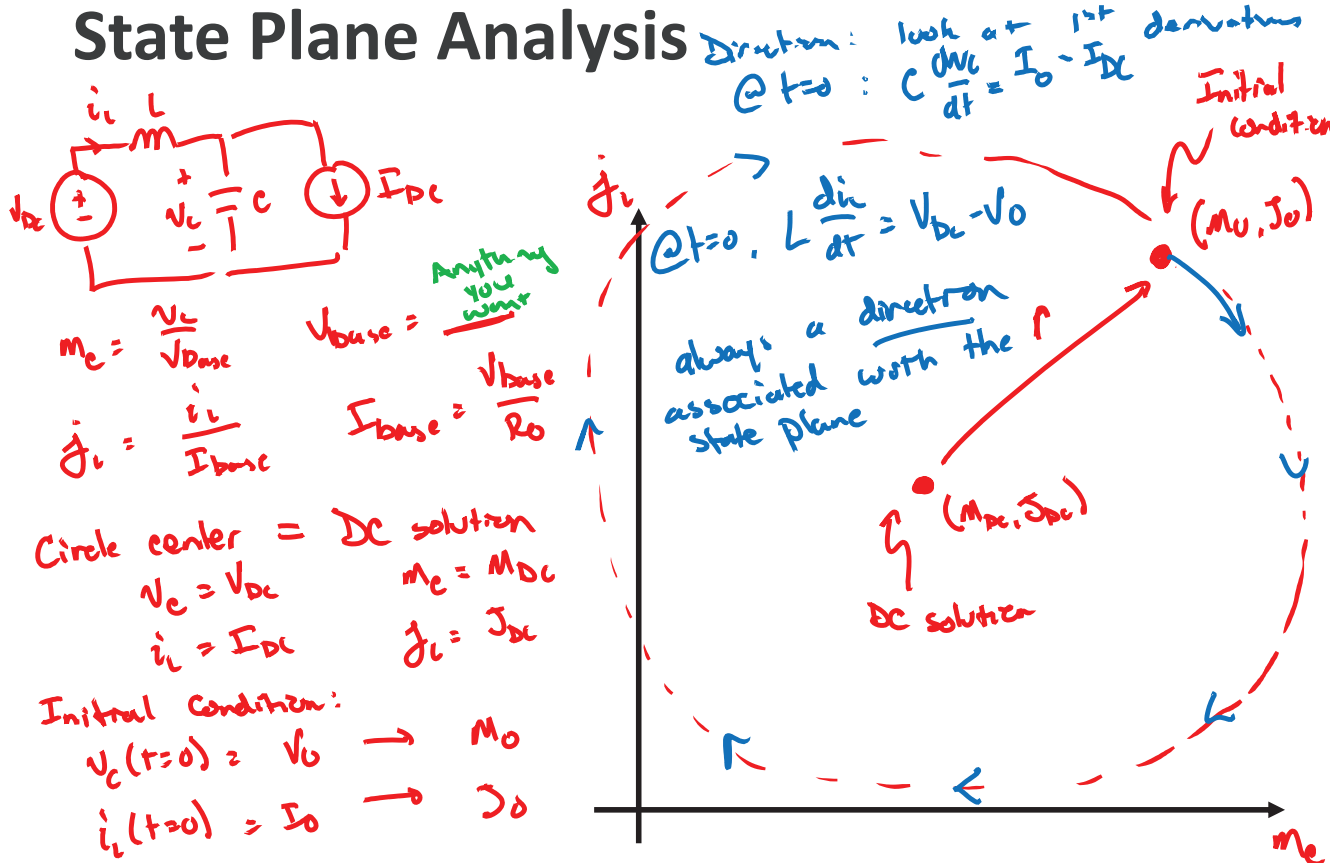


Announcements

- No Office Hours Tuesday, 9/18



State Plane Analysis



[1] R. Oruganti and F. C. Lee, "Resonant Power Processors, Part I – State Plane Analysis", Industry Applications, IEEE Tran. on, vol. 21, no. 6, nov 1985.

[2] D. P. Atherton, Nonlinear Control Engineering. London: Van Nostrand Reinhold, 1982, Ch. 2.

Example Analysis

What is $i_{c,pt}$?

$$i_{c,pt} \cdot \frac{R_0}{V_{base}} = j_{c,pt}$$

$$i_{c,pt} = j_{c,pt} \frac{V_{base}}{R_0}$$

$$j_{c,pt} = I_{DC} + r \sqrt{(m_0 - m_{DC})^2 + (I_0 - I_{DC})^2}$$

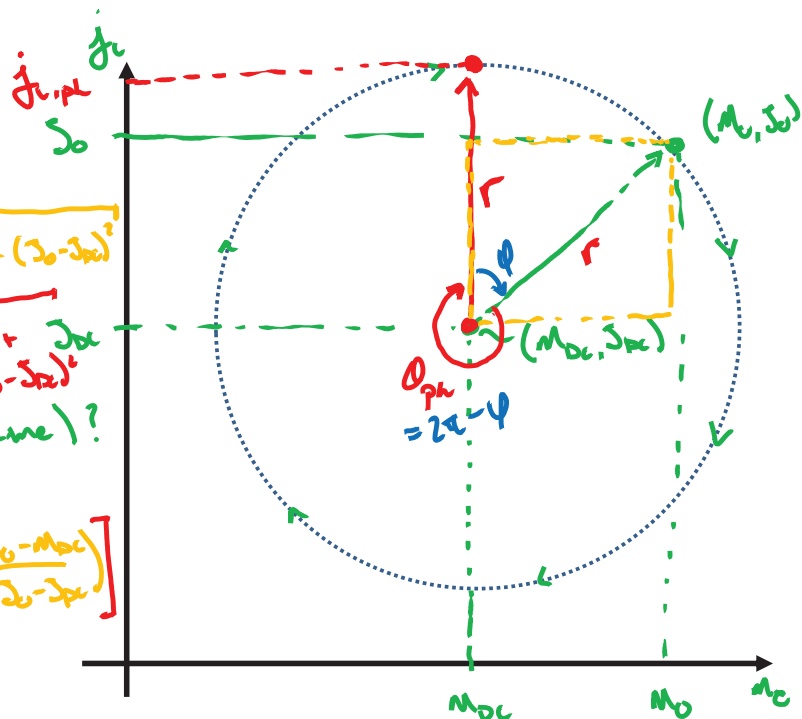
$$j_{c,pt} = I_{DC} + \sqrt{(m_0 - m_{DC})^2 + (I_0 - I_{DC})^2}$$

$$i_{c,pt} = I_{DC} + \frac{V_{base}}{R_0} \sqrt{(m_0 - m_{DC})^2 + (I_0 - I_{DC})^2}$$

When does $i_{c,pt}$ occur (in time)?

$$\theta_{pt} = \omega_0 t_{c,pt}$$

$$t_{c,pt} = \frac{1}{\omega_0} \left[2\pi - \tan^{-1} \left(\frac{m_0 - m_{DC}}{I_0 - I_{DC}} \right) \right]$$



State Plane Algorithm

Start w/ circuit with 1 L & 1 C & DC bias
- May require manipulation or approximation to reduce circuit to 1L - 1C.

(1) Normalize:

$$m_x = \frac{v_x}{V_{base}}, \quad V_{base} \text{ is unconstrained}$$

$$j_x = \frac{i_x}{I_{base}}, \quad I_{base} = \frac{V_{base}}{R_0}$$

$$\theta_x = \omega_0 t_x$$

(2) Plot resonant trajectory on $m_x - j_x$ axes

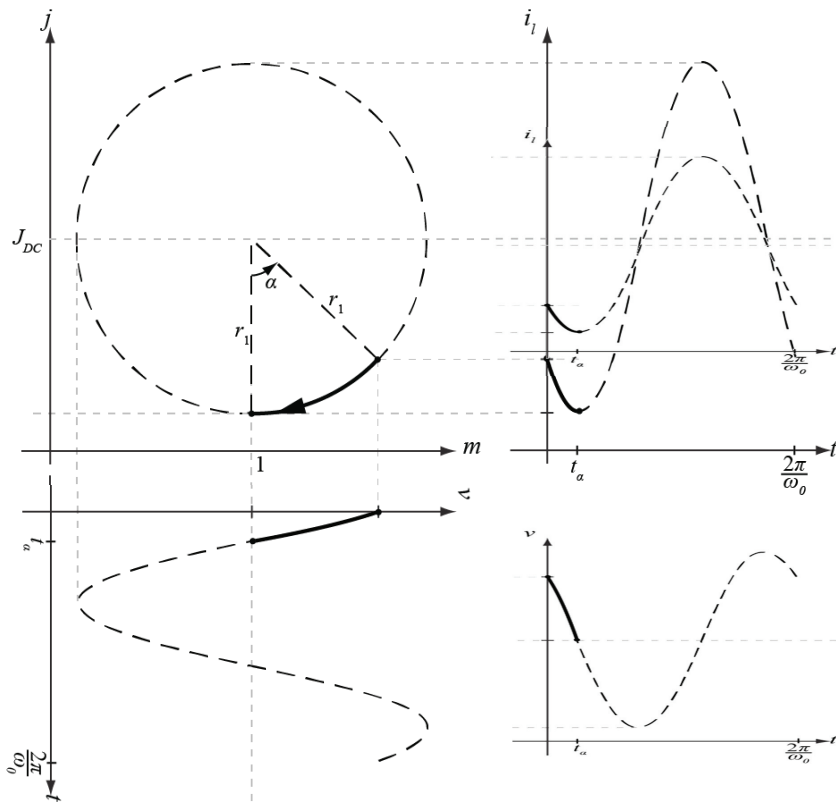
- forms a circle with:

- center @ DC solution
- one point @ initial condition

• direction from FC on first derivatives

(3) Solve for parameters of interest on state plane

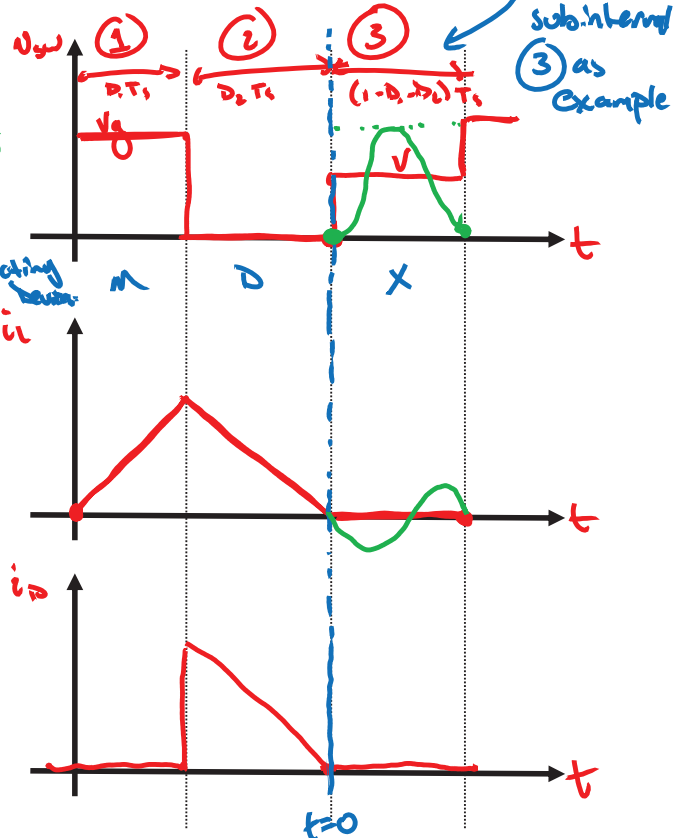
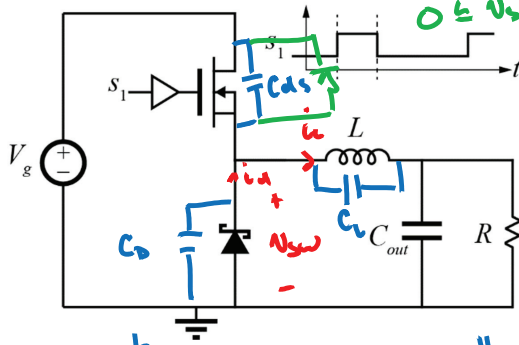
(4) Denormalize.



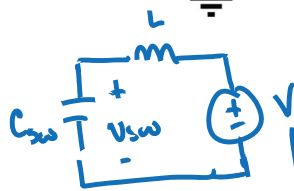
DCM Buck Converter Example (M=1/2)

lets say $V = \frac{V_g}{2}$

diodes enforce $0 \leq v_{sw} \leq V_g$



focus on sub-interval (3) as example



$$C_{sw} = C_{o1} \parallel C_o \parallel C_L$$

DC solution:

$$\begin{aligned} v_{sw} &= V \\ i_L &= \phi \\ v_{sw}'(t=0) &= \phi \\ i_L'(t=0) &= -\frac{V}{L} < \phi \end{aligned}$$

Initial Conditions:

$$\begin{aligned} v_{sw}(t=0) &= \phi \\ i_L(t=0) &= \phi \end{aligned}$$

DCM Buck State Plane

in ③

$$V_{base} = V_g, \quad I_{base} = \frac{V_g}{R_o}$$

$$\text{DC: } v_{sw} = V \rightarrow m_{sw} = \frac{V}{V_g} = M$$

$$i_L = 0 \rightarrow j_L = 0$$

→ center @ (M, 0)

$$\text{IC: } v_{sw} = 0 \rightarrow m_{sw} = 0$$

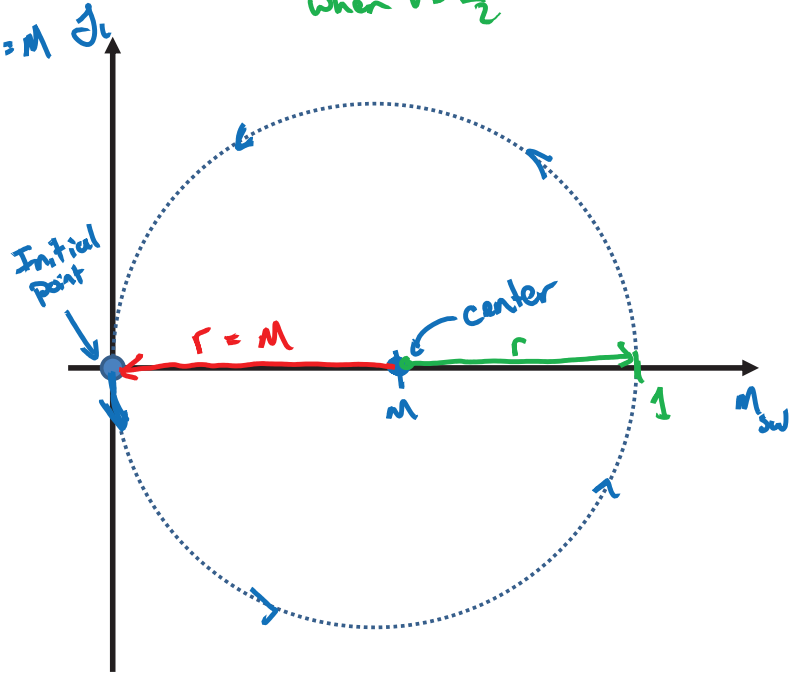
$$i_L = 0 \rightarrow j_L = 0$$

Direction:

diode-limited

$$0 \leq v_{sw} \leq V_g$$

$$0 \leq m_{sw} \leq 1$$



$$M = \frac{1}{2}$$

when $V = \frac{V_g}{2}$