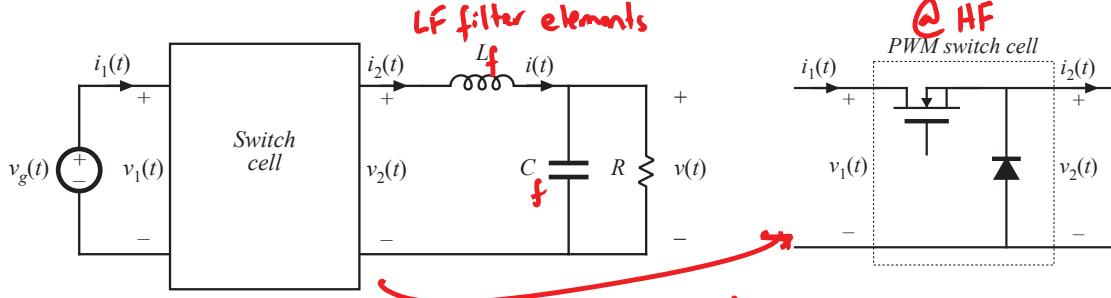


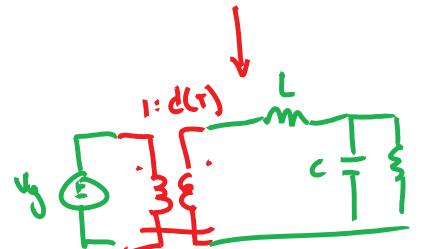
# Identification of Resonant Switch



for PWM converter:

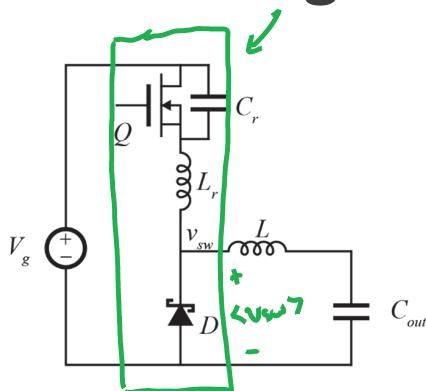
$$\langle v_2 \rangle = d(t) \langle v_1 \rangle$$

$$\langle i_s \rangle = d(t) \langle i_L \rangle$$



Averaged, nonlinear

## Switching Cell Conversion Ratio



$M = f(F, \beta_L)$  for ZVS-QR Buck  
derived according to  $\langle v_{sw} \rangle = V$

In this case:  $M = \frac{V}{V_g} = \frac{\langle v_{sw} \rangle}{V_g}$

more generally

$M = \text{switch cell conversion ratio} = \frac{\langle v_2 \rangle}{\langle v_1 \rangle}$

for Buck only  $M = \mu$

for PWM buck,  $M = d$

Replace  $d$  with  $M$  of any resonant switch cell, you get the behavior of the parent PWM converter with that switch cell.

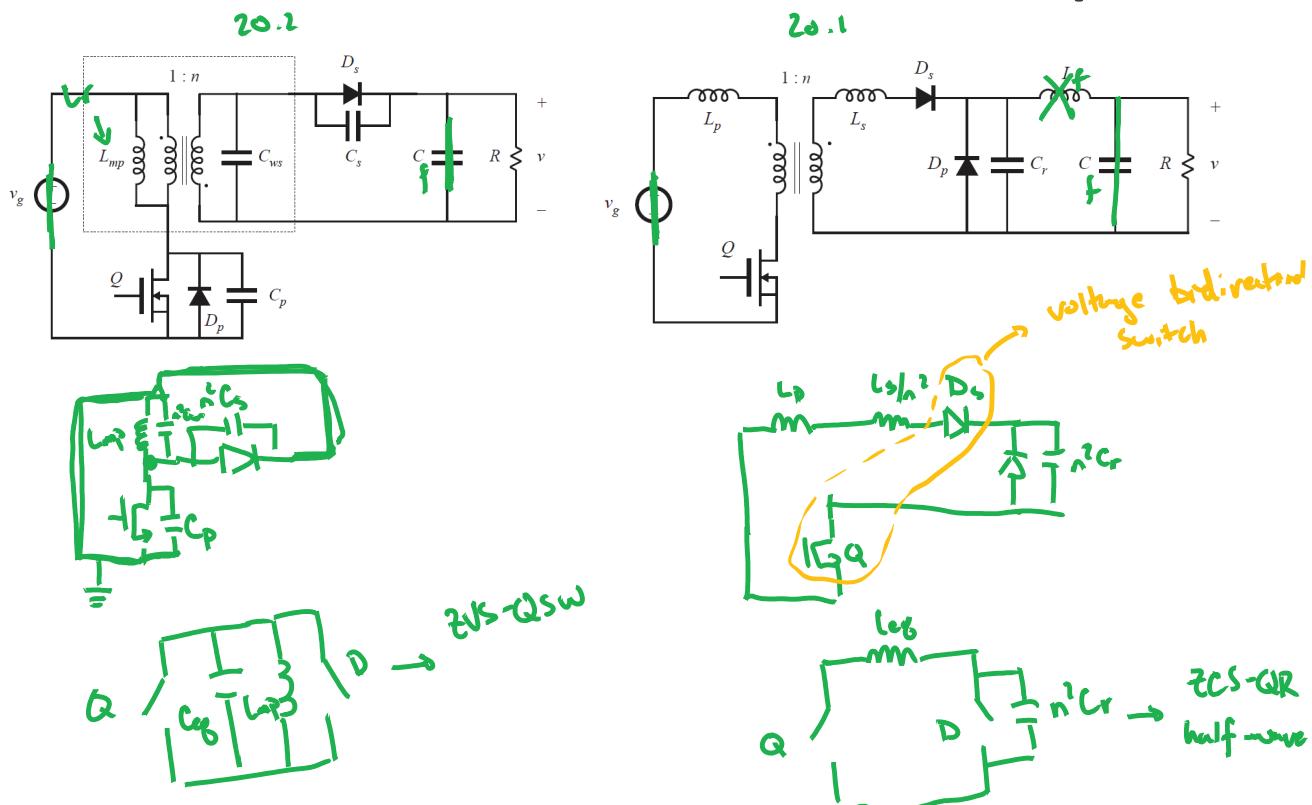
# Conversion Ratios of Various Switch Cells

$$P_{1/2}(x) = \frac{1}{2\pi} \left[ \frac{1}{2}x + \pi + \sin^{-1}x + \frac{1}{x} \left( 1 - \sqrt{1 - x^2} \right) \right]$$

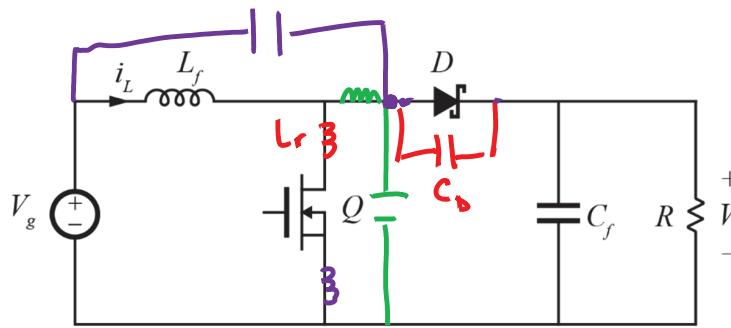
$$\rightarrow P_1(x) = \frac{1}{2\pi} \left[ \frac{1}{2}x + 2\pi + \sin^{-1}x + \frac{1}{x} \left( 1 - \sqrt{1 - x^2} \right) \right] \approx 1$$

Switch Cell	Conv. Ratio $\mu$	Load Current Range	Conv. Ratio Range	Requirements on Q
PWM	$D$	N/A	$0 \leq \mu \leq 1$	
ZVS-QR (half)	$1 - FP_{\frac{1}{2}} \left( \frac{1}{J_L} \right)$	$0 \leq J_L \leq \infty$	$0 \leq \mu \leq 1$	
ZVS-QR (full)	$1 - FP_1 \left( \frac{1}{J_L} \right)$	$0 \leq J_L \leq \infty$	$0 \leq \mu \leq 1$	Bidirectional voltage
ZCS-QR (half)	$FP_{\frac{1}{2}}(J_L)$	$1 \leq J_L \leq \infty$	$0 \leq \mu \leq 1$	Unidirectional Current* 
ZCS-QR (full)	$FP_1(J_L)$	$1 \leq J_L \leq \infty$	$0 \leq \mu \leq 1$	

## Resonant Switch Identification Examples



# ZCS-QR Boost

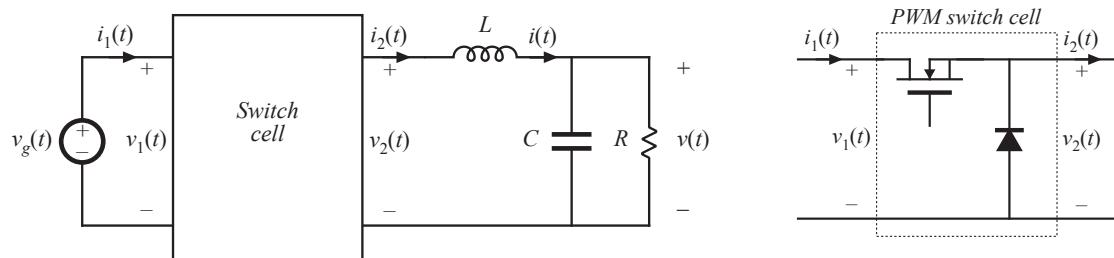


$$\text{PWM Boost} : M = \frac{1}{1-d(\tau)}$$

$$\text{ZCS-QR Boost} : M = \frac{1}{1-m(\tau)}$$

$$m = F P_{n_2}(\beta_2) \quad (\text{if half-wave})$$

## SSM - PWM Parent



PWM:

$$\langle v_2 \rangle = d(t) \langle v_1 \rangle$$

$$\langle i_1 \rangle = d(t) \langle i_2 \rangle$$

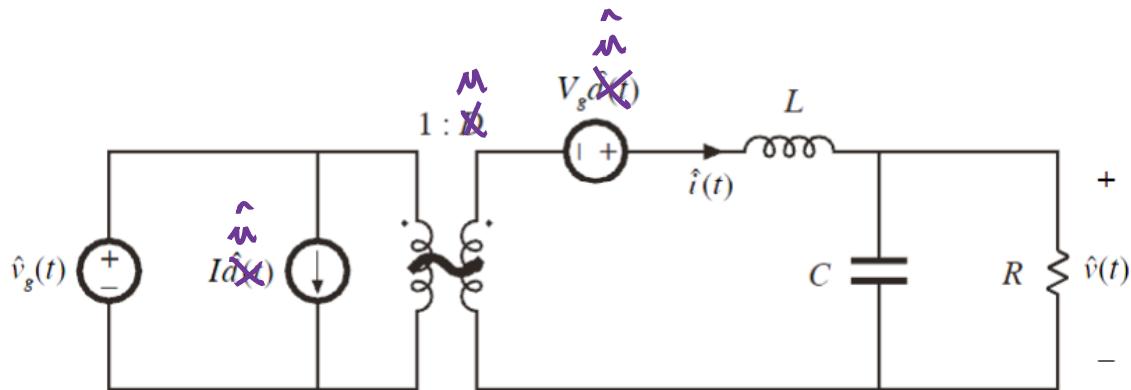
Linearize, SSM

$$\hat{v}_2 = \hat{v}_1 \hat{d} + D \hat{v}_1$$

$$\hat{i}_1 = I_2 \hat{d} + D \hat{i}_2$$

# SSM, PWM Case

Textbook, Fig.7.17(a)



Replace  $D \rightarrow M$  and  $\hat{d} \rightarrow \hat{m}$  PWA converter AC  
SSM model becomes resonant switch SSM

## ZVS-QR Switch Cell SSM

$$m = 1 - \frac{F}{2\pi} \left[ \frac{1}{2\beta_L} + \pi + \sin^{-1} \left( \frac{1}{\beta_L} \right) + \sqrt{\beta_L^2 - 1} + \beta_L \right]$$

$$F = \frac{f_s}{f_0} \quad \beta_L = \frac{I_L}{V_g} R_0$$

$m$  depends on  $f_s$ ,  $i_L$ , and  $V_g$

$$m = k_i \hat{i}_L + k_c \hat{f}_s + k_v \hat{v}_g , \quad \left\{ \begin{array}{l} k_i = \frac{\partial m}{\partial i_L} |_{DC} \\ k_c = \frac{\partial m}{\partial f_s} |_{DC} \\ k_v = \frac{\partial m}{\partial v_g} |_{DC} \end{array} \right.$$

# SSM, Soft-Switching Buck

