## Resonant Circuit Analysis




## Soft Switching

- Advantages
- Reduced switching loss
- Possible operation at higher switching frequency
- Lower EMI
- Disadvantages
- Increased current and/or voltage stresses due to circulating current
- Higher peak and rms current values
- Complexity of analysis and modeling


## Limitations: Gate Drive




## Limitations: $t_{d} / T_{s}$





## Limitations: Thermal



## Limitations: Magnetics Design

Flux density


Current Density



## Limitations: Circuit Modeling




## ZVS with Si diode



- ZVS turn-ON
- Eliminated losses due to $C_{s w}$ discharge during turn-ON transient
- Eliminated losses due to MOSFET $d i_{F} / d t$ during turn-ON transient
- Diode reverse recovery still impacts the waveforms and losses
- Increased current ripple
- Increased conduction losses (by >30\%)
- Increased $d v_{d s} / d t$ upon turnOFF, MOSFET turn-OFF speed is more important


## Loss Breakdown: Soft-Switched Si Boost

$$
\begin{gathered}
f_{s}=100 \mathrm{kHz} \\
P_{\text {loss }}=5.7 \mathrm{~W}, \eta=98.1 \%
\end{gathered}
$$



Reverse-recovery: $21 \%$ of the total loss
$f_{s}=1 \mathrm{MHz}$
$P_{\text {loss }}=17.7 \mathrm{~W}, \eta=94.4 \%$
Experiment: $\eta=95.1 \%$


Reverse-recovery:
$68 \%$ of the total loss

## Soft-switched SiC diode



SiC diode, "soft-switched" operation

$f_{s}=1 \mathrm{MHz}$

MOSFET

- $d i_{/} / d t=200 \mathrm{~A} / \mu \mathrm{s}$
- $C_{d s, e q}=45 \mathrm{pF}$
- $R_{\text {on }}=0.15 \Omega$

SiC diode

- $t_{r r}=0, Q_{r r}=0$
- $2 C_{d, Q e q} C_{d, e q}=64 \mathrm{pF}$
- $V_{D}=1.8 \mathrm{~V}$


## Soft-switched Boost with SiC diode

Conduction losses only, $2^{\text {nd- }}$ order switching losses not included in the model


Power supply technology limits become dominated by:

- Magnetics
- $2^{\text {nd }}-$ order switching loss mechanisms, e.g. gate-drive losses, parasitic inductances (layout and packaging)
- Gate-drive circuitry and controllers to support high-frequency operation


## Speed Limitations with WBG Devices



TriQuint TGF2023-02
12W, DC-to-18 GHz
RF/microwave HEMT
FOM for switching applications
$C_{d s} R_{\text {on }} \approx 1 \Omega p F$
$Q_{g} R_{o n} \approx 10 \Omega p C$

Standard hard-switched PWM operation at 50 MHz $d v_{d s} / d t$ dominated by probe (4 pF) capacitance


Emerging GaN HEMT devices may enable completely new RF-based design approaches in power electronics

## VHF power electronics

|  | Resonant Design <br> Value | Type |  |
| :---: | :---: | :---: | :---: |
| Component | Coilcraft 1812SMS |  |  |
| $L_{F}$ | 33 nH | Coilcraft A04TG |  |
| $L_{2 F}$ | 12.5 nH | 1812SMS |  |
| $L_{\text {rect }}$ | 22 nH | ATC100A |  |
| $C_{2 F}$ | 39 pF | ATC100A |  |
| $C_{\text {rect }}$ | 10 pF | Multilayer Ceramics |  |
| $C_{\text {out }}$ | $75 \mu \mathrm{~F}$ | Multilayer Ceramics |  |
| $C_{\text {in }}$ | $22 \mu \mathrm{~F}$ | Frescale MRF6S9060 |  |
| $S_{\text {main }}$ |  | Fairchild S310 |  |
| $D$ |  | Conventional Design |  |
| Type |  |  |  |
| Component | Value |  |  |
| $L_{\text {boost }}$ | $10 \mu \mathrm{H}$ | Coilcraft D03316T-103ML |  |
| $C_{\text {out }}$ | $75 \mu \mathrm{~F}$ | Multilayer Ceramics |  |
| $C_{\text {in }}$ | $22 \mu \mathrm{~F}$ | Multilayer Ceramics |  |
| $S_{\text {main }}$ |  | LT1371HV |  |
| $D$ |  | Fairchild S310 |  |




## Topics Covered

## - Course Topics

- High Frequency Power Conversion
- Switching losses and device selection
- Resonance in power electronics
- Soft switching (ZVS and ZCS)
- Magnetics design
- Non-resonant soft switching converters
- Constant frequency control
- State-plane analysis
- Resonant switches
- Modeling and Simulation
- Discrete time models
- Resonant Converters
- Resonant converter topologies
- Sinusoidal analysis
- AC-modeling and frequency modulation
- State-plane analysis
- Applications and practical issues of high frequency converters

