

Lecture 8

Recap

Introduction

CT->DT

Impulse
Invariance

Bilinear Trans.

Example

Digital Signal Processing

Lecture 8 - Filter Design - IIR

Electrical Engineering and Computer Science
University of Tennessee, Knoxville

Overview

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Roadmap

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Example

- Introduction
- Discrete-time signals and systems - LTI systems
 - Unit sample response $h[n]$: uniquely characterizes an LTI system
 - Linear constant-coefficient difference equation
 - Frequency response: $H(e^{j\omega})$
 - Complex exponential being eigenfunction of an LTI system: $y[n] = H(e^{j\omega})x[n]$ and $H(e^{j\omega})$ as eigenvalue.
- z transform
 - The z-transform, $X(z) = \sum_{n=-\infty}^{\infty} x[n]z^{-n}$
 - Region of convergence - the z-plane
 - System function, $H(z)$
 - Properties of the z-transform
 - The significance of zeros
 - The inverse z-transform, $x[n] = \frac{1}{2\pi j} \oint_C X(z)z^{n-1} dz$:
inspection, power series, partial fraction expansion
- Sampling and Reconstruction
- Transform domain analysis - nwz

Review - Design structures

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Example

- Different representations of causal LTI systems
 - LCDE with initial rest condition
 - $H(z)$ with $|z| > R_+$ and starts at $n = 0$
- Block diagram vs. Signal flow graph and how to determine system function (or unit sample response) from the graphs
- Design structures
 - Direct form I (zeros first)
 - Direct form II (poles first) - Canonic structure
 - Transposed form (zeros first)
- IIR: cascade form, parallel form, feedback in IIR (computable vs. noncomputable)
- FIR: direct form, cascade form, parallel form, linear phase
- Metric: computational resource and precision
- Sources of errors: coefficient quantization error, input quantization error, product quantization error, limit cycles
 - Pole sensitivity of 2nd-order structures: coupled form
 - Coefficient quantization examples: direct form vs. cascade form

Rationale

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Example

- Review of complex exponentials as eigenfunctions of the LTI
 - $x[n] = e^{j\omega_0 n} \rightarrow y[n] = H(e^{j\omega_0})e^{j\omega_0 n}$
 - or $x[n] = \cos \omega_0 n \rightarrow y[n] = |H(e^{j\omega_0})| \cos(\omega_0 n + \theta)$
- Separation of signal when they occupy different frequency bands — choose the system function that is unity at selective frequencies
- Given a set of specifications, design a rational transfer function that approximates the ideal filter maintaining specifications of δ_p , δ_s , and the transition band.

Stages of digital filter design

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Example

- The specification of the desired properties of the system
 - application-dependent
 - usually done in the frequency domain
- The **approximation** of the specifications using a causal discrete-time system
- The realization of the system
 - e.g., DSP board

Practical frequency-selective filters

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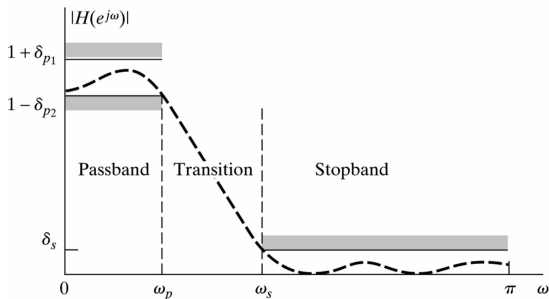
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Example

- Approximate ideal filters by a rational function or LCDE



- Factors that affect the filter performance
 - the maximum tolerable passband ripple, $20 \log_{10} \delta_p$
 - the maximum tolerable stopband ripple, $20 \log_{10} \delta_s$
 - the passband edge frequency ω_p
 - the stopband edge frequency ω_s
 - M and N : order of the LCDE

Example

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Example

- Design a discrete-time lowpass filter to filter a continuous-time signal with the following specs (with a sampling rate of 10^4 samples/s):
 - The gain should be within ± 0.01 of unity in the frequency band $0 \leq \Omega \leq 2\pi(2000)$
 - The gain should be no greater than 0.001 in the frequency band $2\pi(3000) \leq \Omega$
- Parameter setup
 - $\delta_{p1} = \delta_{p2} = 0.01, \delta_s = 0.001$
 - $\omega_p = 2\pi(2000)/10^4, \omega_s = 2\pi(3000)/10^4$
 - Ideal passband gain in decibels?
 - maximum passband gain in decibels?
 - maximum stopband gain in decibels?

Design techniques for IIR filters

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Example

- Analytical — closed-form solution of transfer function
- **Continuous-time** → **Discrete-time**
- Algorithmic

General guidelines for CT->DT

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Example

continuous \rightarrow discrete

$$H_a(s) \rightarrow H(z)$$

$$h_a(t) \rightarrow h[n]$$

- $j\Omega$ -axis (s-plane) \rightarrow unit circle (z-plane)
- if $H_a(s)$ is stable $\rightarrow H(z)$ is stable

Different CT->DT approaches

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Example

- Mapping differentials to differences
 - $z = 1 + sT$
 - the $j\Omega$ -axis is NOT mapped to the unit circle
 - stable poles might not be mapped to inside the unit circle
- Impulse invariance
- Bilinear transformation

Impulse invariance

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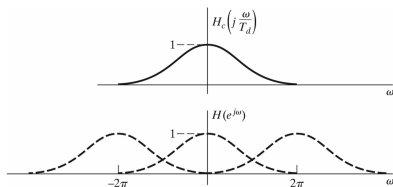
Bilinear Trans.

Example

$$h[n] = T_d h_c(nT_d) \quad (1)$$

$$H(e^{j\omega}) = \sum_{k=-\infty}^{\infty} H_c\left[\frac{j\omega}{T_d} + \frac{j2\pi k}{T_d}\right] \quad (2)$$

- Preserve good time-domain characteristics
- Linear scaling of frequency axis, $\omega = \Omega T$
- Existence of **aliasing**
- Impulse invariance doesn't imply step invariance



Impulse invariance (cont')

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Example

$$H_C(s) = \sum_{k=1}^N \frac{A_k}{s - s_k} \rightarrow H(z) = \sum_{k=1}^N \frac{T_d A_k}{1 - e^{s_k T_d} z^{-1}}$$

- Mapping poles

$$s = s_k \rightarrow z = e^{s_k T_d}$$

- Preserve residues

- $s = j\Omega \rightarrow z = e^{j\Omega T_d} = e^{j\omega}$, the unit circle

- if s_k is stable, i.e., region of s_k is less than 0,
 $\rightarrow |z_k| < 1 \rightarrow$ digital filter is stable

Impulse invariance - An example

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Example

- Find the system function of the digital filter mapped from the analog filter with a system function $H_c(s) = \frac{s+a}{(s+a)^2+b^2}$. Compare magnitude of the frequency response and pole-zero distributions in the s- and z-plane
- Sol: $H(z) = \frac{1 - (e^{-aT} \cos bT)z^{-1}}{(1 - e^{-(a+jb)T}z^{-1})(1 - e^{-(a-jb)T}z^{-1})}$
- Note that zeros are not mapped. Also note that $|H_s(j\Omega)|$ is not periodic but $|H(e^{j\omega})|$ is.

Bilinear transformation

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Example

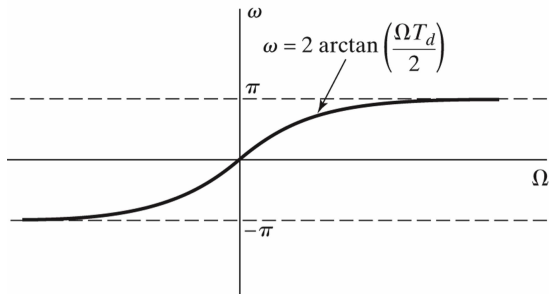
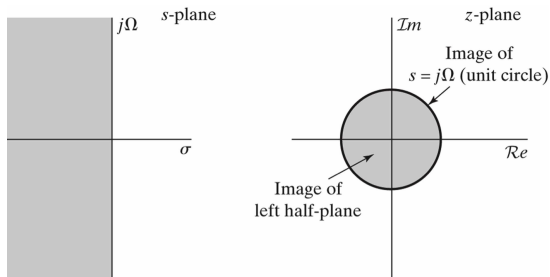
- Mapping from s-plane to z-plane by relating s and z according to a bilinear transformation. $H_c(s) \rightarrow H(z)$

$$s = \frac{2}{T} \left(\frac{1 - z^{-1}}{1 + z^{-1}} \right), \text{ or } z = \frac{1 + \frac{sT}{2}}{1 - \frac{sT}{2}}$$

- Two guidelines
 - Preserves the frequency characteristics? I.e., maps the $j\Omega$ -axis to the unit circle?
 - Stable analog filter mapped to stable digital filter?
- Important properties of bilinear transformation
 - Left-side of the s-plane \rightarrow interior of the unit circle; Right-side of the s-plane \rightarrow exterior of the unit circle. Therefore, stable analog filters \rightarrow stable digital filters.
 - The $j\Omega$ -axis gets mapped exactly **once** around the unit circle.
 - No aliasing
 - The $j\Omega$ -axis is infinitely long but the unit circle isn't \rightarrow nonlinear distortion of the frequency axis

Bilinear transformation - Mappings

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Bilinear transformation - How to tolerate distortions?

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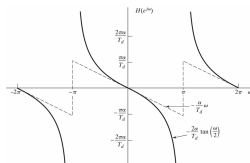
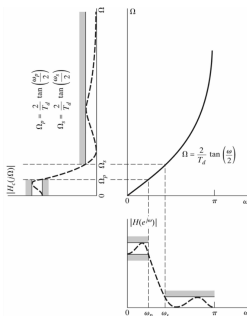
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Example

- **Prewarp** the digital cutoff frequency to an analog cutoff frequency through $\Omega = \frac{2}{T} \tan \frac{\omega}{2}$
- Better used to approximate **piecewise constant** filters which will be mapped as constant as well
- Can't be used to obtain digital lowpass filter with linear-phase



- Avoid aliasing at the price of distortion of the frequency axis

The class of analog filters

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Example

■ Butterworth filter

- $|H_c(j\Omega)|^2 = \frac{1}{1+(\frac{j\Omega}{j\Omega_c})^{2N}}$

- Note about the butterworth circle with radius Ω_c

- Ω_c is also called the 3dB-cutoff frequency when $-10\log_{10}|H_c(j\Omega)|^2|_{\Omega=\Omega_c} \approx 3$

- Monotonic function in both passband and stopband

- Matlab functions: `buttord`, `butter`

■ Chebyshev filter

- Type I Chebyshev has an equiripple freq response in the passband and varies monotonically in the stopband,

- $|H_c(j\Omega)|^2 = \frac{1}{1+\epsilon^2 T_N^2(\Omega/\Omega_p)}$

- Type II Chebyshev is monotonic in the passband and equiripple in the stopband, $|H_c(j\Omega)|^2 = \frac{1}{1+\epsilon^2 [\frac{T_N(\Omega_s/\Omega_p)}{T_N(\Omega_s/\Omega)}]^2}$

- Matlab functions: `cheb1ord`, `cheby1`, `cheb2ord`, `cheby2`

The class of analog filters (cont'd)

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■ Elliptic filter

- $|H_c(j\Omega)|^2 = \frac{1}{1 + \epsilon^2 R_N^2(\Omega/\Omega_p)}$ where $R_N(\Omega)$ is a rational function of order N satisfying the property $R_N(1/\Omega) = 1/R_N(\Omega)$ with the roots of its numerator lying within the interval $0 < \Omega < 1$ and the roots of its denominator lying in the interval $1 < \Omega < \infty$
- Equiripple in both the passband and the stopband
- Matlab functions: `ellipord`, `ellip`

Example

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Example

- Specs of the discrete-time filter: passband gain between 0dB and -1dB, and stopband attenuation of at least -15dB.

$$1 - \delta_p \geq -1 \text{ dB}, \delta_s \leq -15 \text{ dB}$$

$$20 \log_{10} |H(e^{j0.2\pi})| \geq -1 \rightarrow |H(e^{j0.2\pi})| \geq 10^{-0.05} = 0.8913 \quad (3)$$

$$20 \log_{10} |H(e^{j0.3\pi})| \leq -15 \rightarrow |H(e^{j0.3\pi})| \leq 10^{-0.75} = 0.1778 \quad (4)$$

Example (cont'd)

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Example

■ Impulse invariance

- Round up to the next integer of N
- Due to aliasing problem, meet the passband exactly with exceeded stopband

$$1 + \left(\frac{j\frac{0.2\pi}{T}}{j\Omega_c}\right)^{2N} = 10^{0.1} \quad (5)$$

$$1 + \left(\frac{j\frac{0.3\pi}{T}}{j\Omega_c}\right)^{2N} = 10^{1.5} \quad (6)$$

■ Bilinear transformation

- Round up to the next integer of N
- By convention, choose to meet the stopband exactly with exceeded passband

$$1 + \left(\frac{j2 \tan(0.1\pi)}{j\Omega_c}\right)^{2N} = 10^{0.1} \quad (7)$$

$$1 + \left(\frac{j2 \tan(0.15\pi)}{j\Omega_c}\right)^{2N} = 10^{1.5} \quad (8)$$

Example - Comparison

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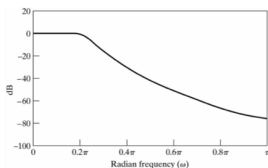
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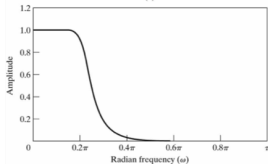
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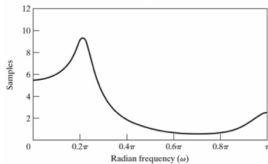
Example



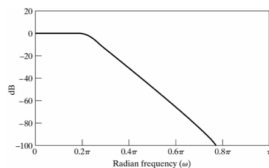
(a)



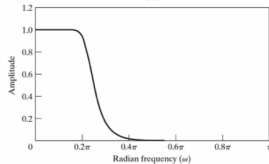
(b)



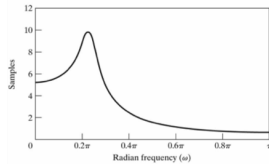
(c)



(a)



(b)



(c)