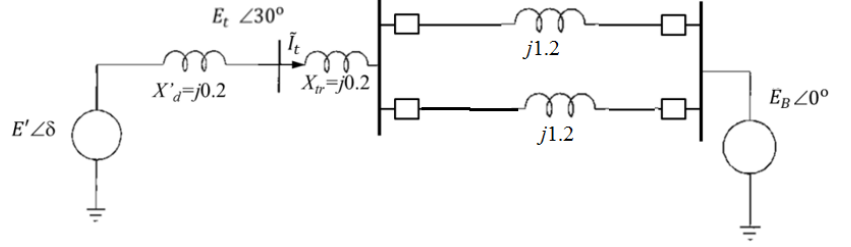


## Homework #7

**1. (50 points)** The circuit model below represents the steady-state operating condition of a single-machine-infinite-bus system.  $E_t = E_B = 1.0$  pu. The generator is represented by the classical model with  $H = 10$  (MWs/MVA) and  $K_D = 3$  (pu torque/pu speed deviation). Consider a small disturbance ended at  $t = 0$ s.

- Write the linearized state equations of the system. Determine the undamped natural frequency ( $\omega_n$ ) of oscillation in both rad/s and Hz, damping ratio ( $\zeta$ ), and damped frequency ( $\omega_d$ ) in both rad/s and Hz.
- Consider a small disturbance of  $\Delta\delta = 10^\circ$  and  $\Delta\omega = 0$  rad/s at  $t = 0$ s. Determine the equations of  $\delta$  and  $\omega$  on the zero-input response of the generator, and plot  $\delta$  (degree) and  $\omega$  (rad/s) for  $t = 0 \sim 10$ s.
- If the input power of the generator is increased by 10% at  $t = 0$ s with  $\Delta\delta = 0^\circ$  and  $\Delta\omega = 0$  rad/s, determine the equations of  $\delta$  and  $\omega$  on the zero-state response of the generator, and plot  $\delta$  (degree) and  $\omega$  (rad/s) for  $t = 0$  to 10s.



**2. (50 points)** Small-signal stability analysis for a 3-machine system:

$$\frac{2H_i}{\omega_0} \ddot{\delta}_i = P_{mi} - E_i'^2 G_{ii} - D_i \frac{\dot{\delta}_i}{\omega_0} - \sum_{\substack{j=1 \\ j \neq i}}^n E_i' E_j' (B_{ij} \sin \delta_{ij} + G_{ij} \cos \delta_{ij})$$

where  $B_{ij}$  and  $G_{ij}$  in pu are respectively elements of the susceptance and conductance matrices:

$$\mathbf{B} = \begin{bmatrix} -2.7 & 1.5 & 1.2 \\ 1.5 & -2.5 & 1.0 \\ 1.2 & 1.0 & -2.2 \end{bmatrix}, \quad \mathbf{G} = \mathbf{0}.$$

The other parameters and data are given in the table:

Parameters	Machine 1	Machine 2	Machine 3
$2H_i$ (s)	50	10	10
$D_i$ (pu)	50	10	10
$P_{mi}$ (pu)	-1.0	0.5	0.5
$E_i'$ (pu)	1.0	1.0	1.0
Steady-state rotor angle $\delta_{i0}$ (deg)	0.90	21.76	23.73

Define  $\delta_{i\Delta} = \delta_i - \delta_{i0}$ ,  $\delta_{ij\Delta} = \delta_{i\Delta} - \delta_{j\Delta}$ . Then, the linearization of the system is obtained as follows:

$$\begin{cases} \dot{\delta}_{i\Delta} = \omega_{ri\Delta} \\ \frac{2H_i}{\omega_0} \dot{\omega}_{ri\Delta} = -\frac{D_i}{\omega_0} \omega_{ri\Delta} - \sum_{\substack{j=1 \\ j \neq i}}^3 K_{sij} (\delta_{i\Delta} - \delta_{j\Delta}) = 0 \quad i = 1, 2, 3 \end{cases} \quad \text{where } K_{sij} = E_i' E_j' (B_{ij} \cos \delta_{ij0} - G_{ij} \sin \delta_{ij0})$$

The matrix representation  $\dot{\mathbf{X}} = \mathbf{A}\mathbf{X}$  of these equations is

$$\frac{d}{dt} \begin{bmatrix} \delta_{1\Delta} \\ \delta_{2\Delta} \\ \delta_{3\Delta} \\ \omega_{1\Delta} \\ \omega_{2\Delta} \\ \omega_{3\Delta} \end{bmatrix} = \begin{bmatrix} & & & 1 & 0 & 0 \\ & \mathbf{0} & & 0 & 1 & 0 \\ & & & 0 & 0 & 1 \\ -\alpha_{11} & -\alpha_{12} & -\alpha_{13} & -\beta_1 & 0 & 0 \\ -\alpha_{21} & -\alpha_{22} & -\alpha_{23} & 0 & -\beta_2 & 0 \\ -\alpha_{31} & -\alpha_{32} & -\alpha_{33} & 0 & 0 & -\beta_3 \end{bmatrix} \begin{bmatrix} \delta_{1\Delta} \\ \delta_{2\Delta} \\ \delta_{3\Delta} \\ \omega_{1\Delta} \\ \omega_{2\Delta} \\ \omega_{3\Delta} \end{bmatrix} \quad \text{where } \alpha_{ii} = \frac{\omega_0}{2H_i} \sum_{\substack{j=1 \\ j \neq i}}^3 K_{sij} \quad \alpha_{ij} = -\frac{\omega_0}{2H_i} K_{sij} \quad \beta_i = \frac{D_i}{2H_i}$$

Matrix  $\mathbf{A}$  as two oscillatory modes (i.e. two pairs of complex eigenvalues) with frequencies in 0.1-3Hz. and two non-oscillatory modes (i.e. real eigenvalues).

- Find the natural frequency and damping ratio of each oscillatory mode.
- For the first three state variables  $\delta_{1\Delta}, \delta_{2\Delta}, \delta_{3\Delta}$  on rotor angles, calculate the mode shape  $\phi_{ki}$ , mode composition  $\psi_{ik}$  and participation factor  $p_{ki} = \psi_{ik}\phi_{ki}$  ( $k=1, 2, 3$ ) for each oscillatory mode  $i$ . The magnitudes of  $\phi_{ki}$ ,  $\psi_{ik}$  and  $p_{ki}$  with each mode  $i$  should be normalized on the basis of the magnitude of the largest one, i.e.

$$\bar{\phi}_{ki} = \frac{\phi_{ki}}{\max\{|\phi_{1i}|, |\phi_{2i}|, |\phi_{3i}|\}}, \quad 0 \leq |\bar{\phi}_{ki}| \leq 1$$

$$\bar{\psi}_{ik} = \frac{\psi_{ik}}{\max\{|\psi_{i1}|, |\psi_{i2}|, |\psi_{i3}|\}}, \quad 0 \leq |\bar{\psi}_{ik}| \leq 1$$

$$\bar{p}_{ki} = \frac{p_{ki}}{\max\{p_{1i}, p_{2i}, p_{3i}\}}, \quad 0 \leq |\bar{p}_{ki}| \leq 1$$

- For each mode, in a polar coordinates charts, draw  $\phi_{1i}, \phi_{2i}, \phi_{3i}$  on  $\delta_{1\Delta}, \delta_{2\Delta}, \delta_{3\Delta}$  to show the mode shape similar to the charts in Slide #25. Do the same also for  $\psi_{ik}$  and for  $p_{ki}$  to show the charts respectively on the mode composition and participation factors with  $\delta_{1\Delta}, \delta_{2\Delta}, \delta_{3\Delta}$ . This requires plots of  $3 \times 2 = 6$  charts which each show phasors corresponding to  $\delta_{1\Delta}, \delta_{2\Delta}, \delta_{3\Delta}$ ,

Hints: In Matlab, eigenvalues and eigenvectors can be solved by `eig(A)`. Each mode has two eigenvalues  $\sigma \pm j\omega$ . Find the right and left eigenvectors of  $\sigma + j\omega$ , whose first three elements respectively give the mode shape and composition regarding  $\delta_{1\Delta}, \delta_{2\Delta}, \delta_{3\Delta}$  for that mode. A polar coordinates chart can be drawn by `polar()` or `polarplot()` in Matlab.