

The Energy Flow Approach for Oscillation Source Location and Damping Evaluation

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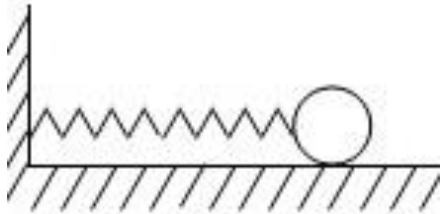
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Background

- **What is oscillation source?** – **cause of oscillation**
 - Disturbance source in forced oscillation
 - Generator with negative damping (often caused by wrong parameters) in free/natural oscillation
- **Why should we find oscillation source?**
 - Online location of oscillation source is the key to **effective measures for oscillation suppression**
 - Remove the disturbance source or adjust the negatively damped generator

Energy Based Idea

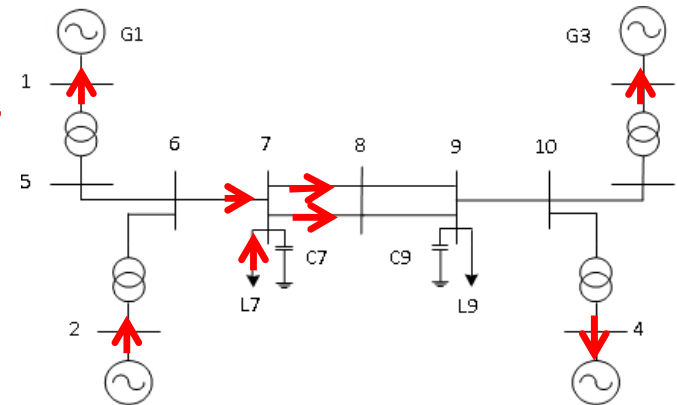
- The concept of energy is widely used in oscillation or vibration analysis
 - Oscillations are accompanied by the conversion of energy
 - Kinetic energy, potential energy
 - The amount of energy is consistent with the oscillation amplitude
 - More energy, larger oscillation amplitude
 - The dissipation of energy brings damping effect
 - Friction



The **component producing energy** is the **oscillation source**, which maintains or increases the oscillation amplitude

Concept of Energy Flow

- Energy in power system dynamics: **Transient energy**
 - The construction of energy function is very difficult
 - Not suitable for online application with measurements
- **Energy flow**
 - Computed with measurements, independent of energy functions
 - The energy dissipation or production can be identified with the energy flow on the network



Energy Flow Computation

- The energy flowing from bus i to branch L_{ij} is [1]

$$\begin{aligned}
 W_{ij} &= \int (I_{ij,x} dU_{i,y} - I_{ij,y} dU_{i,x}) \\
 &= \int (P_{ij} d\theta_i + \frac{Q_{ij}}{U_i} dU_i) = \int (P_{ij} 2\pi\Delta f_i dt + Q_{ij} d(\ln U_i))
 \end{aligned}$$

- Computed with WAMS data and independent of energy functions
- Identical to the transient energy
- The energy flow into an element is composed of two types of terms:
 - conservative term (independent of integral path) - transient energy
 - non-conservative term (dependent of integral path) - energy dissipation

$$\int \text{Im} \left((-I_{Gi})^* dV_i \right) = \left(\frac{1}{2} T_j \omega_0 \omega^2 - P_m \delta \right) \Big|_{x_0}^x + \int D \omega_0 \omega^2 dt$$

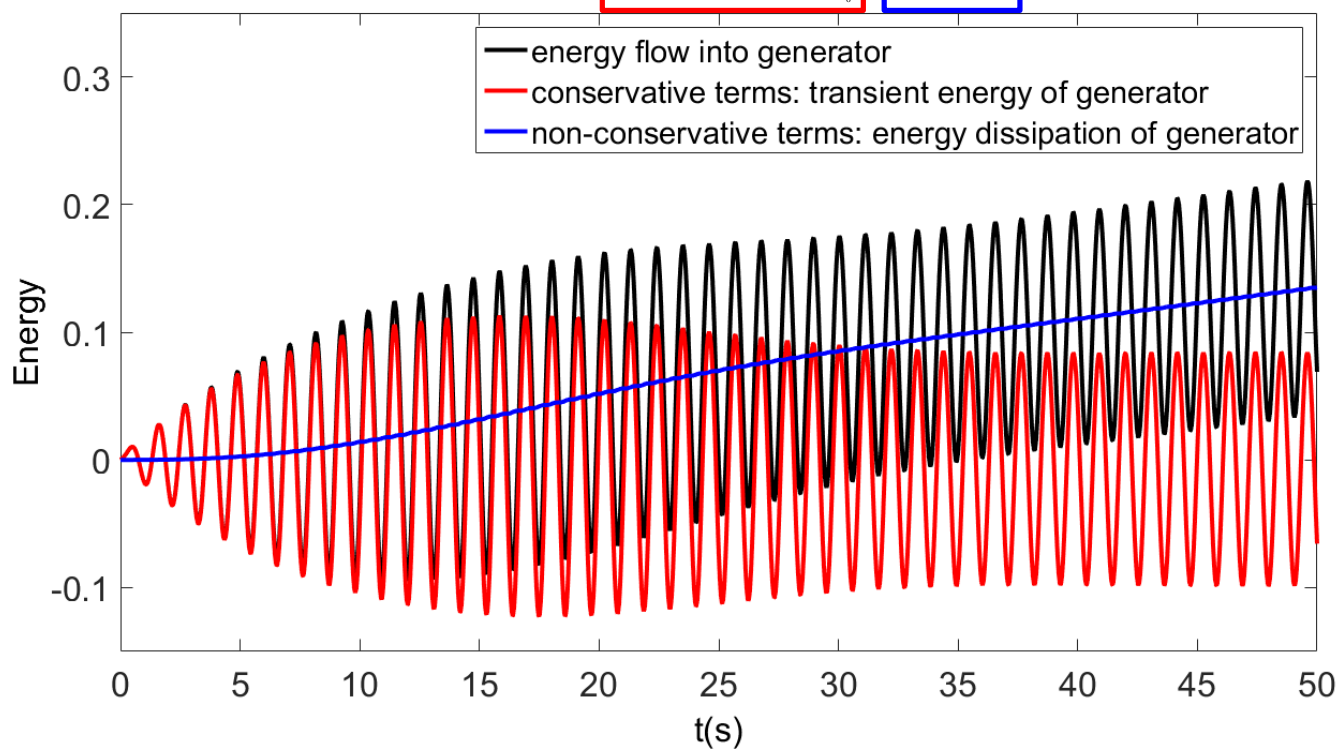


Conservative and Non-Conservative Terms

conservative term - transient energy - oscillating

non-conservative term - energy dissipation – monotonically changing (rising or descending)

$$\int \text{Im} \left((-I_{Gi})^* dV_i \right) = \left(\frac{1}{2} T_J \omega_0 \omega^2 - P_m \delta \right) \Big|_{x_0}^x + \int D \omega_0 \omega^2 dt$$

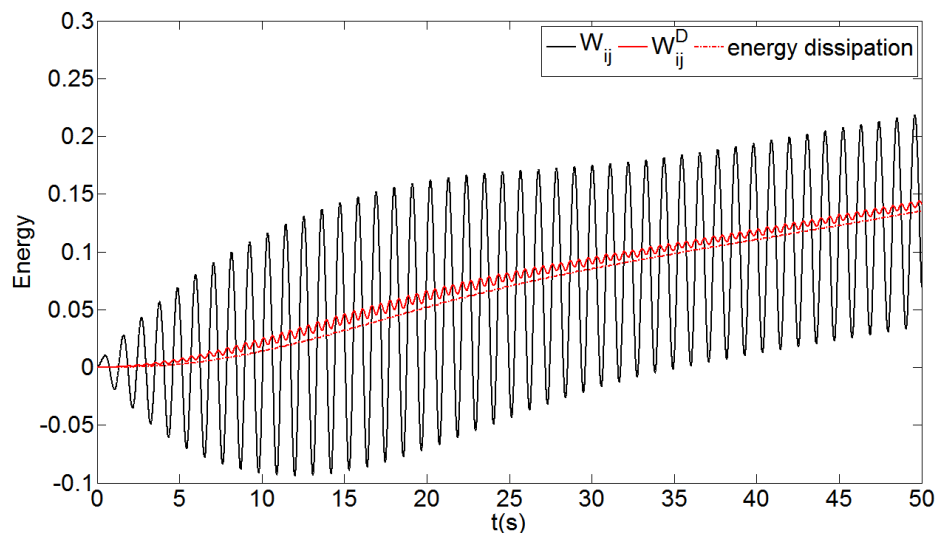


Energy Dissipation or Production

- The energy dissipation/production can be extracted from the energy flow, which reflects the damping of a component in low frequency oscillation
- **Net Energy Flow / Dissipating Energy Flow**

$$\begin{aligned}
 W_{ij}^D &= \int (\Delta P_{ij} d\Delta \theta_i + \Delta Q_{ij} d(\Delta \ln U_i)) \\
 &= \int (\Delta P_{ij} 2\pi \Delta f_i dt + \Delta Q_{ij} d(\Delta \ln U_i))
 \end{aligned}$$

- Computed with deviations
- Reserve non-conservative terms but eliminate conservative terms



Energy flow into a generator that dissipates transient energy and has positive damping

Energy Dissipation Corresponds to Positive Damping

- Energy dissipation is consistent with damping torque of a generator
 - Mathematically proved: in Heffron-Phillips model, actual energy dissipation in a period equals the energy dissipated by the damping torque

$$\frac{T_{d0}'}{X_d - X_d'} \int_t^{t+\frac{2\pi}{\omega_d}} (\dot{E}_q')^2 dt = K_D \omega_0 \int_t^{t+\frac{2\pi}{\omega_d}} \omega^2 dt$$

- Damping torque can be evaluated with energy dissipation

Test
results

Case	Oscillation Type	DTA	Energy Dissipation	Relative Error(%)	
No AVR	Free	1.9037	1.9070	0.17	
	Forced	1.9037	1.8990	-0.25	
AVR, no PSS	a	Free	1.2446	1.2519	0.59
		Forced	1.2446	1.2333	-0.91
	b	Free	-1.1747	-1.1784	0.31
		Forced	-	-	-
AVR, PSS	Free	1.6989	1.7572	3.43	
	Forced	1.6989	1.6218	-4.54	

Energy Dissipation in Detailed Generator Model

Generator with a field winding and 3 damper windings

$$\begin{aligned}\dot{\delta} &= \omega_0 \omega \\ T_J \dot{\omega} &= P_m - P_e - D \omega \\ \dot{\psi}_{fd} &= U_{fd} - R_{fd} I_{fd} \\ \dot{\psi}_{1d} &= -R_{1d} I_{1d} \\ \dot{\psi}_{1q} &= -R_{1q} I_{1q} \\ \dot{\psi}_{2q} &= -R_{2q} I_{2q}\end{aligned}$$

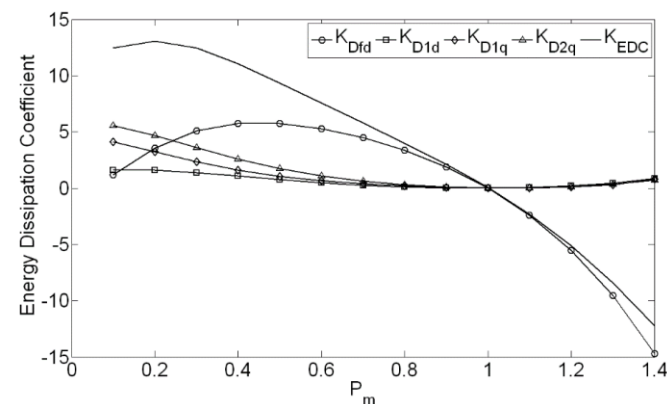
Conservative terms

$$\begin{aligned}& -P_m \delta + \frac{1}{2} T_J \omega_0 \omega^2 \\ & + \frac{1}{2} \left(X_d - \frac{X_{ad}^2 (X_{11d} + X_{ffd} - 2X_{ad})}{X_{ffd} X_{11d} - X_{ad}^2} \right) I_d^2 \\ & + \frac{1}{X_{ffd} X_{11d} - X_{ad}^2} \left(\frac{X_{11d} \psi_{fd}^2}{2} + \frac{X_{ffd} \psi_{1d}^2}{2} - X_{ad} \psi_{fd} \psi_{1d} \right) \\ & + \frac{1}{2} \left(X_q - \frac{X_{aq}^2 (X_{11q} + X_{22q} - 2X_{aq})}{X_{11q} X_{22q} - X_{aq}^2} \right) I_q^2 \\ & + \frac{1}{X_{11q} X_{22q} - X_{aq}^2} \left(\frac{X_{22q} \psi_{1q}^2}{2} + \frac{X_{11q} \psi_{2q}^2}{2} - X_{aq} \psi_{1q} \psi_{2q} \right)\end{aligned}$$

Non-conservative terms

$$\begin{aligned}W_D &= D \omega_0 \int \omega^2 dt \\ W_{fd} &= \int -(U_{fd} I_{fd} - I_{fd}^2 R_{fd}) dt \\ W_{1d} &= \int I_{1d}^2 R_{1d} dt \\ W_{1q} &= \int I_{1q}^2 R_{1q} dt \\ W_{2q} &= \int I_{2q}^2 R_{2q} dt\end{aligned}$$

Energy dissipations of windings : damping [2]



Energy dissipation coefficients as Pm changes



Energy Production of Disturbance Source in Forced Oscillation

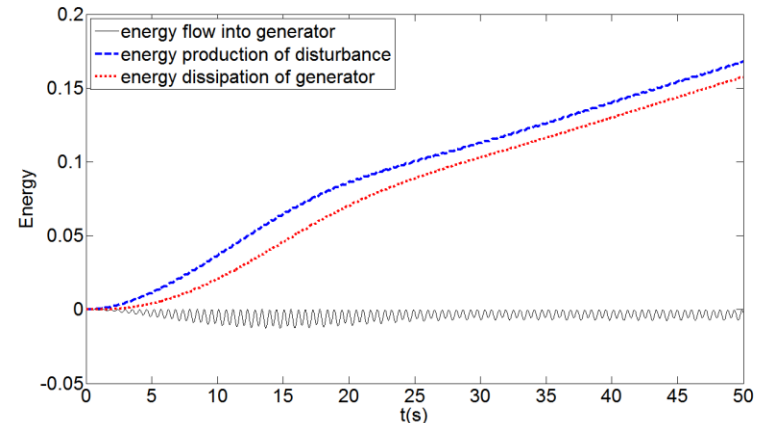
- The disturbance source in forced oscillation produces

Periodic disturbance on
mechanical power

$$P_m' = P_m + P_d \sin(\omega_d t)$$

Energy production of
disturbance

$$\int (P_d \sin(\omega_d t) \omega_0 \omega) dt$$

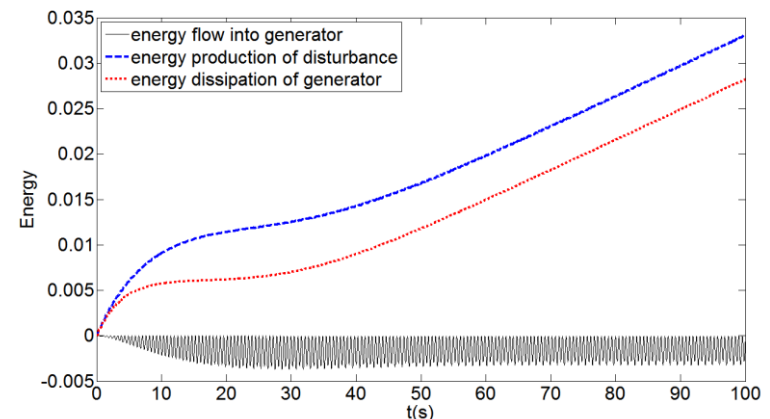


Periodic disturbance on
field voltage

$$E_{fd}' = E_{fd} + E_d \sin(\omega_d t)$$

Energy production of
disturbance

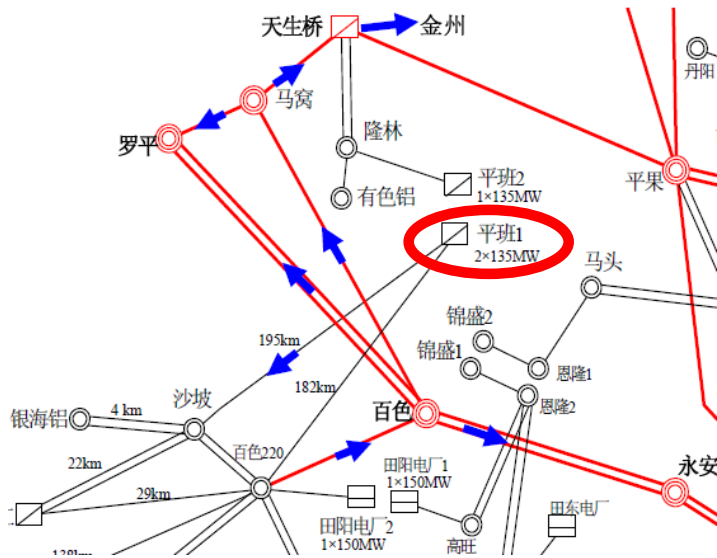
$$\frac{1}{X_d - X_d'} \int (E_d \sin(\omega_d t) \dot{E}_q') dt$$



Online Oscillation Source Location

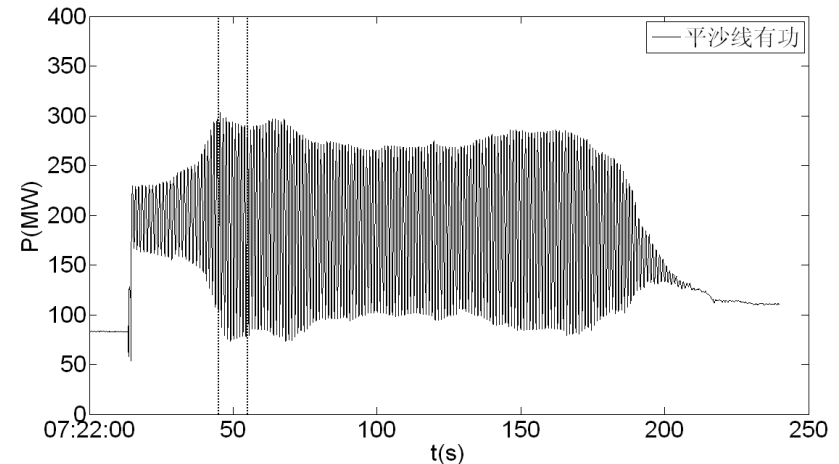
- PMU/WAMS based
 - Used data: **P, Q, U, f**
- Steps
 - When the oscillation is detected, compute the **energy flow** in the network using a short period (often less than 10s) of data with $W_{ij}^D = \int (\Delta P_{ij} 2\pi\Delta f_i dt + \Delta Q_{ij} d(\Delta \ln U_i))$
 - Compute the slope of W_{ij}^D using linear fitting, which reflects the **power of the energy flow**
 - Find the **energy source** using **the direction and the magnitude of the energy flow power**, and it is the **oscillation source**

Actual Oscillation Incidents Analysis

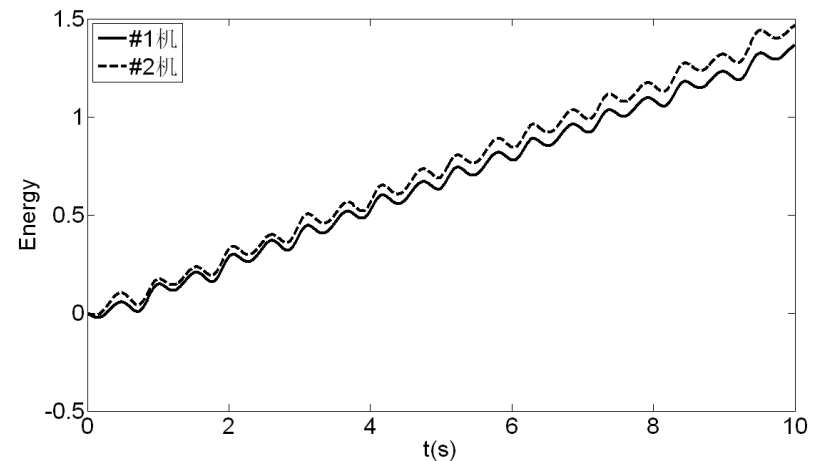


Pingban plant oscillation - 0.94Hz

- Caused by the **trip of one sending line** Pingban-Baise
- Negatively damped **free oscillation**
- The generators in Pingban are **producing energy**

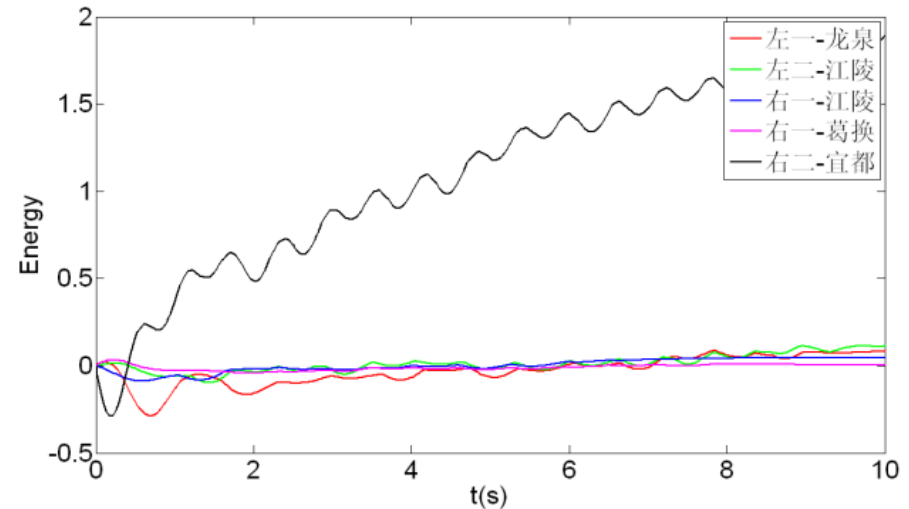
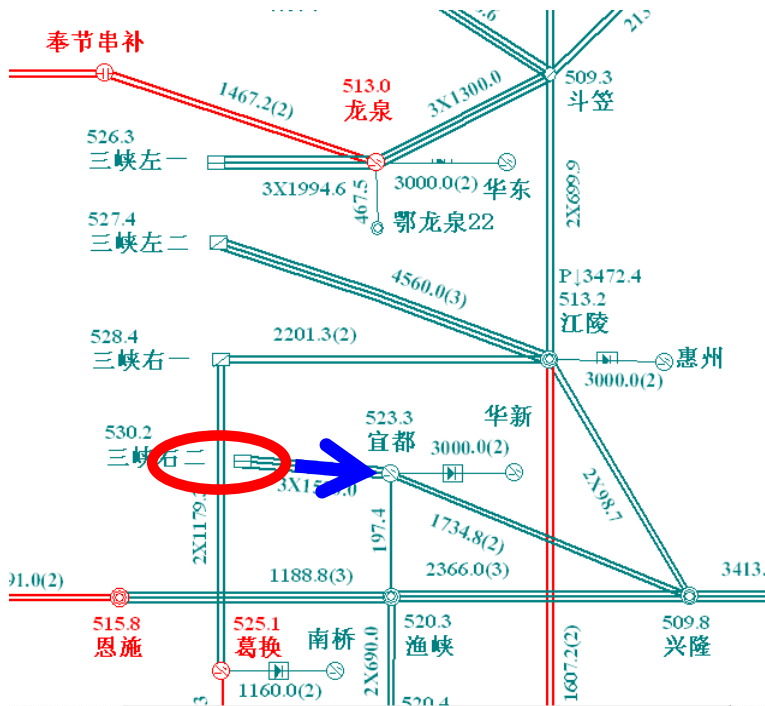


P of line Pingban-Shapo



Energy flow from Pingban generators to the system

Actual Oscillation Incidents Analysis

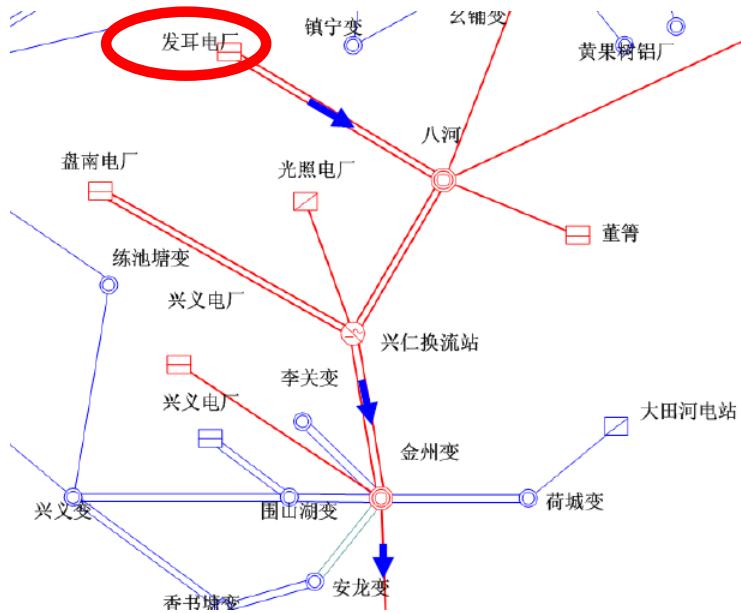


Energy flow from different plants to the system

Three gorges station oscillation - 0.82Hz

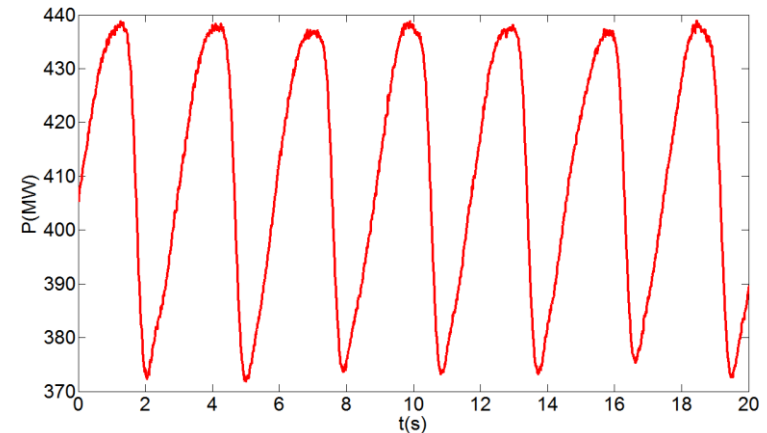
- Caused by **wrong PSS parameters** in Youer plant
- Nearly zero damped **free oscillation**
- The Youer plant is producing energy

Actual Oscillation Incidents Analysis

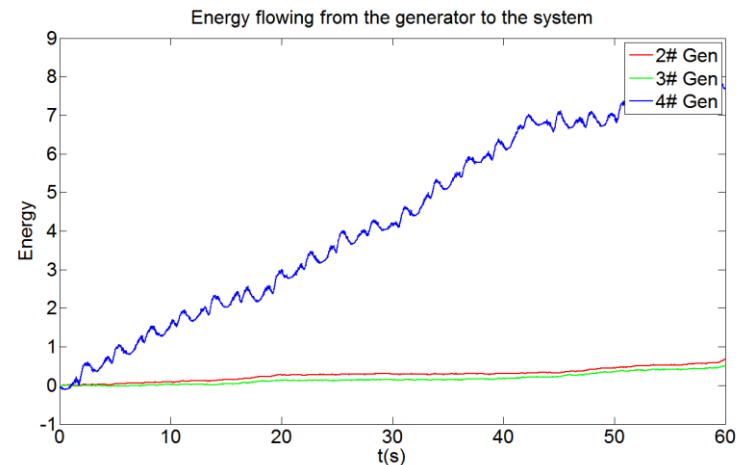


Faer plant oscillation - 0.30Hz

- Caused by **governor fault** in gen #4 of Faer plant, which induces power oscillation of the generator
- **Forced oscillation**
- **Gen #4 is producing energy**



P of line gen #4



Energy flow from generators to the system

Online System Implementation

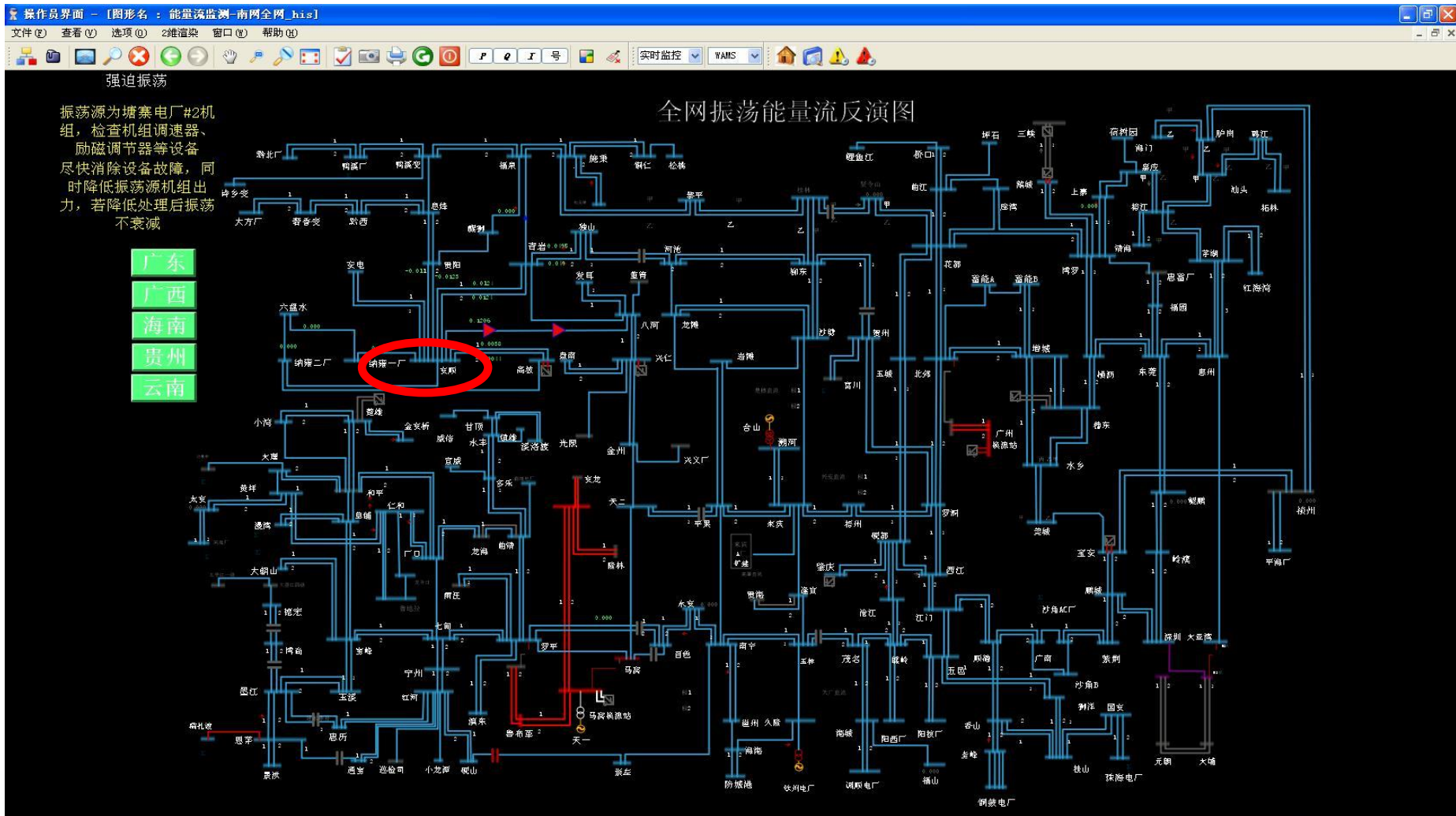
- Based on PMU/WAMS in **China Southern Grid**
- **Successfully locate oscillation sources in many incidents since its commissioning in 2013**



Main interface

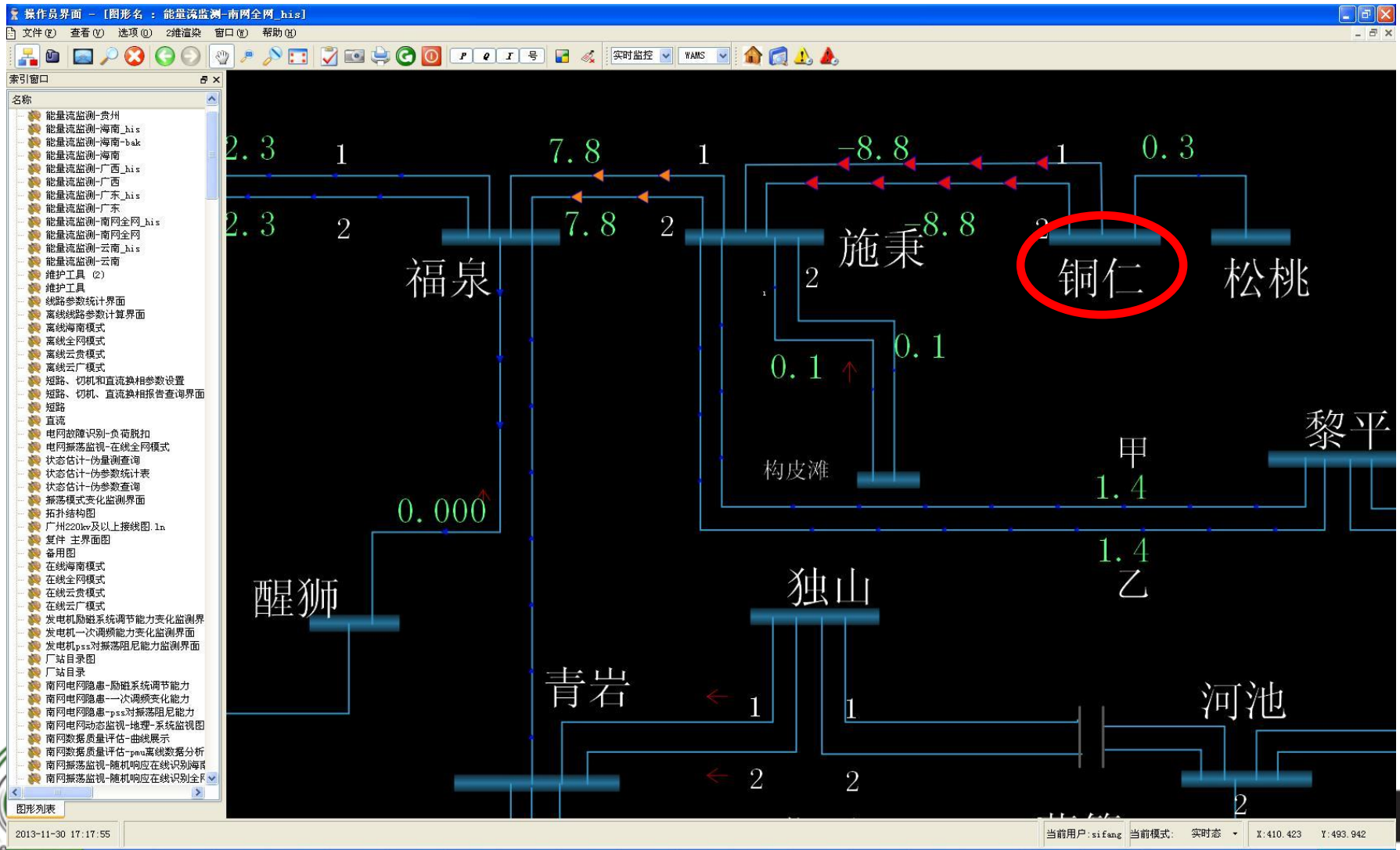
Online System Implementation

When oscillation detected



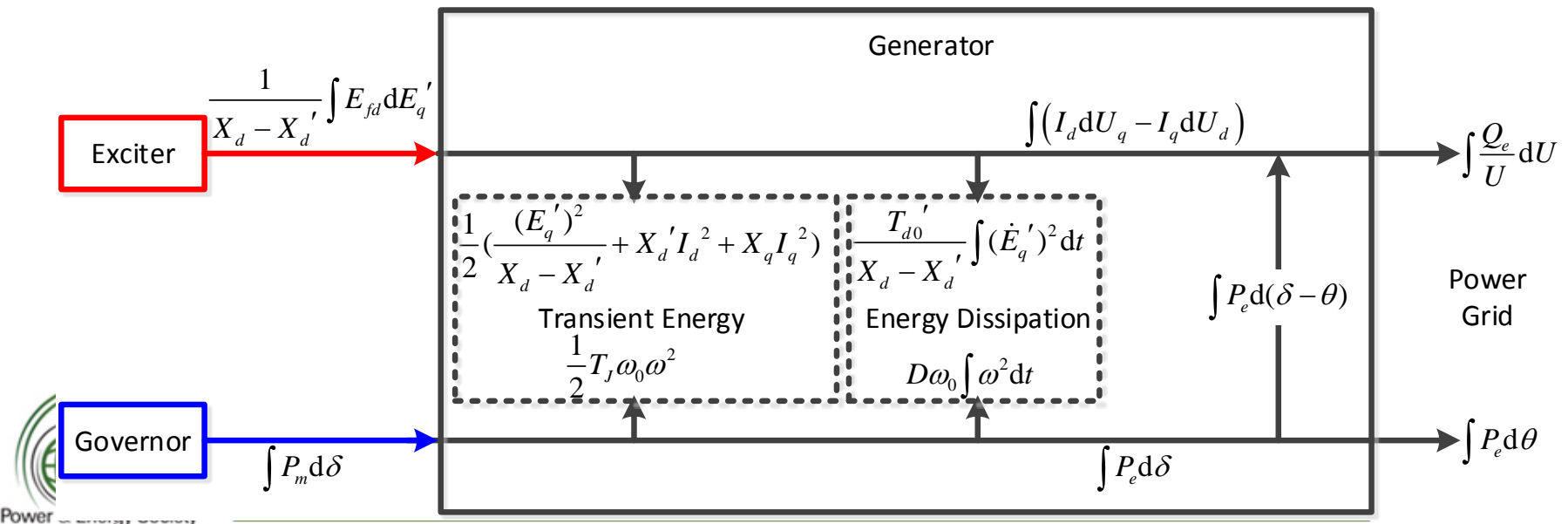
Online System Implementation

When oscillation detected



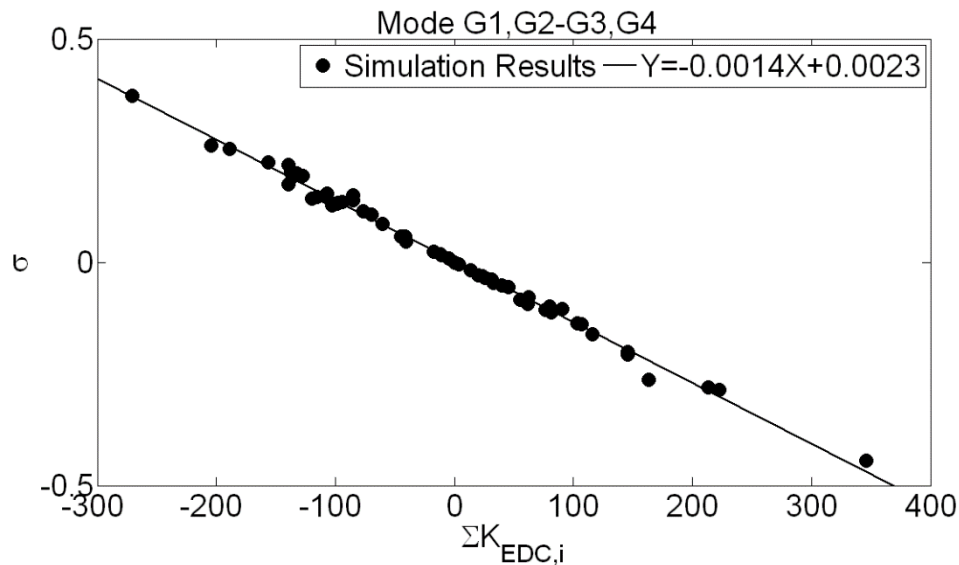
Other Applications

- Also implemented in [Center China Grid Company](#)
- Successfully used in China [Xinjiang](#) and [Xizang](#) Grids for oscillation incident analysis
- Through the energy flow inside the generator, **the oscillation source can be further located at exciter or governor**, which is helpful for cause analysis and defect correction



Connection with Modal/Eigen Analysis

- The **energy dissipation** is connected with **damping ratio** in modal analysis [3]



$$\sigma = -\gamma \sum_i K_{EDC,i}$$

σ : real-part of eigenvalue
 $K_{EDC,i}$: energy dissipation coefficient of generator

The damping of the whole system of a mode comes from the total energy dissipations of generators



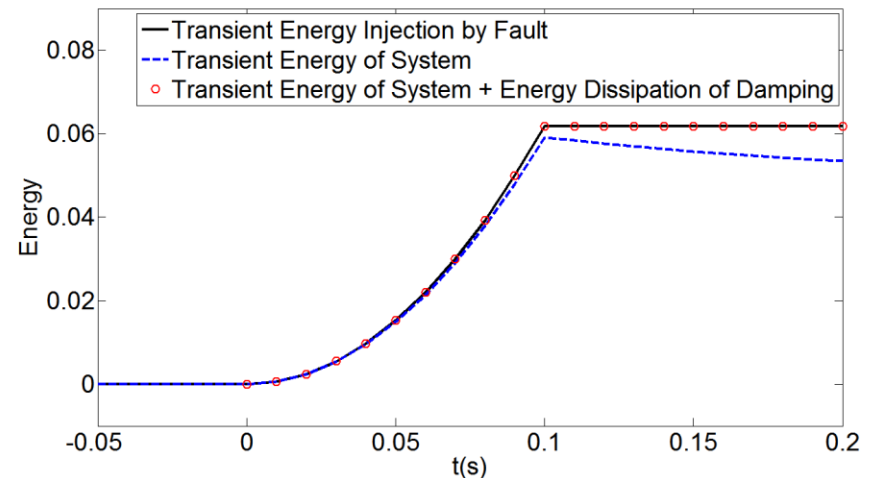
Discussions on New Developments

- **Physical meaning** of oscillation energy flow
 - Connection with the actual electrical power
- Application in **transient stability**
 - The **transient energy injection** of a fault can be computed through **the energy flow at the fault point with the voltages and the currents**
 - Energy function is not needed
 - Transient stability may be studied through the energy flow on the network

$$W_{1d} = \int \underline{I_{1d}^2 R_{1d}} dt$$

$$W_{1q} = \int \underline{I_{1q}^2 R_{1q}} dt$$

$$W_{2q} = \int \underline{I_{2q}^2 R_{2q}} dt$$



Thanks!

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