

ECE 301
Transients

Second Order Systems

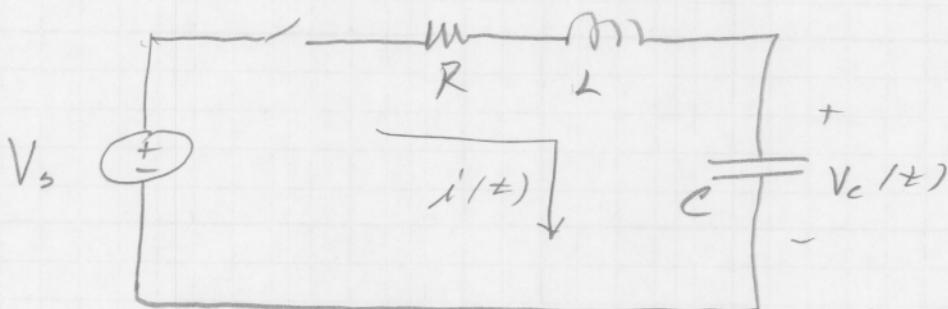
Circuits with series or parallel RLC result in a 2nd order differential equation of the form

$$\frac{d^2x}{dt^2} + a \frac{dx}{dt} + b x(t) = f(t)$$

Since we are assuming a constant source, $f(t) = \text{constant}$.

To better illustrate this consider the

Series RLC



We can write

$$Ri(t) + L \frac{di}{dt} + V_c(t) = V_s \quad (1)$$

The next step depends on whether we want a solution for $V_c(t)$, or $i(t)$. Let us go for $V_c(t)$ first.

In Eq (1) we use

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$$i = C \frac{dV_c}{dt}$$

to obtain

$$RC \frac{dV_c}{dt} + LC \frac{d^2 V_c}{dt^2} + V_c(0) = V_s$$

or

$$\frac{d^2 V_c}{dt^2} + \frac{R}{L} \frac{dV_c}{dt} + \frac{V_c(0)}{LC} = \frac{V_s}{LC} \quad (2)$$

If we want a solution in $i(t)$
we can use

$$Ri(t) + \frac{L di}{dt} + \frac{1}{C} \int_0^t i dt + V_c(0) = V_s \quad (3)$$

Taking the derivative wrt t gives

$$R \frac{di}{dt} + L \frac{d^2 i}{dt^2} + \frac{i(t)}{C} = 0$$

or

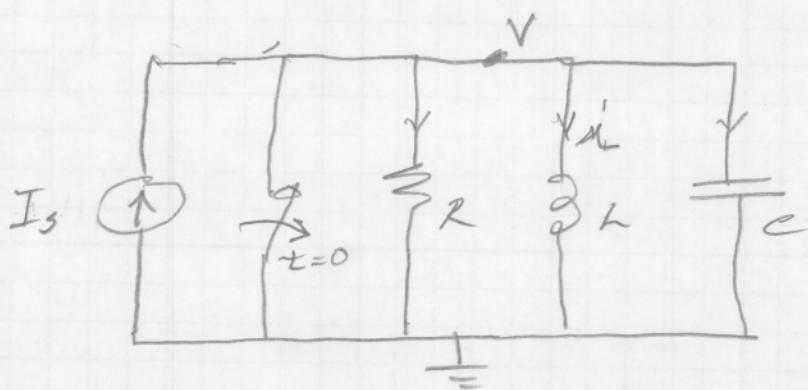
$$\frac{d^2 i}{dt^2} + \frac{R}{L} \frac{di}{dt} + \frac{i(t)}{RC} = 0 \quad (4)$$

Notice that characteristic equation
is the same for both (2) and (4)
and this is expected. The C.E. is

$$\boxed{s^2 + \frac{R}{L}s + \frac{1}{RC} = 0} \quad (5)$$

Now consider the parallel RLC

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Using nodal equations,

$$\frac{V}{R} + C \frac{\partial V}{\partial t} + \lambda = I_S \quad (6)$$

If we want a solution in $i_L(t)$, we use

$$V(t) = L \frac{di}{dt}$$

and substitute into Eq. (6):

$$\frac{L}{R} \frac{di}{dt} + LC \frac{\partial^2 i}{\partial t^2} + \lambda(t) = I_S$$

$$\frac{\partial^2 i}{\partial t^2} + \frac{1}{RC} \frac{di}{dt} + \frac{\lambda(t)}{LC} = \frac{I_S}{LC} \quad (7)$$

The C.E. is

$$s^2 + \frac{1}{RC} s + \frac{1}{LC} = 0 \quad (8)$$

If we want a solution in $V(t)$ we use

$$i = \frac{1}{L} \int_0^t V(t) dt + i(0) \quad (9)$$

Substitute Eq 19 into Eq 16

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$$\frac{V}{R} + C \frac{dV}{dt} + \frac{1}{L} \int V(z) dz + i(t) = I_s$$

Take the derivative of the above w.r.t t to find

$$\frac{1}{R} \frac{dV}{dt} + C \frac{d^2 V}{dt^2} + \frac{V(t)}{L} = 0$$

and then

$$\frac{d^2 V}{dt^2} + \frac{1}{RC} \frac{dV}{dt} + \frac{V(t)}{LC} = 0 \quad (10)$$

The characteristic equation is

$$s^2 + \frac{1}{RC}s + \frac{1}{LC} = 0 \quad (11)$$

Note that Eq 11) and Eq 8) are the same.

In the final analysis we need to solve a diff. eq. of the form

$$\frac{d^2 x}{dt^2} + A \frac{dx}{dt} + B x(t) = C \quad (12)$$

or

$$\frac{d^2 x}{dt^2} + D \frac{dx}{dt} + E x(t) = 0 \quad (13)$$

As the most general case let us use Eq (12). Also, for help in explaining things let us use a special form of

$$\frac{d^2x}{dt^2} + 2\zeta\omega_n \frac{dx}{dt} + \omega_n^2 x(t) = C \quad (14)$$

where

$$2\zeta\omega_n = A$$

$$\omega_n^2 = B$$

ω_n is called the undamped natural resonant frequency

ζ is called the damping coefficient.

The general solution of (14) is

$$x(t) = x_p(t) + x_c(t)$$

where

$$x_p(t) = \frac{C}{B} \quad (15)$$

(refer back to Eq (12)).

$x_p(t)$ is the particular solution.

The complementary solution will be of the form

$$x_c(t) = A_1 e^{s_1 t} + A_2 e^{s_2 t}$$

where s_1 and s_2 are the roots of the characteristic equation. The characteristic equation is

$$s^2 + 2\zeta\omega_n s + \omega_n^2 = 0$$

From the quadratic equation we know

$$s_1 = \frac{-2\zeta\omega_n + \sqrt{(2\zeta\omega_n)^2 - 4\omega_n^2}}{2}$$

$$s_1 = -\zeta\omega_n + \omega_n \sqrt{\zeta^2 - 1} \quad (16)$$

and

$$s_2 = -\zeta\omega_n - \omega_n \sqrt{\zeta^2 - 1} \quad (17)$$

There are 3 cases to consider for these roots:

CASE 1: $\zeta > 1$

This is the case of overdamping. We have two real and distinct roots; our solution is

$$x(t) = \frac{C}{B} + k_1 e^{s_1 t} + k_2 e^{s_2 t} \quad (18)$$

We will need to know

$x(0)$ and $\frac{dx(0)}{dt}$ in order to

solve for k_1 and k_2 .

CASE 2; $\xi = 1$

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This is called critical damping.
FOR this case

$$s_1 = s_2 = -\xi \omega_n$$

and

$$x(t) = \frac{C}{R} + (k_1 + 2k_2)e^{s_1 t} \quad (15)$$

Again, we must know two I.C.
to solve for k_1 and k_2 . Namely

$$x(0), \quad \frac{dx(0)}{dt}$$

CASE 3; $\xi < 1$

This is the case of underdamping

For

$$s = -\xi \omega_n \pm j \omega_n \sqrt{\xi^2 - 1}$$

we write

$$s = -\xi \omega_n \pm j \omega_n \sqrt{1 - \xi^2}$$

$$s_1 = -\xi \omega_n + j \omega_d; \quad s_2 = -\xi \omega_n - j \omega_d$$

$$\omega_d = \omega_n \sqrt{1 - \xi^2}$$

ω_d is called the damped natural
resonant frequency.

We write

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$$\begin{aligned}x(t) &= \frac{C}{B} + k_1 e^{-(\xi w_n + j w_d)t} + k_2 e^{-(\xi w_n - j w_d)t} \\&= \frac{C}{B} + k_1 e^{-\xi w_n t} e^{-j w_d t} + k_2 e^{-\xi w_n t} e^{j w_d t} \\&= \frac{C}{B} + e^{-\xi w_n t} [k_2 e^{j w_d t} + k_1 e^{-j w_d t}] \\&= \frac{C}{B} + e^{-\xi w_n t} [k_2 (\cos w_d t + j \sin w_d t) \\&\quad + k_1 (\cos w_d t - j \sin w_d t)]\end{aligned}$$

collecting terms

$$x(t) = \frac{C}{B} + e^{-\xi w_n t} [(k_1 + k_2) \cos w_d t + j(k_2 - k_1) \sin w_d t]$$

or

$$x(t) = \frac{C}{B} + e^{-\xi w_n t} [A_1 \cos w_d t + A_2 \sin w_d t]$$

We find A_1 and A_2 using initial conditions;

$$x(0), \frac{dx(0)}{dt}$$

Next for illustrations