Circuits II

Prof. Daniel Costinett

ECE 202 Lecture 42
April 24, 2020

THE UNIVERSITY OF TENNESSEE KNOXVILLE

Announcements

- TNvoice evaluations
  - 5 points EC on final if we get 100% participation
  - 67%, currently; deadline Monday 4/27

Final Exam

- One-week, take-home exam
  - Same format/restrictions as Midterm 2
    - Open-book, open-course-website, no other online resources
    - No collaboration
    - MATLAB, LTSpice, or other computer tools can be used but will receive no credit unless otherwise stated
- Cumulative, covering entire course content
- Exam password e-mailed out April 27th before midnight
- Exam due to canvas before **midnight, May 4th**

Course Content

- Magnetically Coupled Circuits (Ch 13)
- Sinusoidal Steady-State Analysis (Ch 10)
- AC Circuit Power Analysis (Ch 11)
- Circuit An Analysis in the s-Domain (Ch 14)
- Frequency Response (Ch 15)
- Fourier Circuit Analysis (Ch 17)
- Polyphase Circuits (Ch 12)
- Two-Port Networks (Ch 16)

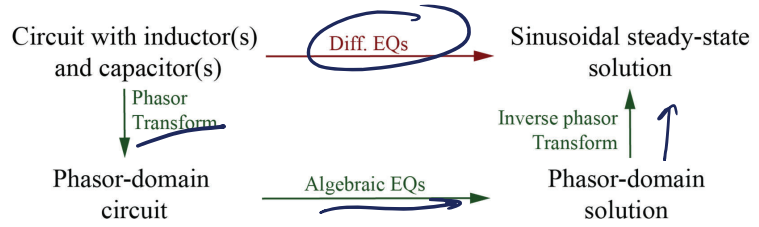
Slido: #Q711

THE UNIVERSITY OF TENNESSEE KNOXVILLE

Transform Domains

Phasor Transform

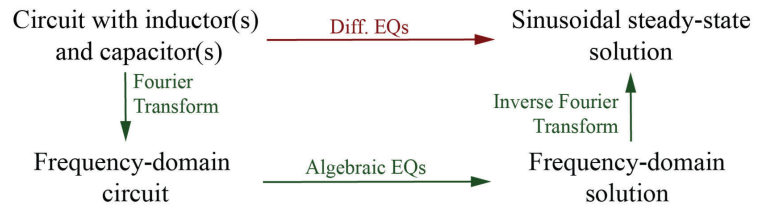
$$u(t) = A\cos(\omega_0 t + \varphi)$$



ω is variable

Fourier Transform

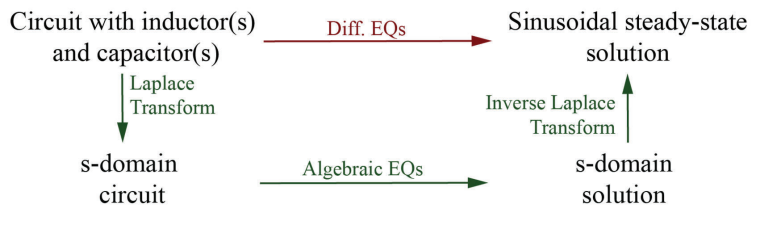
$$u(t) = \sum C_n \cos(n\omega_0 t + \varphi_n)$$



$s = j\omega$

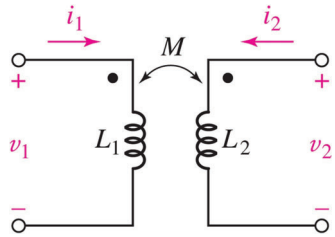
Laplace Transform

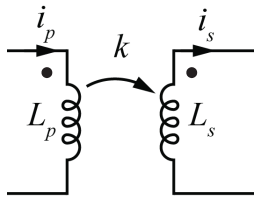
$$u(t) = \sum K_n e^{s_n t}$$



Ch 13 – Magnetically Coupled Circuits

Coupled Inductors





Defining Equations

$$v_1(t) = L_1 \frac{di_1}{dt} + M \frac{di_2}{dt}$$

$$v_2(t) = M \frac{di_1}{dt} + L_2 \frac{di_2}{dt}$$

Coupling Coefficient

$$k = \frac{M}{\sqrt{L_p L_s}}$$

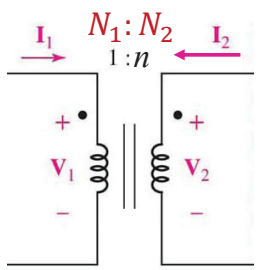
Dot convention

- Current into the dot on one terminal produces a positive open circuit voltage w.r.t. the dot on the other

Recall

- Equivalent circuits

Ideal Transformer



Defining Equations

$$\frac{V_1}{N_1} = \frac{V_2}{N_2} = \cdots$$

$$0 = N_1 I_1 + N_2 I_2 + \cdots$$

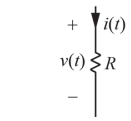
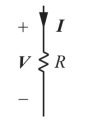
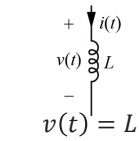
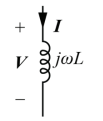
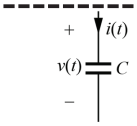
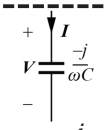
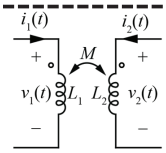
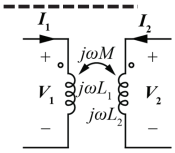
Coupled inductors with:

- no energy storage (L→ ∞)
- Perfect coupling (*k=1*)

Recall

- Z/V/I reflection

Ch 10 – Sinusoidal Steady State

Time Domain	Phasor Domain
	
$v(t) = i(t)R$	$\boldsymbol{V} = \boldsymbol{I}R$
	
$v(t) = L\dfrac{di}{dt}$	$\boldsymbol{V} = j\omega L\boldsymbol{I}$
	
$i(t) = C\dfrac{dv}{dt}$	$\boldsymbol{V} = \dfrac{-j}{\omega C}\boldsymbol{I}$
	
$v_1(t) = L_1\dfrac{di_1}{dt} + M\dfrac{di_2}{dt}$ $v_2(t) = M\dfrac{di_1}{dt} + L_2\dfrac{di_2}{dt}$	$\boldsymbol{V}_1 = j\omega L_1\boldsymbol{I}_1 + j\omega M\boldsymbol{I}_2$ $\boldsymbol{V}_2 = j\omega M\boldsymbol{I}_1 + j\omega L_2\boldsymbol{I}_2$

Phasor Notation

$$A\cos(\omega t + \varphi) \Leftrightarrow A\measuredangle\varphi$$

$$= Re\{Ae^{j(\omega t+\varphi)}\}$$

$$= Re\{A\cos(\omega t + \varphi) + jA\sin(\omega t + \varphi)\}$$

Impedance and Admittance

$$Z = R + jX$$

Impedance Resistance Reactance

$$Y = \frac{1}{Z} = G + jB$$

Admittance Conductance Susceptance

Circuit Analysis

- Real circuits always have all real signals in the time domain
- All 201 analysis techniques apply
- Gives only forced/steady-state/particular response, for single sinusoidal source
- Phasor superposition

Slido: #Q711

Ch 11 – AC Power Analysis

Average (DC) Power: $P = \lim_{T\to\infty}\frac{1}{T}\int_{-\infty}^{\infty} p(t)dt$

For periodic signals: $P = \int_{t_0}^{t_0+T} p(t)dt$

Average power in a resistor: $P_R = \left[\underbrace{\sqrt{\int i(t)^2 dt}}_{I_{rms} = I_{eff}}\right]^2 R$

For sinusoids: $I_{rms} = \dfrac{I_A}{\sqrt{2}}$

Sinusoidial Power

$$p(t) = [V_A\cos(\omega t + \varphi_V)][I_A\cos(\omega t + \varphi_I)]$$

$$= \underbrace{\frac{V_A I_A}{2}\cos(2\omega t + \varphi_V + \varphi_I)}_{\text{Double-frequency}} + \underbrace{\frac{V_A I_A}{2}\cos(\varphi_V - \varphi_I)}_{\text{DC = average}}$$

$$\frac{V_A I_A}{2} = V_{rms}I_{rms}$$

Complex Power

$$S = \frac{\boldsymbol{V}\boldsymbol{I}^*}{2} = \boldsymbol{V}_{rms}\boldsymbol{I}_{rms}$$

$$S = P + jQ$$

Complex [VA] Real/Avg [W] Reactive/Quad. [VAR]

Apparent Power: $|S| = \dfrac{V_A I_A}{2} = V_{rms}I_{rms}$

Power Factor: $PF = \dfrac{P}{|S|}$ (leading/lagging)

Impedance match for max power transfer: $Z_L = Z_{th}{}^*$

Slido: #Q711

Ch 14 – Laplace Transform

Unilateral Laplace Transform: $F(s) = \mathcal{L}\{f(t)\} = \int_{0^-}^{\infty} e^{-st} f(t)dt$

Inverse Laplace Transform: $f(t) = \mathcal{L}^{-1}\{F(s)\} = \frac{1}{2\pi j}\int_{\sigma_0 - j\infty}^{\sigma_0 + j\infty} e^{st}F(s)ds$, σ_0 in ROC (to the right of all poles in complex plane)

Complex frequency = Laplace variable = $s = \sigma + j\omega$

Laplace transform is a **linear transformation**. Other properties and transforms in tables

Inverse Transforms: *Long Division* → *Factor* → *PFE* → *Tables*

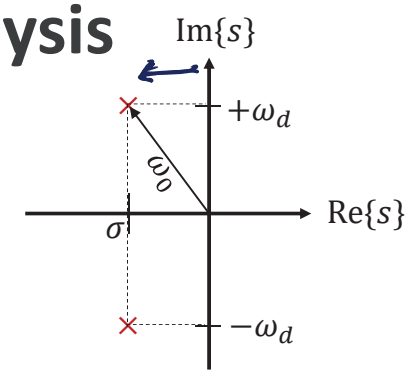
if order num ≥ order den

PFE Special cases:

Repeated: $\frac{N(s)}{(s+5)^2} = \frac{k_1}{s+5} + \frac{k_2}{(s+5)^2}$ (Differentiation or coefficient matching)

Complex: $\frac{N(s)}{s^2+4} = \frac{k_1 s + k_2}{s^2+4} = \frac{k_1}{s-j2} + \frac{k_1^*}{s+j2}$

Ch 14 – Laplace Circuit Analysis



Poles and Zeros:

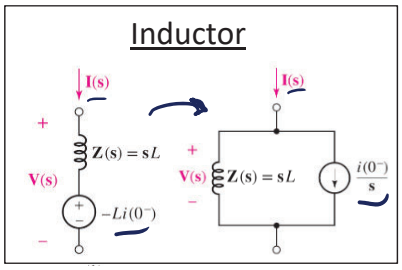
$F(s) = \frac{N(s)}{D(s)}$

Zeros: roots of $N(s)$

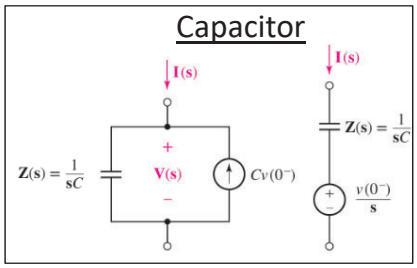
Poles: roots of $D(s)$

Circuit Transformation:

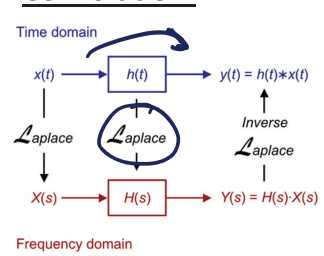
Inductor



Capacitor



Convolution:



impulse response

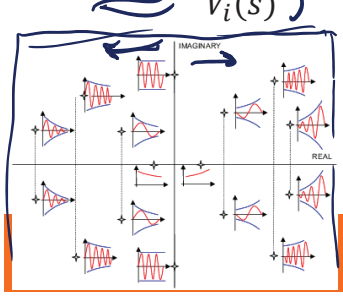
$$v_o(t) = v_i(t) * h(t) = \int_{-\infty}^{\infty} v_i(t-\tau)h(\tau)d\tau$$

Transfer Functions:

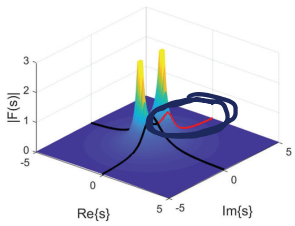
$H(s) = \frac{V_o(s)}{V_i(s)}$

Poles of $H(s)$ define "form" of terms in natural response of the circuit

Poles of $V_i(s)$ define "form" of terms in forced response of the circuit



Ch 15 – Frequency Response



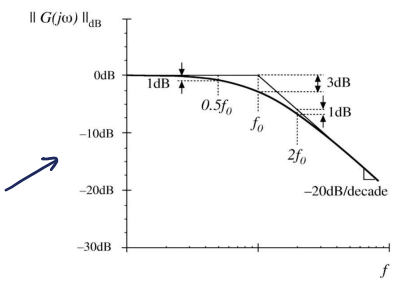
Frequency Response: $H(s \to j\omega)$

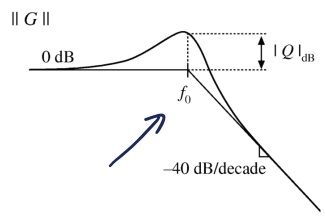
- Circuit response to sinusoidal inputs
- Valid if all poles in LHP

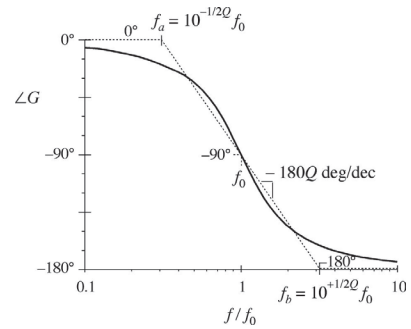
Bode plot: mag-phase plots on log-log axes

- $\|H(j\omega)\|_{dB} = 20\log(|H(j\omega)|)$
- $\measuredangle H(j\omega)$

Templates and Approximations:



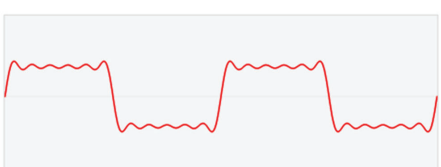




Filter Design

- Bandwidth, graphical analysis, Chebyshev and Butterworth, Sallen-Key Amplifier
- Resonant circuits

Ch 17 – Fourier Series and Transform



https://en.wikipedia.org/wiki/Fourier_transform

Fourier Series:

For periodic $f(t)$ with period $T_0 = \frac{2\pi}{\omega_0}$

$$f(t) = a_0 + \sum_{k=1}^{\infty} a_k \cos(k\omega_0 t) + b_k \sin(k\omega_0 t)$$

$$a_k = \frac{2}{T_0}\int_{t_0}^{t_0+T_0} f(t)\cos(k\omega_0 t)\,dt$$

$$b_k = \frac{2}{T_0}\int_{t_0}^{t_0+T_0} f(t)\sin(k\omega_0 t)\,dt$$

Fourier Transform:

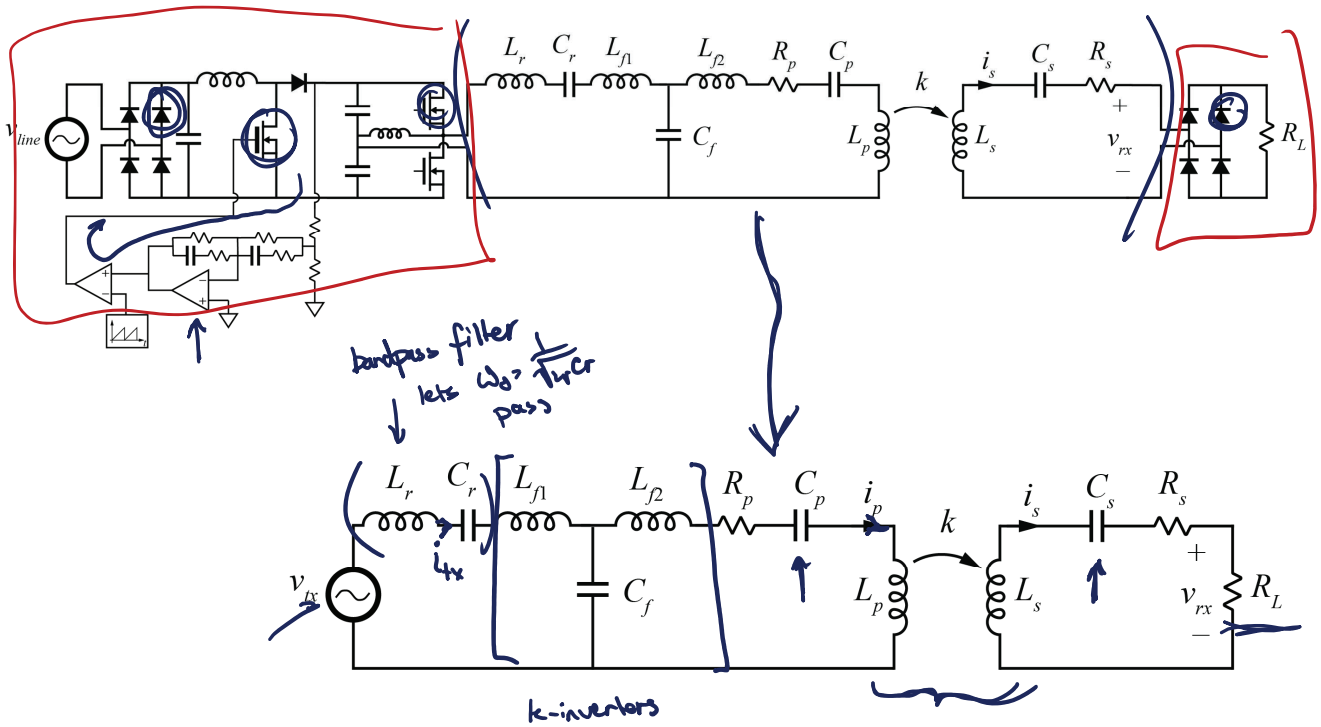
For periodic or non-periodic $f(t)$

$$F(\omega) = \mathcal{F}\{f(t)\} = \int_{-\infty}^{\infty} e^{-j\omega t} f(t)dt$$

$$f(t) = \mathcal{F}^{-1}\{F(\omega)\} = \frac{1}{2\pi}\int_{-\infty}^{\infty} e^{j\omega t} F(\omega)d\omega$$

- Frequency content of a signal
- Gives mag/phase of sinusoids that add up to original signal

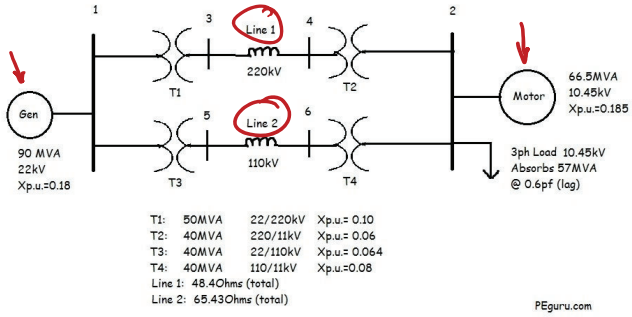
A Return to Lecture 1

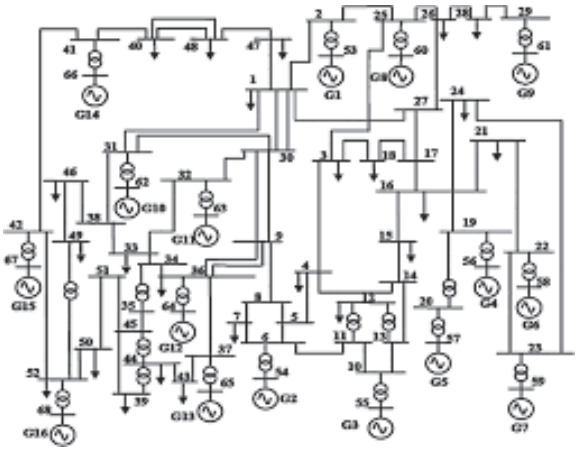


FUTURE TOPICS

Power Systems

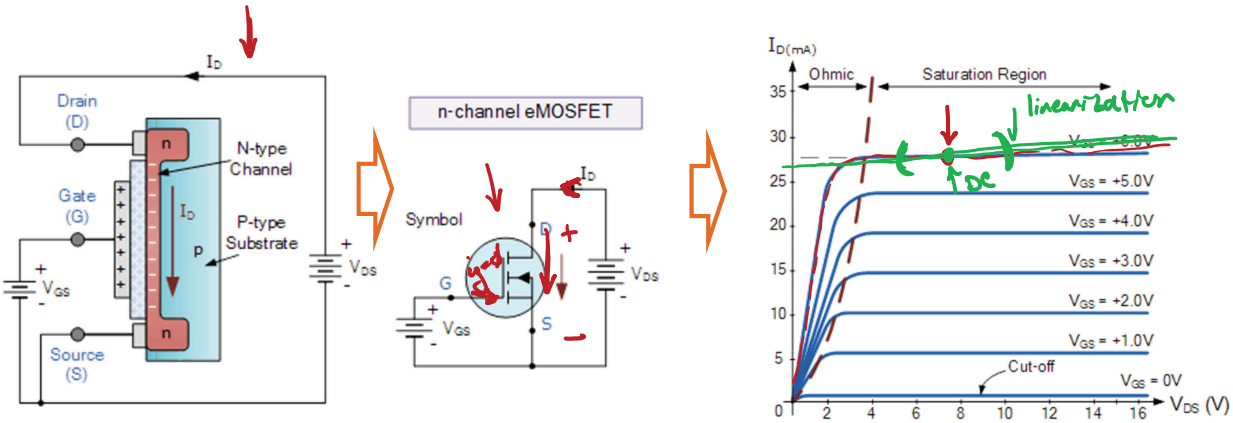
- ECE 325 -- Electric Energy System Components

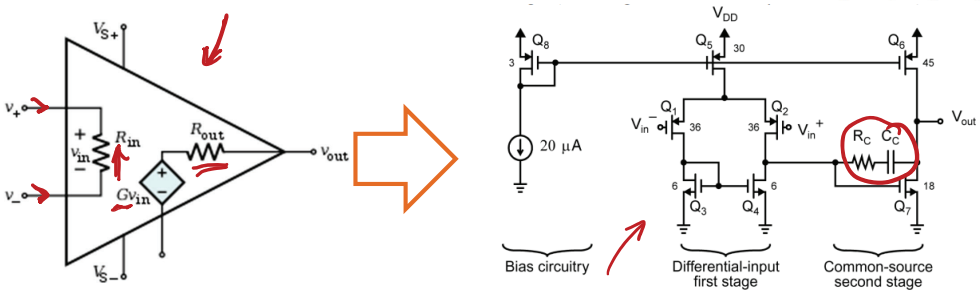




Nonlinear Circuits

- ECE 335 & 336 – Electronic Devices

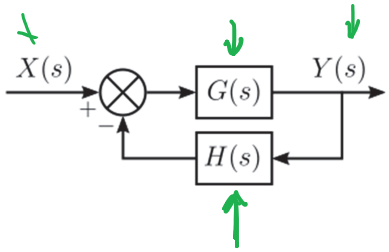




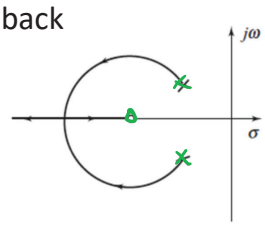
Closed-Loop Control

- ECE 316 – Signals and Systems

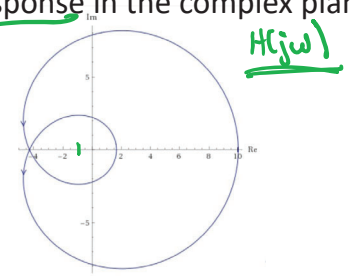
Classic Control



Root Locus: How poles and zeros move as you change feedback



Nyquist Plots: Frequency response in the complex plane



Modern Control

$$\dot{\mathbf{x}}(t) = \mathbf{A}(t)\mathbf{x}(t) + \mathbf{B}(t)\mathbf{u}(t)$$
$$\mathbf{y}(t) = \mathbf{C}(t)\mathbf{x}(t) + \mathbf{D}(t)\mathbf{u}(t)$$

matrices

poles ← eigs(A)

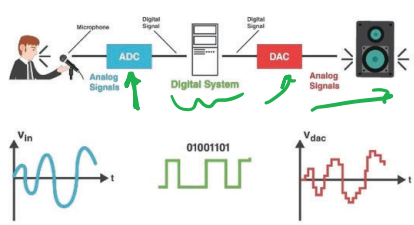
$$H(s) = \boldsymbol{C}(s\boldsymbol{I} - \boldsymbol{A})^{-1}\boldsymbol{B} + \boldsymbol{D}$$

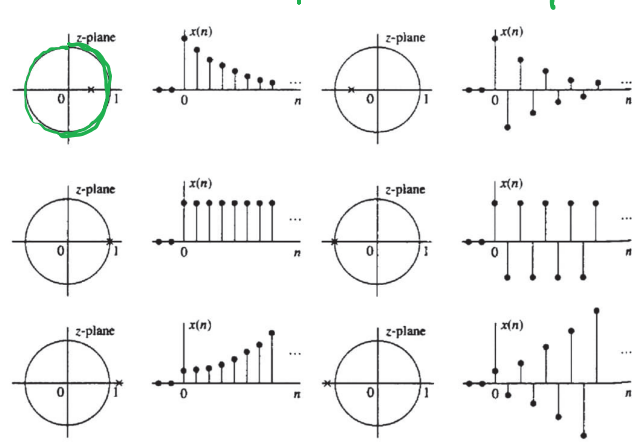
Digital / Discrete Time Signals

- ECE 315 – Signals and Systems

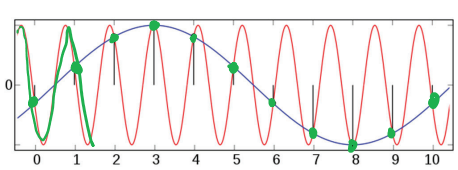
Cont. time $\sum_n A_n \frac{d^n}{dt^n} v_o(t) = \sum_m B_m \frac{d^m}{dt^m} v_i(t) \xrightarrow{\mathcal{L}} \sum_n A_n s^n V_o(s) = \sum_m B_m s^m V_i(s)$

Discrete time $\sum_n A_n y[k-n] = \sum_m B_m u[k-m] \xrightarrow{\mathcal{Z}} \sum_n A_n z^{-n} Y(z) = \sum_m B_m z^{-m} U(z)$





Sampling and aliasing:



FINAL REMARKS

Thank you for all your hard work

Good luck

THE UNIVERSITY OF TENNESSEE KNOXVILLE

Slido: #Q711