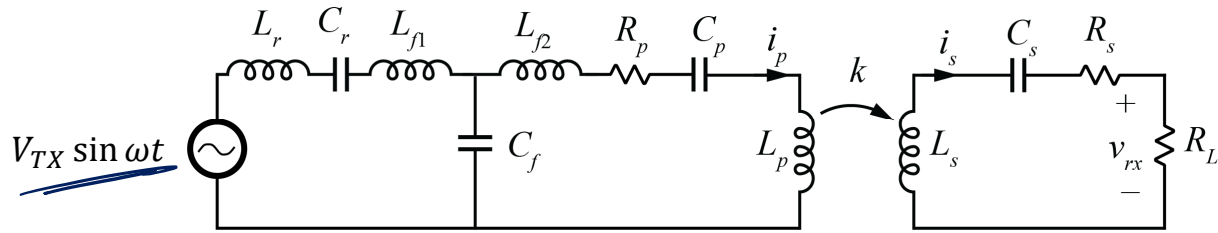


## CHAPTER 10: SINUSOIDAL STEADY-STATE

# Motivation



Want to be able to analyze more complex circuits w/out complex & error-prone diff eqs analysis & algebra

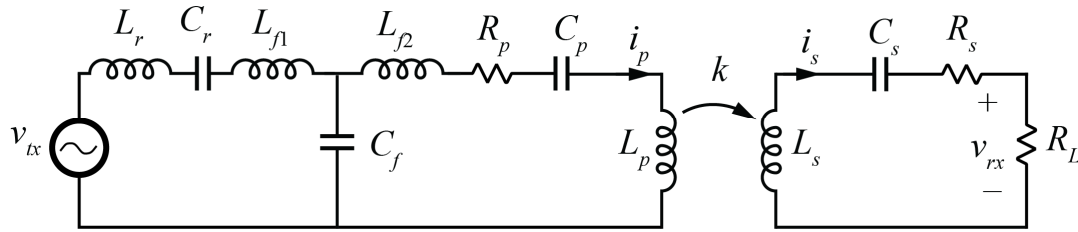
Sinusoidal → Good model for e.g. applications in RF, Power systems, oscillators, certain power conversion

later: extend to non-sinusoidal sources

steady-state → Ignore, initially any transient dynamics

later: extend to transient dynamics

# Motivation



Numerical

Analytical

Time Domain

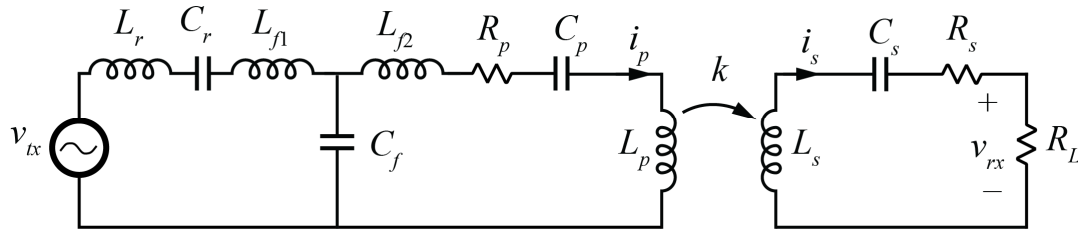
Frequency Domain

system of  
Diff EQs

$$\left\{ \begin{array}{l} \frac{dA}{dt} = \beta_A \cdot \frac{D^n}{K_{DA}^n + D^n} \cdot \left( 1 - \frac{C^n}{K_{CA}^n + C^n} \right) - \alpha_A \cdot A \\ \frac{dX}{dt} = \beta_X \cdot \frac{A^n}{K_{AX}^n + A^n} - \alpha_X \cdot X \\ \frac{dC}{dt} = \beta_C \cdot \frac{K_{AXC}^n}{K_{AXC}^n + (A+X)^n} - \alpha_C \cdot C \\ \frac{dB}{dt} = \beta_B \cdot \frac{C^n}{K_{CB}^n + C^n} \cdot \left( 1 - \frac{D^n}{K_{DB}^n + D^n} \right) - \alpha_B \cdot B \\ \frac{dY}{dt} = \beta_Y \cdot \frac{B^n}{K_{BY}^n + B^n} - \alpha_Y \cdot Y \\ \frac{dD}{dt} = \beta_D \cdot \frac{(B+Y)^n}{K_{BYD}^n + (B+Y)^n} - \alpha_D \cdot D \end{array} \right.$$



# Motivation

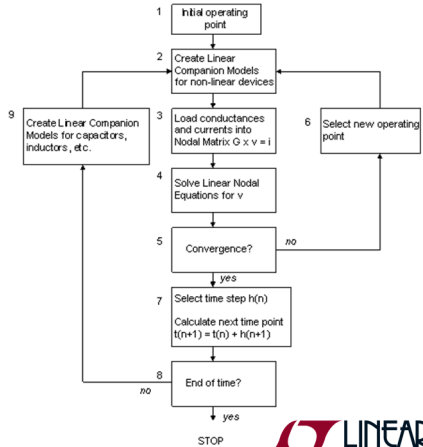


Numerical

Analytical

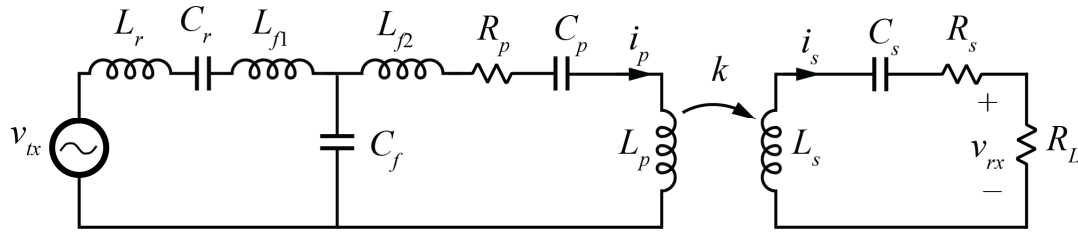
Time Domain

Frequency Domain



$$\left\{ \begin{array}{l} \frac{dA}{dt} = \beta_A \cdot \frac{D^n}{K_{DA}^n + D^n} \cdot \left( 1 - \frac{C^n}{K_{CA}^n + C^n} \right) - \alpha_A \cdot A \\ \frac{dX}{dt} = \beta_X \cdot \frac{A^n}{K_{AX}^n + A^n} - \alpha_X \cdot X \\ \frac{dC}{dt} = \beta_C \cdot \frac{(A+X)^n}{K_{AC}^n + (A+X)^n} - \alpha_C \cdot C \\ \frac{dB}{dt} = \beta_B \cdot \frac{C^n}{K_{CB}^n + C^n} \cdot \left( 1 - \frac{D^n}{K_{DB}^n + D^n} \right) - \alpha_B \cdot B \\ \frac{dY}{dt} = \beta_Y \cdot \frac{B^n}{K_{BY}^n + B^n} - \alpha_Y \cdot Y \\ \frac{dD}{dt} = \beta_D \cdot \frac{(B+Y)^n}{K_{DY}^n + (B+Y)^n} - \alpha_D \cdot D \end{array} \right.$$

# Motivation

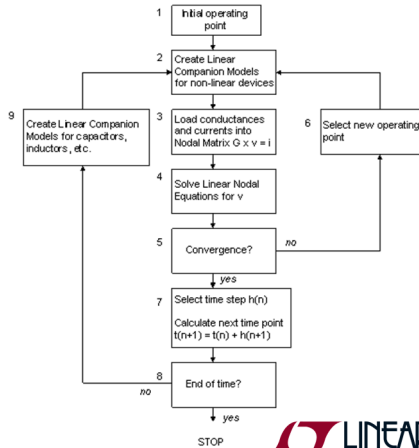


Numerical

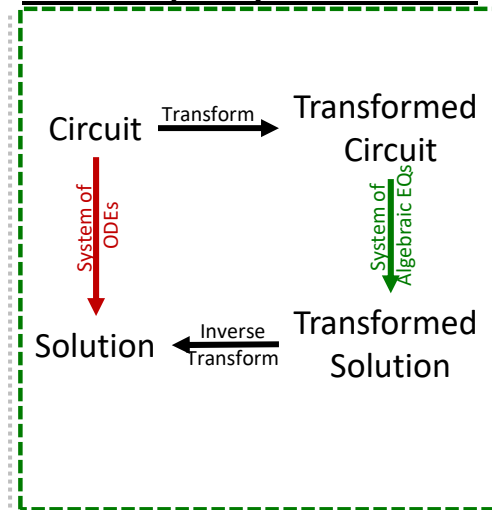
Analytical

Time Domain

Frequency Domain



$$\left\{ \begin{array}{l} \frac{dA}{dt} = \beta_A \cdot \frac{D^n}{K_{DA}^n + D^n} \cdot \left( 1 - \frac{C^n}{K_{CA}^n + C^n} \right) - \alpha_A \cdot A \\ \frac{dX}{dt} = \beta_X \cdot \frac{A^n}{K_{AX}^n + A^n} - \alpha_X \cdot X \\ \frac{dC}{dt} = \beta_C \cdot \frac{K_{AXC}^n}{K_{AXC}^n + (A+X)^n} - \alpha_C \cdot C \\ \frac{dB}{dt} = \beta_B \cdot \frac{C^n}{K_{CB}^n + C^n} \cdot \left( 1 - \frac{D^n}{K_{DB}^n + D^n} \right) - \alpha_B \cdot B \\ \frac{dY}{dt} = \beta_Y \cdot \frac{B^n}{K_{BY}^n + B^n} - \alpha_Y \cdot Y \\ \frac{dD}{dt} = \beta_D \cdot \frac{K_{BYD}^n}{K_{BYD}^n + (B+Y)^n} - \alpha_D \cdot D \end{array} \right.$$



# Form of the Solution

$N^{\text{th}}$  order circuit with sinusoidal input described by

$N$  derivatives of  $v_o(t)$

$M$  derivatives of  $v_i(t)$

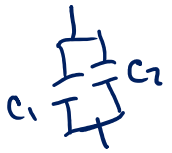
$M < N \approx \#$  of capacitors & inductors

$$b_N \frac{d^N}{dt^N} v_o(t) + \dots + b_1 \frac{d}{dt} v_o(t) + b_0 v_o(t) = a_M \frac{d^M}{dt^M} v_i(t) + \dots + a_1 \frac{d}{dt} v_i(t) + a_0 v_i(t)$$

$$\sum_{i=0}^N b_i \frac{d^i}{dt^i} v_o(t) = \sum_{i=0}^M a_i \frac{d^i}{dt^i} v_i(t)$$

solution for  $v_o(t)$  will be of the form

$$v_o(t) = v_{o,h}(t) + v_{o,p}(t)$$



# Transient Response

$v_{o,h}(t)$  is the homogeneous solution to the differential equation, the natural response of the system, or the transient response of the system. For any non-ideal (damped) circuit,  $v_{o,h}(t)$  will tend to zero over time

$v_{o,h}(t)$  is the solution to the equation

$$\sum_{i=0}^N b_i \frac{d^i}{dt^i} v_{o,h}(t) = 0$$

which will be of the form

$$v_{o,h}(t) = \sum_{i=0}^N A_i e^{s_i t}$$

$s_i \rightarrow$  roots of characteristic polynomial

$A_i \rightarrow$  determined by initial conditions

Note: some of the time constants ( $s_i$ ) of a circuit are independent of the input

# Steady-State Response

$v_{o,p}(t)$  is the particular solution to the differential equation, the forced response of the system, or the steady-state response of the system. In general, it does not tend to zero, if non-zero inputs are present.

$v_{o,p}(t)$  is the non-zeroing solution to the equation

$$\sum_{i=0}^N b_i \frac{d^i}{dt^i} v_o(t) = \sum_{i=0}^M a_i \frac{d^i}{dt^i} v_i(t)$$



# LTI Systems

For a function  $f(\cdot)$

## Linearity

if:  $v_{o,1}(t) = f(v_{i,1}(t))$        $v_{o,2}(t) = f(v_{i,2}(t))$

then:  $av_{o,1}(t) + bv_{o,2}(t) = f(av_{i,1}(t) + bv_{i,2}(t))$

*superposition applies*

## Time Invariance

if:  $v_o(t) = f(v_i(t))$

then:  $v_o(t - T) = f(v_i(t - T))$

LTI:  $v_x(t) + v_y(t)$ ,  $\alpha v_x(t)$ ,  $\frac{dv_x(t)}{dt}$ ,  $\int_0^t v_x(t) dt$  (neglecting ICs)

Not LTI:  $v_x(t) \cdot v_y(t)$ ,  $v_x(t)^2$ ,  $|v_x(t)|$   $\rightarrow$  *power isn't a linear calculation*

*LTI*

# Causality

- Causal systems cannot predict the future
- $v_o(t_0)$  does not depend on values of  $v_i(t)$ ,  $t > t_0$

$$v_{o,1}(t) = f(v_{i,1}(t)) \quad v_{o,2}(t) = f(v_{i,2}(t))$$

$$\text{if: } v_{i,1}(t) = v_{i,2}(t) \quad \forall \quad t < t_0$$

$$\text{then: } v_{o,1}(t) = v_{o,2}(t) \quad \forall \quad t < t_0$$

# Preview of Frequency Domain

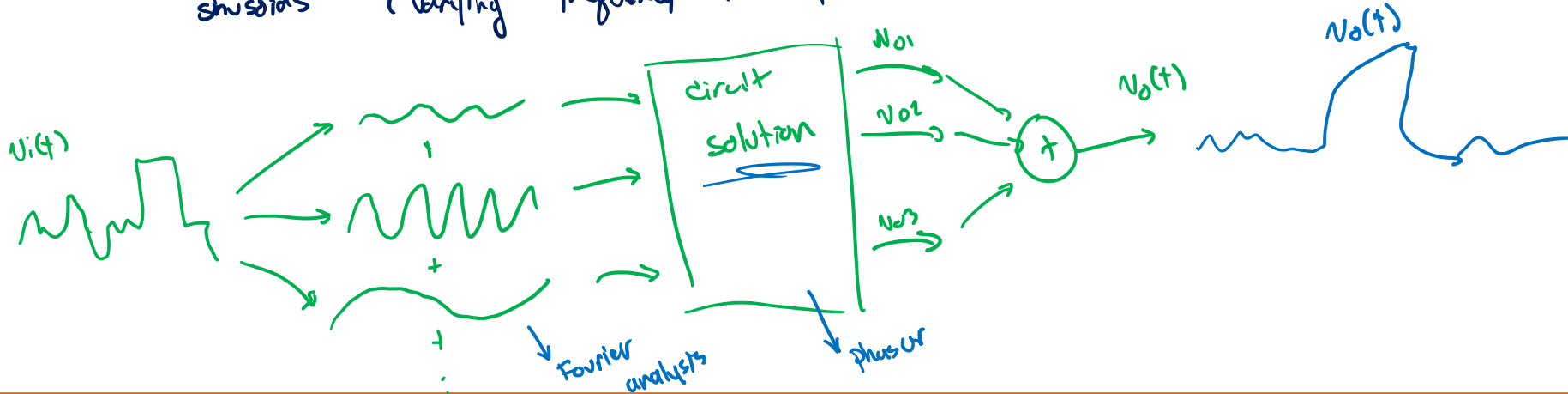
for LTI systems

Ch 10

- Develop "phasor analysis" → for sinusoidal inputs & steady state only
- we know superposition applies

Remainder of course

- (1) Make it very easy to solve circuits with sinusoidal inputs
- (2) Find a way to express any arbitrary input as a sum of sinusoids (varying frequency & amplitude)



steady-state

$$\sum_{i=0}^N b_i \frac{d^i}{dt^i} v_o(t) = \sum_{i=0}^M a_i \frac{d^i}{dt^i} v_i(t)$$

let's guess  $v_o(t) = A \cos(\omega t + \varphi)$

$$v_i(t) = \underline{V_I \cos(\omega t)}$$

→ if inputs are sinusoids @  $\omega$   
outputs are sinusoids @  $\omega$

$$\frac{d}{dt} v_o(t) = v_o'(t) = -A\omega \sin(\omega t + \varphi)$$

$$v_o''(t) = -A\omega^2 \cos(\omega t + \varphi)$$

$$v_o'''(t) = A\omega^3 \sin(\omega t + \varphi)$$

$$v_o^{(4)}(t) = A\omega^4 \cos(\omega t + \varphi)$$

⋮