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# Lecture 6: Semiconductor Device Implementation

ECE 481: Power Electronics

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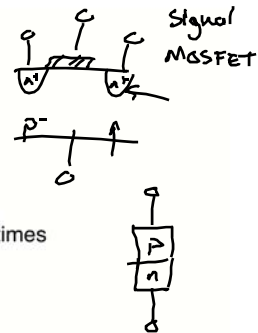
## 4.2. A brief survey of power semiconductor devices

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- Power diodes
- Power MOSFETs
- Bipolar Junction Transistors (BJTs)
- Insulated Gate Bipolar Transistors (IGBTs)
- Thyristors (SCR, GTO, MCT)

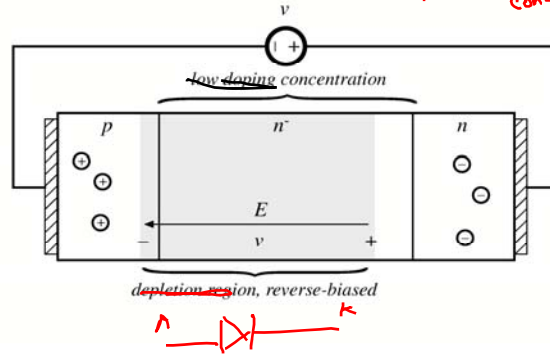
- On resistance vs. breakdown voltage vs. switching times
- Minority carrier and majority carrier devices



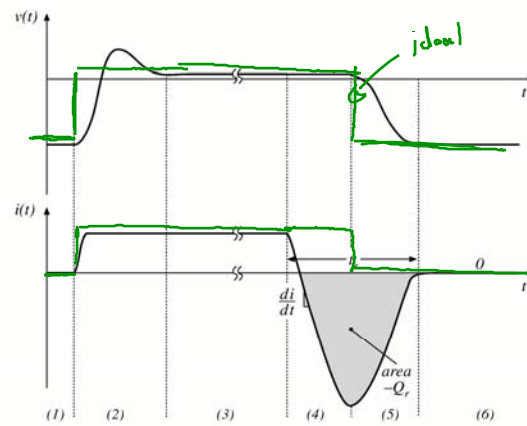
## 4.2.1. Power diodes

A power diode, under reverse-biased conditions:

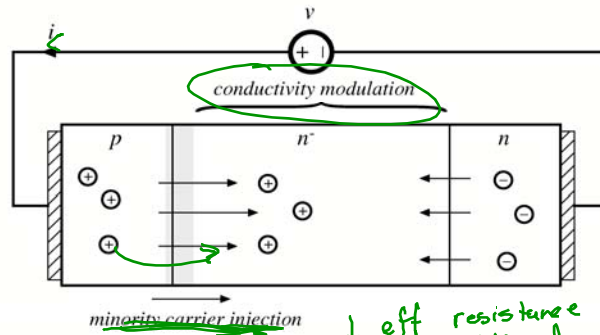
$W_{dep} \propto \frac{1}{doping\ conc.}$



## Typical diode switching waveforms



## Forward-biased power diode



↓ eff resistance of large, lightly doped region (reg for large  $V_{BR}$ )

## Charge-controlled behavior of the diode

The diode equation:

$$q(t) = Q_0(e^{\lambda v(t)} - 1)$$

Charge control equation:

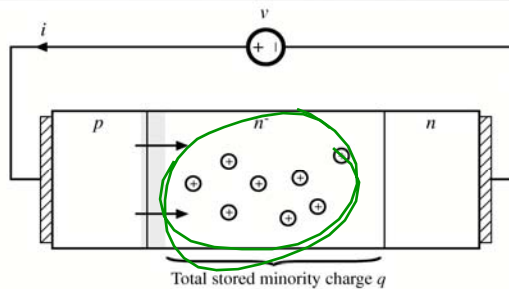
$$\frac{dq(t)}{dt} = i(t) - \frac{q(t)}{\tau_L}$$

With:

$$\lambda = 1/(26 \text{ mV}) \text{ at } 300 \text{ K}$$

$\tau_L =$  minority carrier lifetime

(above equations don't include current that charges depletion region capacitance)



In equilibrium:  $dq/dt = 0$ , and hence

$$i(t) = \frac{q(t)}{\tau_L} = \frac{Q_0}{\tau_L} (e^{\lambda v(t)} - 1) = I_0 (e^{\lambda v(t)} - 1)$$

↑  $\tau$ , ↑  $q$

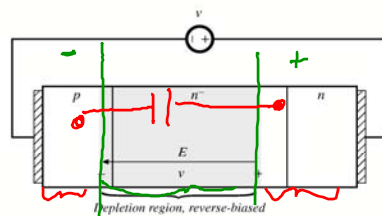
## Charge-control in the diode: Discussion

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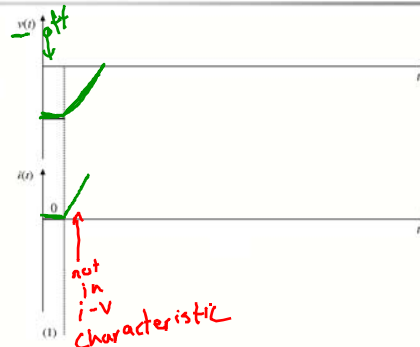
- The familiar  $i-v$  curve of the diode is an equilibrium relationship that can be violated during transient conditions
- During the turn-on and turn-off switching transients, the current deviates substantially from the equilibrium  $i-v$  curve, because of change in the stored charge and change in the charge within the reverse-bias depletion region
- Under forward-biased conditions, the stored minority charge causes “conductivity modulation” of the resistance of the lightly-doped  $n^-$  region, reducing the device on-resistance

## Diode in OFF state: reversed-biased, blocking voltage

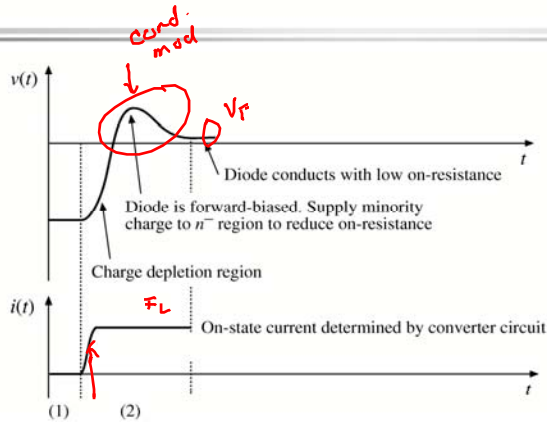
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- Diode is reverse-biased
- No stored minority charge:  $q = 0$
- Depletion region blocks applied reverse voltage; charge is stored in capacitance of depletion region



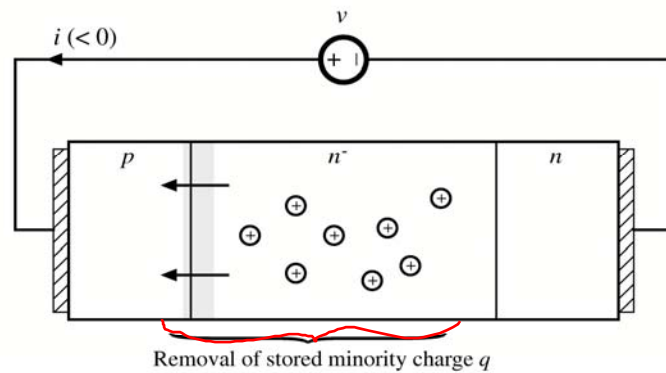
## Turn-on transient

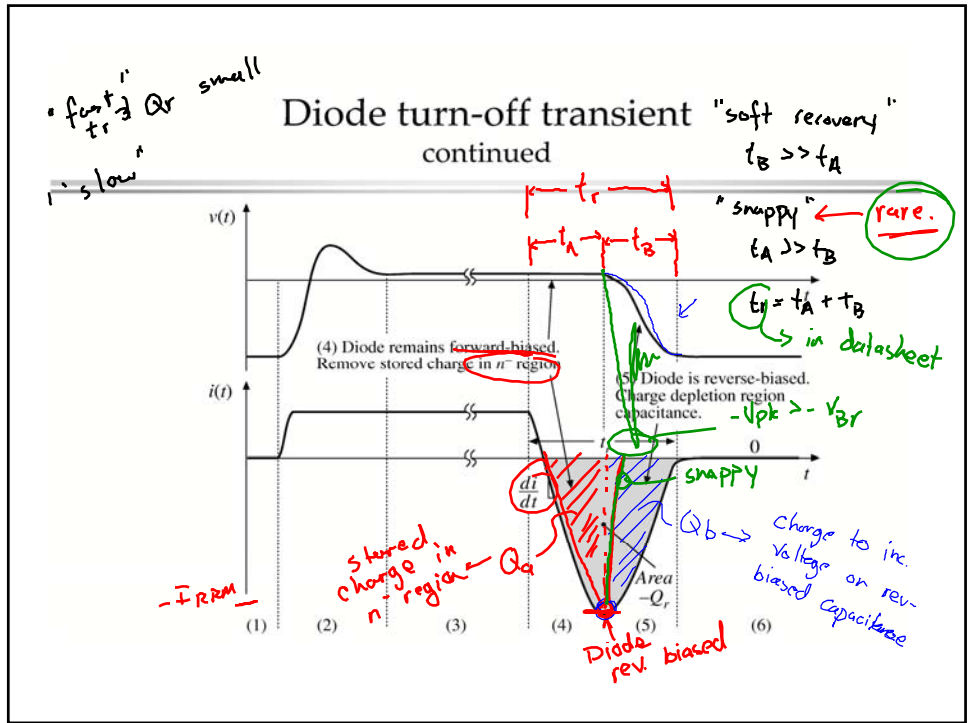


The current  $i(t)$  is determined by the converter circuit. This current supplies:

- charge to increase voltage across depletion region
- charge needed to support the on-state current
- charge to reduce on-resistance of  $n^-$  region

## Turn-off transient





## Datasheet Reported Turn-off Characteristics

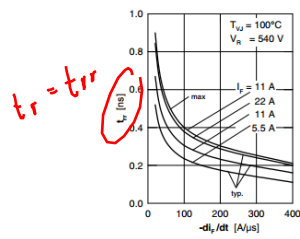


Fig. 5 Recovery time versus  $-di/dt$

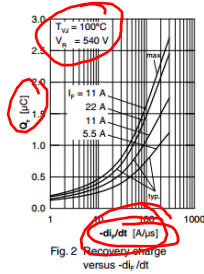


Fig. 2 Recovery charge versus  $-di/dt$

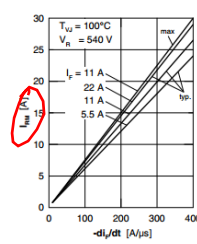
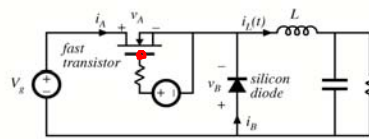


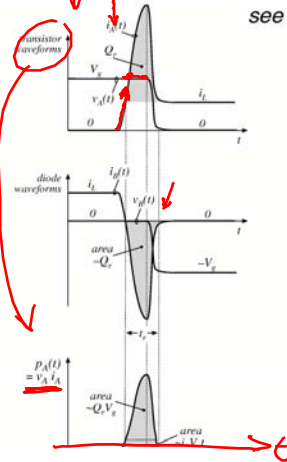
Fig. 3 Peak reverse current versus  $-di/dt$

*Turn-off waveforms depend on  $T_j$ ,  $\frac{di}{dt}$ ,  $V_R$ ,  $I_F$*

## The diode switching transients induce switching loss in the transistor



- Diode recovered stored charge  $Q_r$  flows through transistor during transistor turn-on transition, inducing switching loss
- $Q_r$  depends on diode on-state forward current, and on the rate-of-change of diode current during diode turn-off transition



see Section 4.3.2

## Reverse Recovery Loss



Assume MOSFET Ideal  
 (1) switches very fast  
 (2) low r<sub>on</sub>

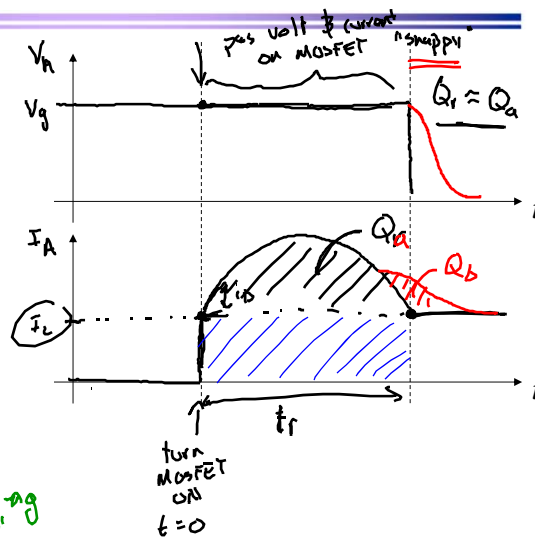
$$W_{off} = \int_{t_r} V_A I_A dt$$

$$W_{off} = V_g \int_{t_r} I_A dt$$

$$= V_g [Q_r + I_L t_r]$$

$$P_{off} = W_{off} f_s$$

↳ "switching loss"



## Switching loss calculation

Energy lost in transistor:

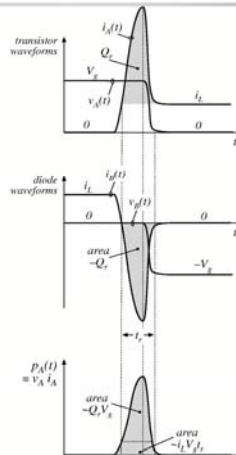
$$W_D = \int_{\text{switching transition}} v_A(t) i_A(t) dt$$

With abrupt-recovery diode:

$$W_D \approx \int_{\text{switching transition}} V_g (i_L - i_D(t)) dt$$

$$= V_g i_L t_r + V_g Q_r$$

- Often, this is the largest component of switching loss



Soft-recovery diode:

$$(t_2 - t_1) \gg (t_1 - t_0)$$

Abrupt-recovery diode:

$$(t_2 - t_1) \ll (t_1 - t_0)$$

## Types of power diodes

Standard recovery → "slow"

Reverse recovery time not specified, intended for 50/60Hz

→ Fast recovery and ultra-fast recovery

Reverse recovery time and recovered charge specified

Intended for converter applications → 10's of kHz & up

Schottky diode

A majority carrier device

Essentially no recovered charge → no conductivity modulation

Model with equilibrium  $i-v$  characteristic, in parallel with depletion region capacitance

Restricted to low voltage (few devices can block 100V or more)



## Characteristics of several commercial power rectifier diodes

| Part number                           | Rated max voltage | Rated avg current | $V_f$ (typical) | $t_r$ (max) |
|---------------------------------------|-------------------|-------------------|-----------------|-------------|
| <b>Fast recovery rectifiers</b>       |                   |                   |                 |             |
| IN3913                                | 400V              | 30A               | 1.1V            | 400ns       |
| SD453N25S20PC                         | 2500V             | 400A              | 2.2V            | 2 $\mu$ s   |
| <b>Ultra-fast recovery rectifiers</b> |                   |                   |                 |             |
| MUR815                                | 150V              | 8A                | 0.975V          | 35ns        |
| MUR1560                               | 600V              | 15A               | 1.2V            | 60ns        |
| RHRU100120                            | 1200V             | 100A              | 2.6V            | 60ns        |
| <b>Schottky rectifiers</b>            |                   |                   |                 |             |
| MBR6030L                              | 30V               | 60A               | 0.48V           |             |
| 444CNQ045                             | 45V               | 440A              | 0.69V           |             |
| 30CPQ150                              | 150V              | 30A               | 1.19V           |             |
| <b>SiC Schottky</b>                   |                   |                   |                 |             |
| SCS220AGC                             | 600V              | 20A               | 1.55V           | 0ns         |
| APT30SCD120S                          | 1.2kV             | 99A               | 1.8V            | 0ns         |

n-type or fast

## Paralleling diodes

→ minority carrier concentration increases w/ temp.

Attempts to parallel diodes, and share the current so that  $i_1 = i_2 = i/2$ , generally don't work.

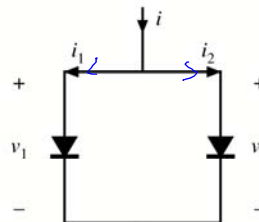
*Reason:* thermal instability caused by temperature dependence of the diode equation.

Increased temperature leads to increased current, or reduced voltage.

One diode will hog the current.

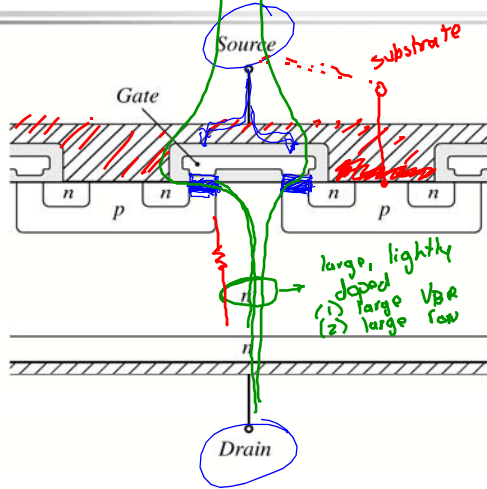
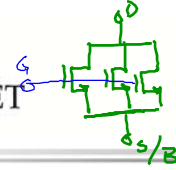
To get the diodes to share the current, heroic measures are required:

- Select matched devices → on-chip
- Package on common thermal substrate
- Build external circuitry that forces the currents to balance



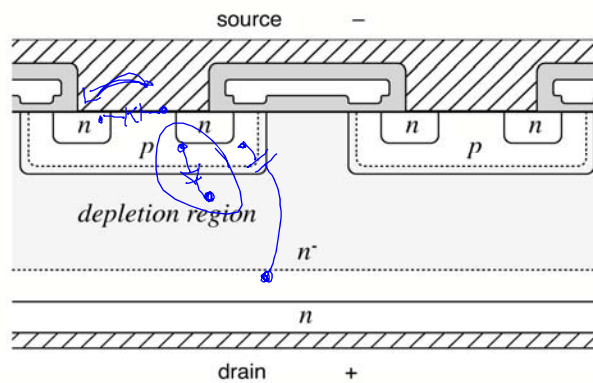
if  $I_1 > I_2$   
 ↳  $T_1 > T_2$   
 ↳ M.C. concentration in  $D_1$  increases  
 ↳  $\rho$  of  $D_1$  decreases  
 ↳  $I_1$  increases

### 4.2.2 The Power MOSFET



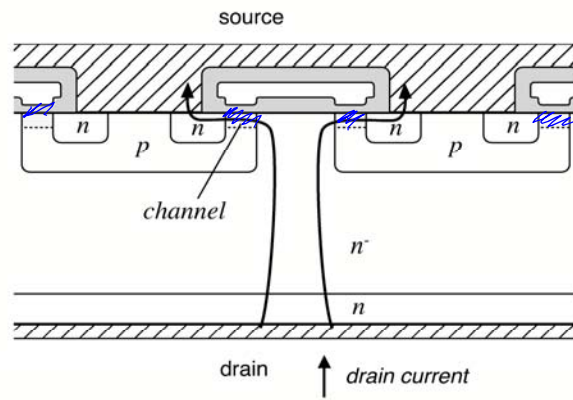
- Gate lengths approaching one micron
- Consists of many small enhancement-mode parallel-connected MOSFET cells, covering the surface of the silicon wafer
- Vertical current flow
- n-channel device is shown

### MOSFET: Off state



- p-n junction is reverse-biased
- off-state voltage appears across n<sup>+</sup> region

## MOSFET: on state



- $p$ - $n$  junction is slightly reverse-biased
- positive gate voltage induces conducting channel
- drain current flows through  $n$  region and conducting channel
- on resistance = total resistances of  $n$  region, conducting channel, source and drain contacts, etc.