

Alternative: The Phase Margin Test

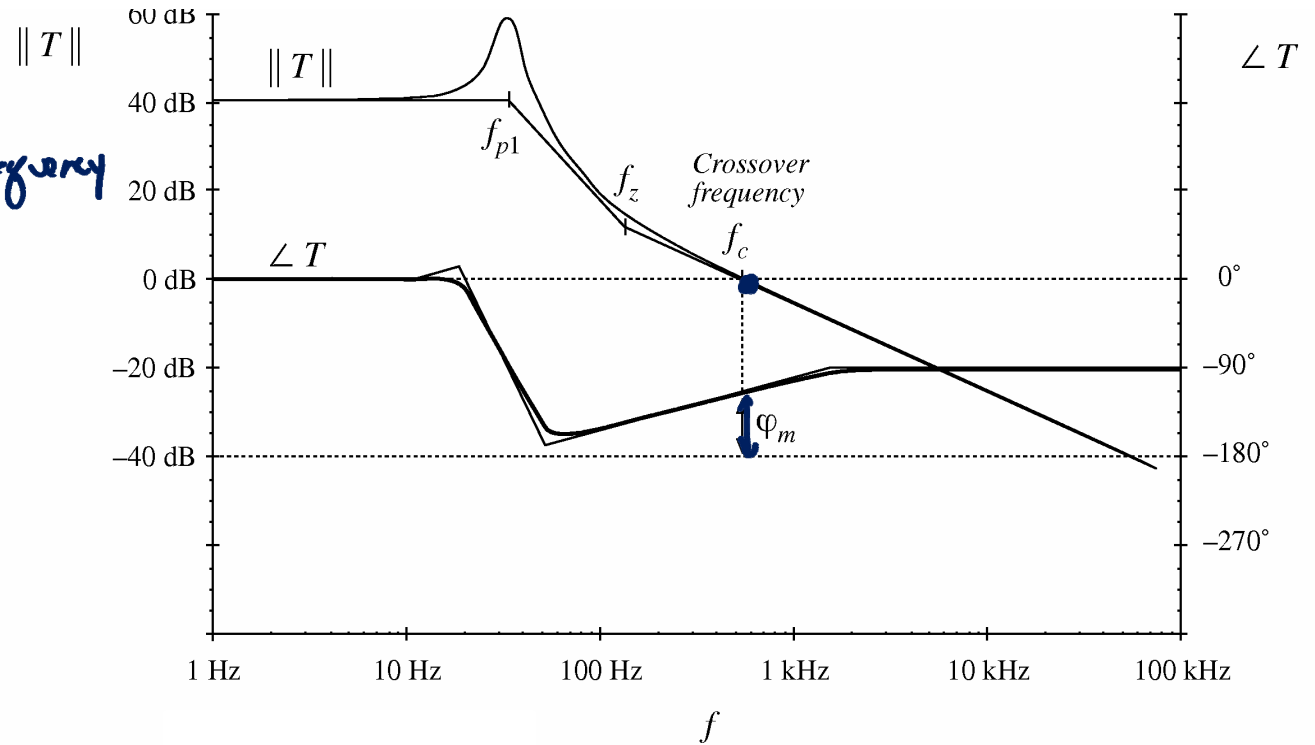
Required:

(1) $T(s)$ has no RHP poles

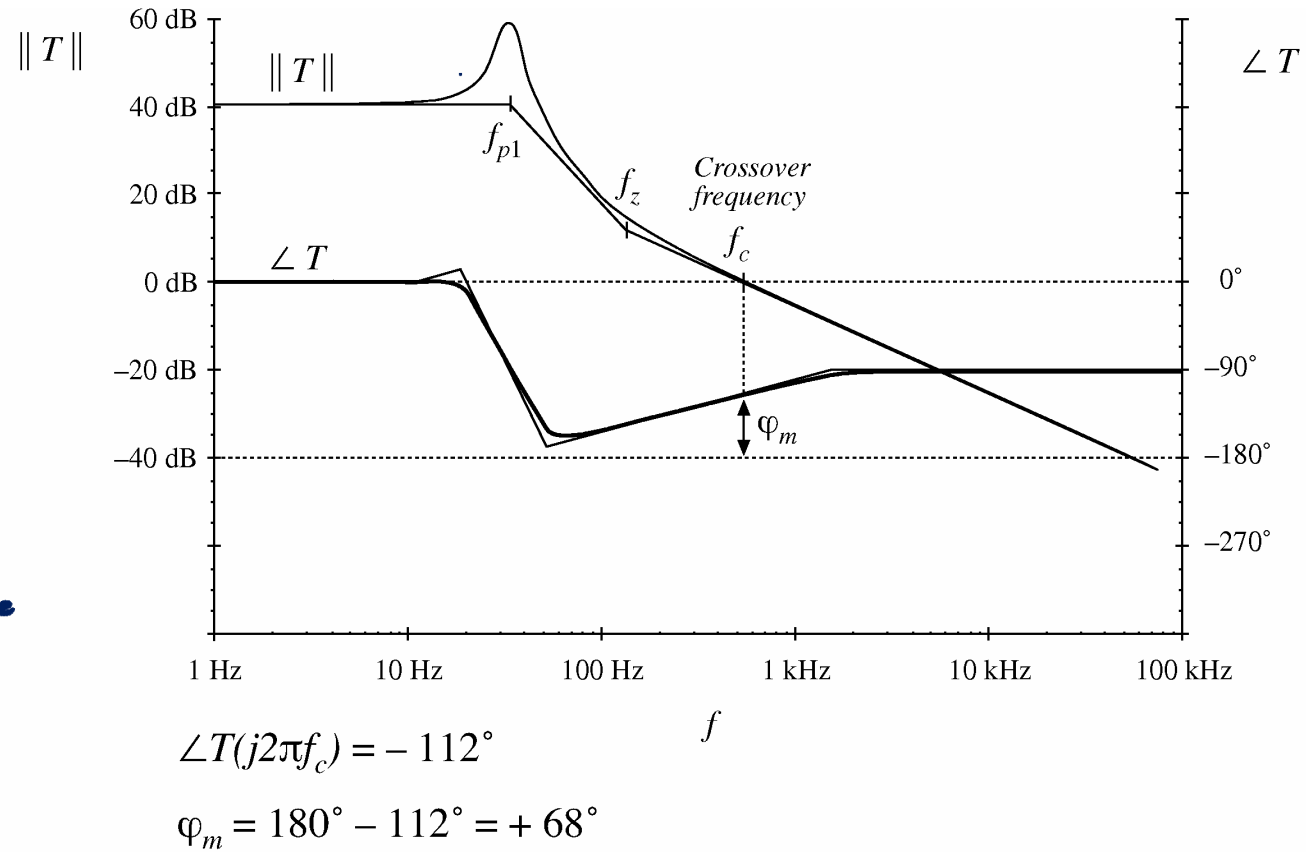
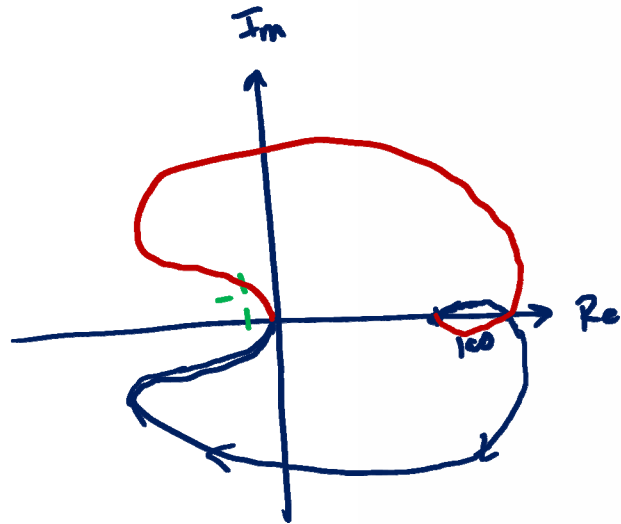
(2) $\|T(j\omega_c)\| = \phi$ for exactly one ω_c
 there is only one $f_c = \text{crossover frequency}$

System is stable if

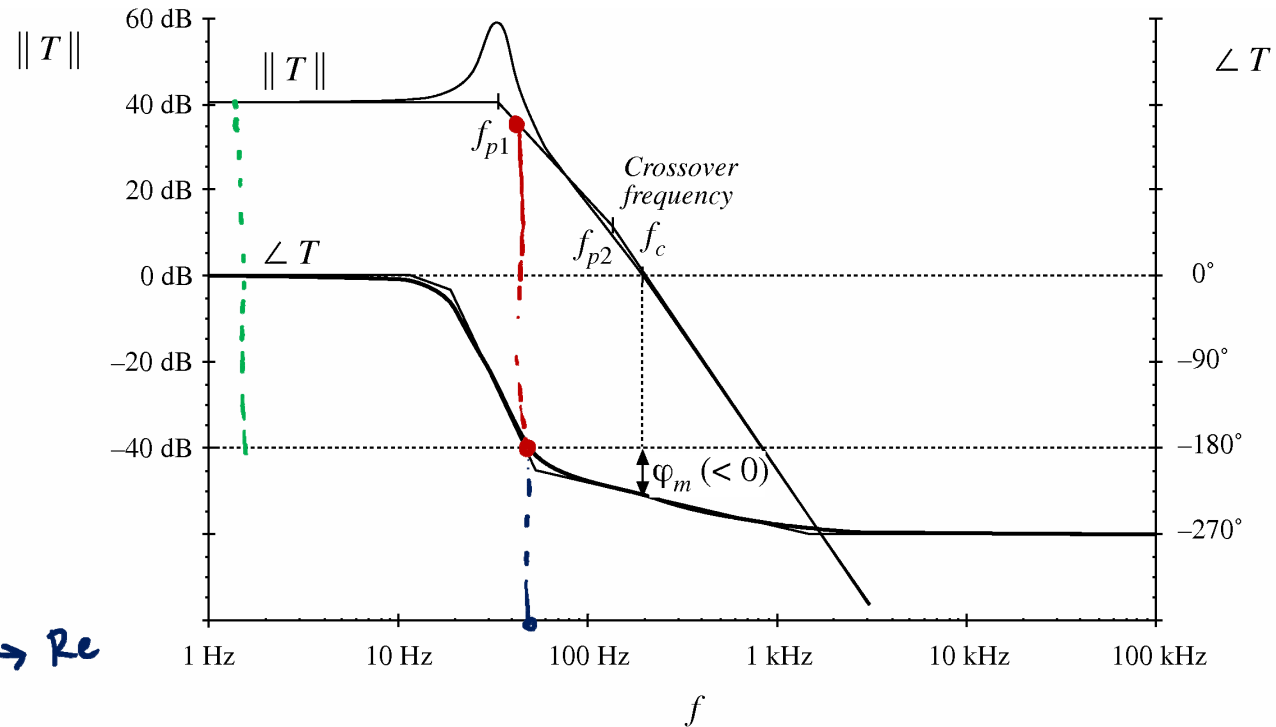
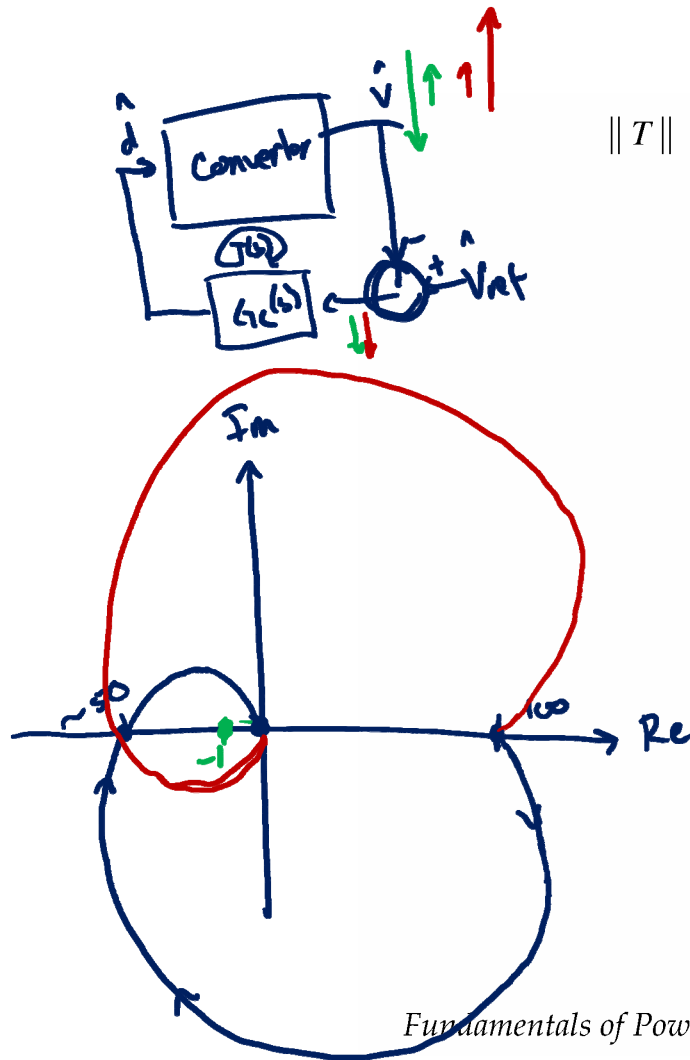
$$\varphi_m = 180^\circ + \angle T(j\omega_c) \geq 0^\circ$$



Example: Stable System



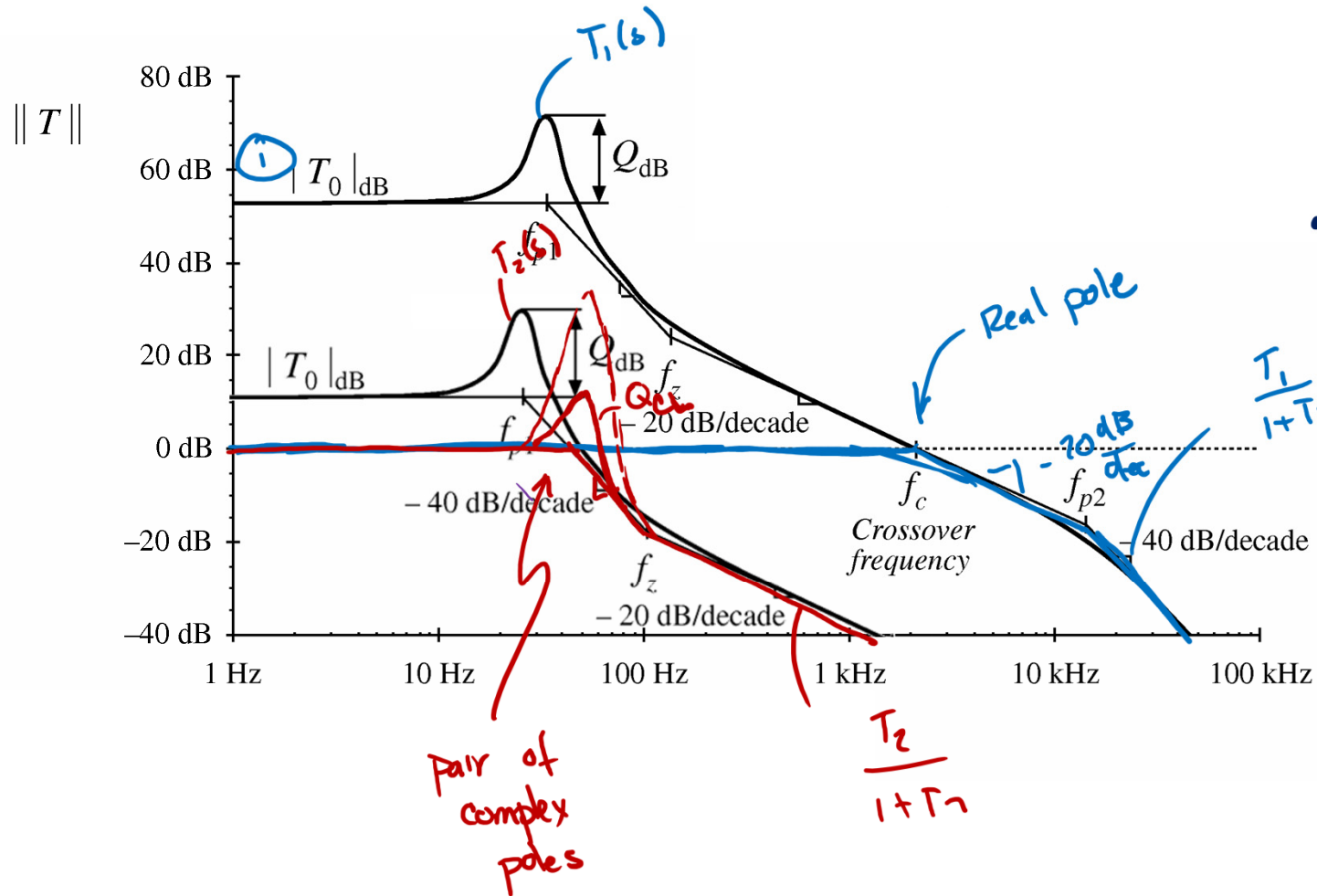
Example: Unstable System



$$\angle T(j2\pi f_c) = -230^\circ$$

$$\varphi_m = 180^\circ - 230^\circ = -50^\circ$$

T(s) vs T/1+T

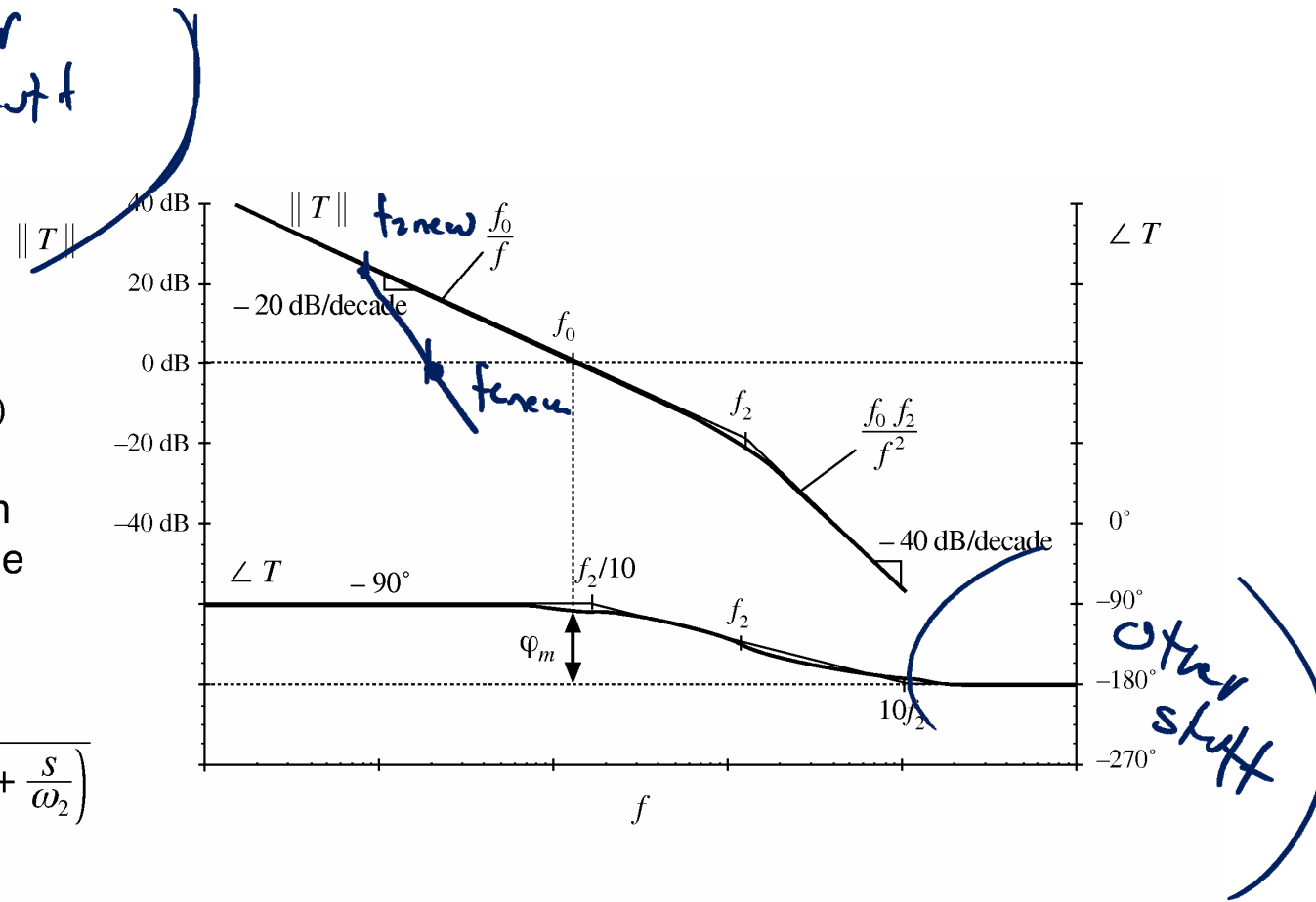


- $f_c \sim BW_{CL}$
 - design high f_c for fast response
- Q_{CL} present when f_c (rises)
 @ -40 dB/dec slope
 - will result in ringing

A Generic Second-Order System

Consider the case where $T(s)$ can be well-approximated in the vicinity of the crossover frequency as

$$T(s) = \frac{1}{\left(\frac{s}{\omega_0}\right) \left(1 + \frac{s}{\omega_2}\right)}$$



Closed-Loop Response

If

$$T(s) = \frac{1}{\left(\frac{s}{\omega_0}\right)\left(1 + \frac{s}{\omega_2}\right)}$$

Then

$$\frac{T(s)}{1 + T(s)} = \frac{1}{1 + \frac{1}{T(s)}} = \frac{1}{1 + \frac{s}{\omega_0} + \frac{s^2}{\omega_0\omega_2}}$$

or,

$$\frac{T(s)}{1 + T(s)} = \frac{1}{1 + \frac{s}{Q\omega_c} + \left(\frac{s}{\omega_c}\right)^2}$$

where

$$\omega_c = \sqrt{\omega_0\omega_2} = 2\pi f_c \quad Q_{\mathbf{cl}} = \frac{\omega_0}{\omega_c} = \sqrt{\frac{\omega_0}{\omega_2}}$$

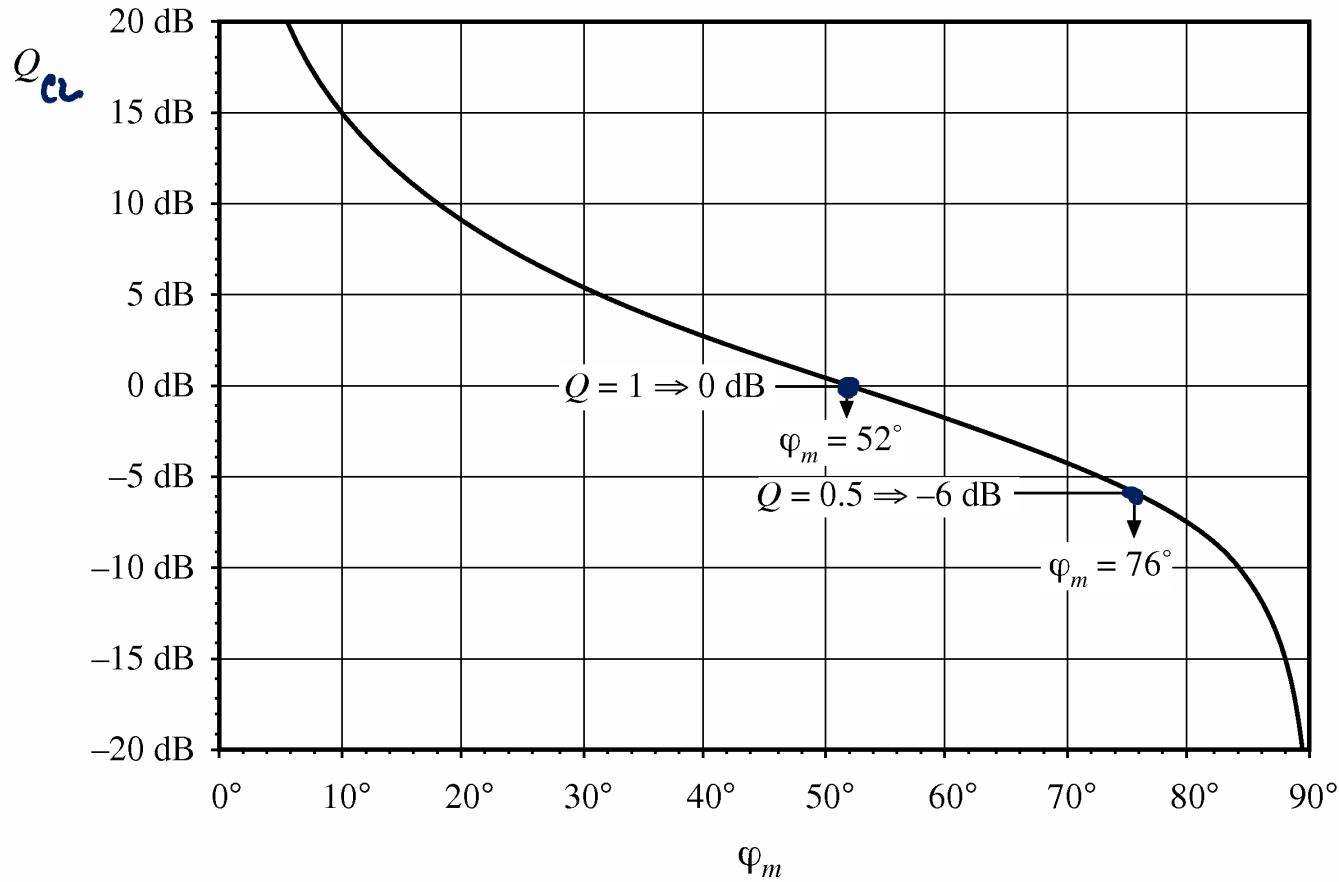
Q_{CL} vs. ϕ_m

Solve for exact crossover frequency, evaluate phase margin, express as function of ϕ_m . Result is:

$$Q = \frac{\sqrt{\cos \phi_m}}{\sin \phi_m}$$

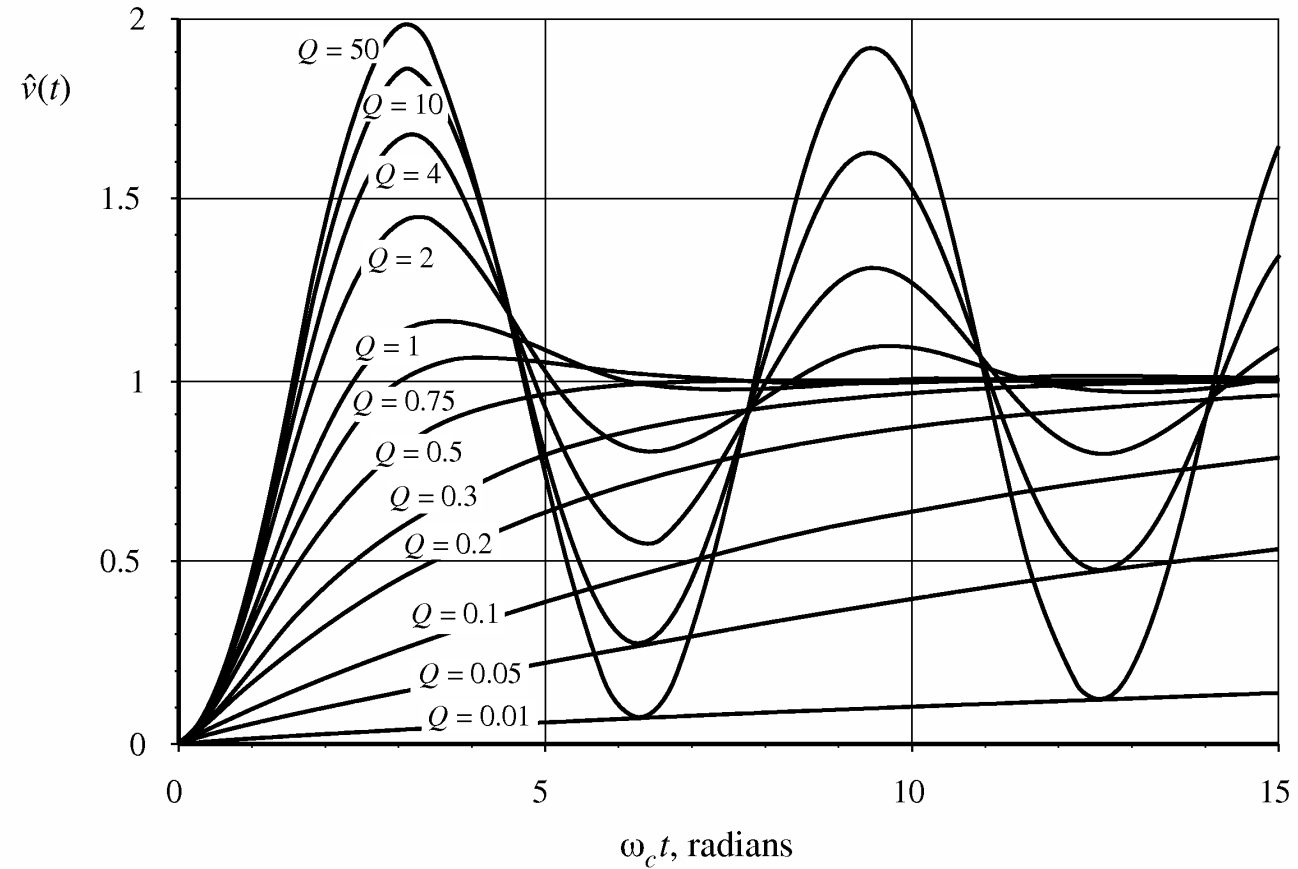
$$\phi_m = \tan^{-1} \sqrt{\frac{1 + \sqrt{1 + 4Q^4}}{2Q^4}}$$

Q_{CL} vs. ϕ_m

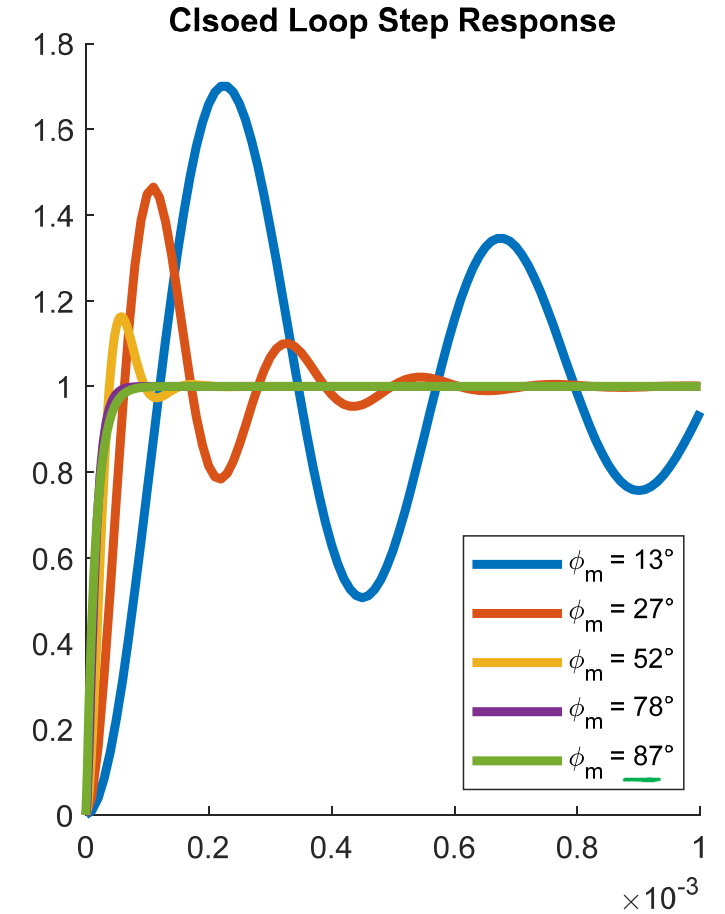
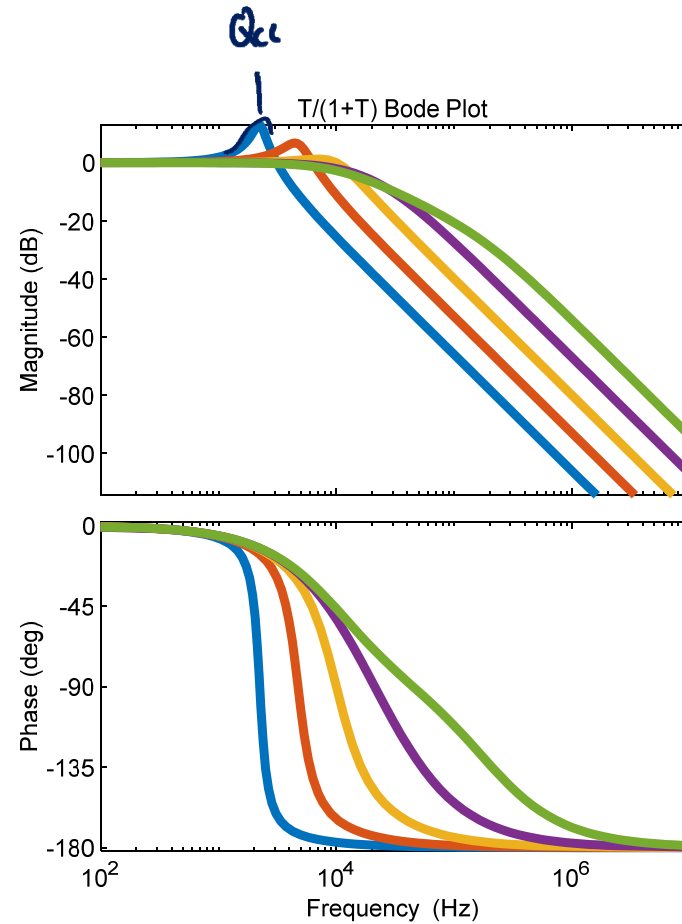
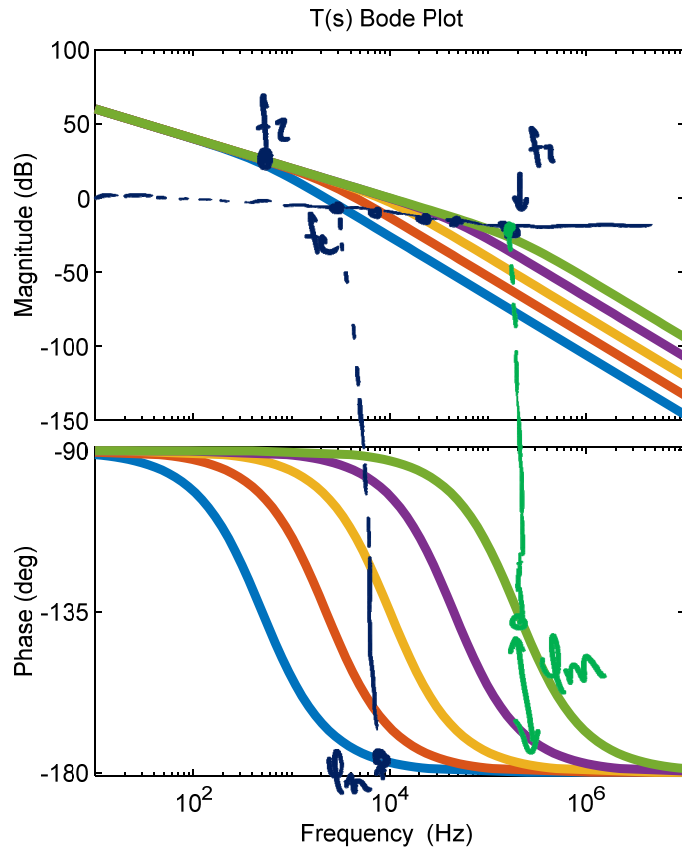


Closed-Loop Step Response vs. Q_{CL}

$$t_r = \frac{1}{\pi Q}$$



Design of Phase Margin: Constant LF Gain Case



Design of Phase Margin: Constant f_c Case

