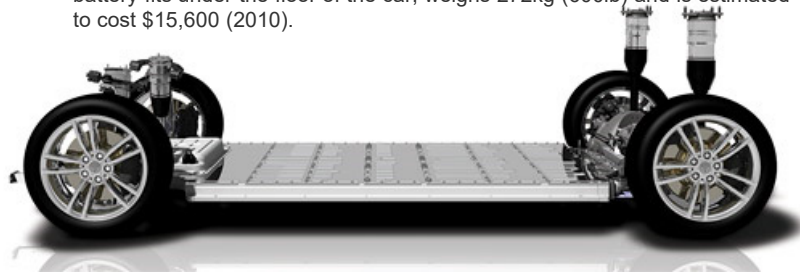


Introduction to Battery Modeling

Example EV Batteries

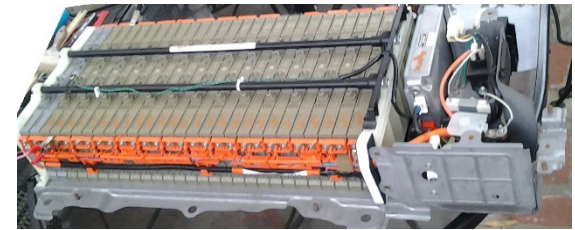


Cutaway battery of Nissan Leaf electric vehicle. The Leaf includes a 24kWh lithium-ion battery with a city driving range of 160km (100 miles). The battery fits under the floor of the car, weighs 272kg (600lb) and is estimated to cost \$15,600 (2010).



Tesla Model S frame-integrated battery. The Model S includes a 60-85kWh lithium-ion battery with a city driving range of 480km (300miles). The battery weighs 544kg (1200lb) and is estimated to cost \$24-34,000.

Toyota Prius HEV Battery. The 2004 Prius included a 1.3 kWh NiMH battery consisting of 168 cells and with a \$3K retail replacement cost



Cell Equivalent-Circuit Models

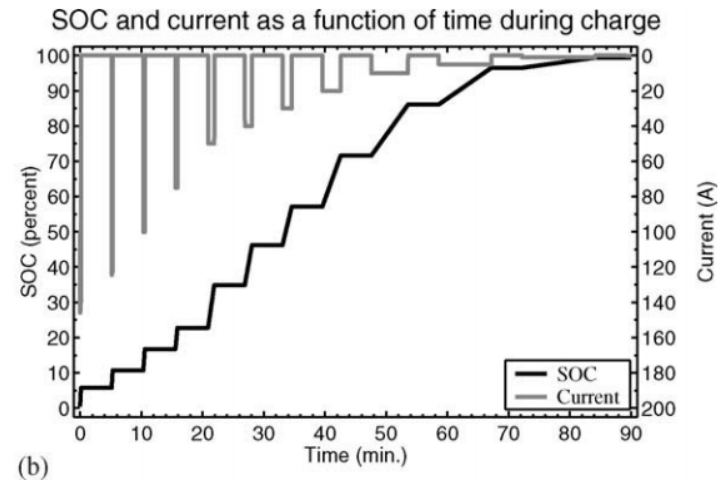
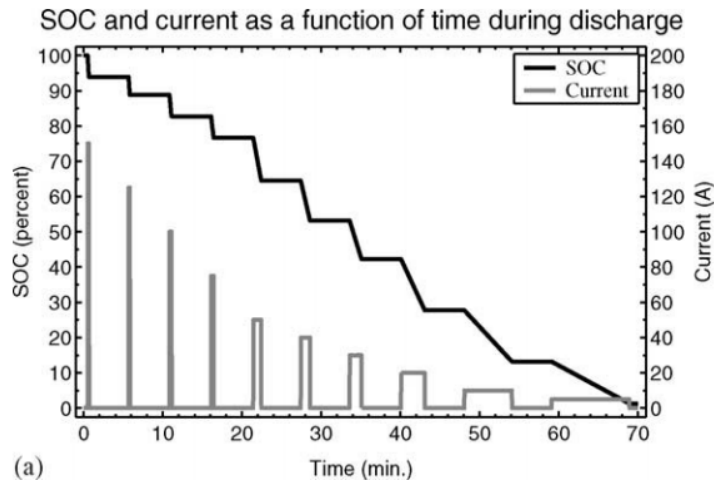
Objective:

- Dynamic circuit model capable of predicting cell voltage in response to charge/discharge current, temperature

Further key techniques discussed in [Plett 2004-Part 2] and [Plett 2004-Part 3]

- Model parameters found using least-square estimation or Kalman filter techniques based on experimental test data
- Run-time estimation of state of charge (SOC)

Approach: Pulsed current tests



Battery Nomenclature

- Known beforehand:

Capacity C [Ah]
Nominal voltage V_{nom} [V]

Max Charge Rate
Max Discharge Rate

} specified as $k \frac{C}{1hr}$
ex

$$\text{Max Charge} = 1C$$

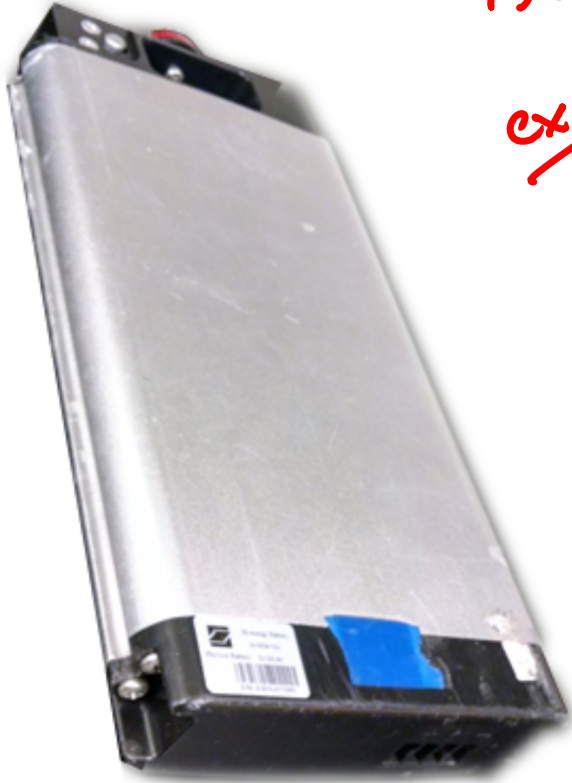
for 10Ah cell \Rightarrow 10A max charge

$$\text{Max discharge} = 5C$$

for 10Ah battery \rightarrow 50A

Example Battery

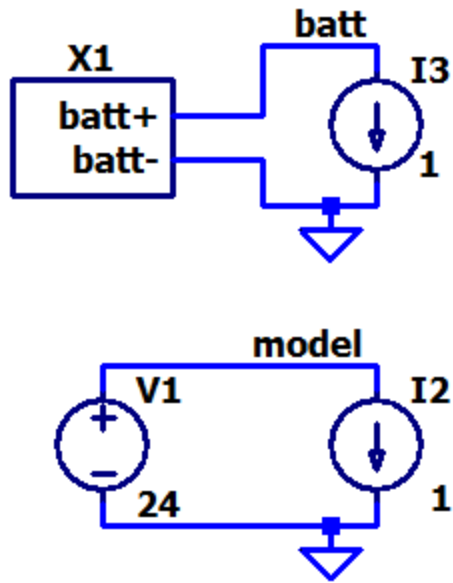
"7s5p" \rightarrow 7 cells in series, 5 in parallel



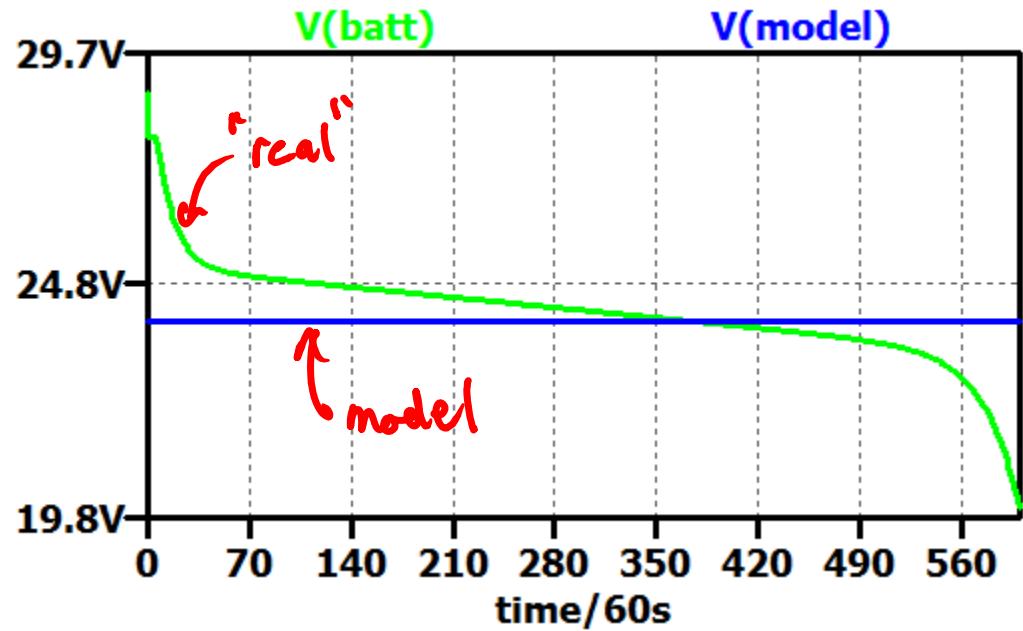
ex/ cells: $\left\{ \begin{array}{l} V_{nom} = 3.4V, \quad C = 2Ah \\ \text{Max charge} = 0.2C \\ \text{Max discharge} = 1.9C \end{array} \right.$

pack: $\left\{ \begin{array}{l} V_{nom} = 24V, \quad C = 10Ah \\ \text{Max charge} = 1C \\ \text{Max discharge} = 10C \end{array} \right.$

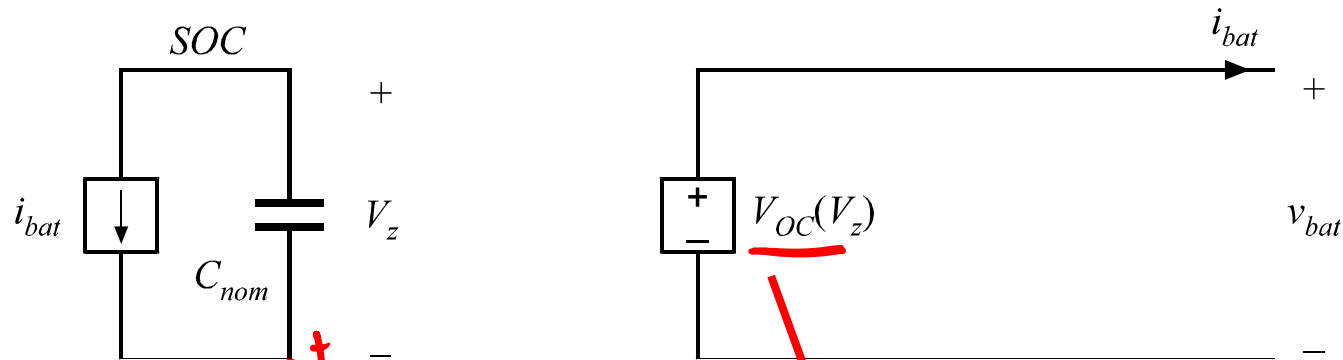
Model 0: Voltage Source



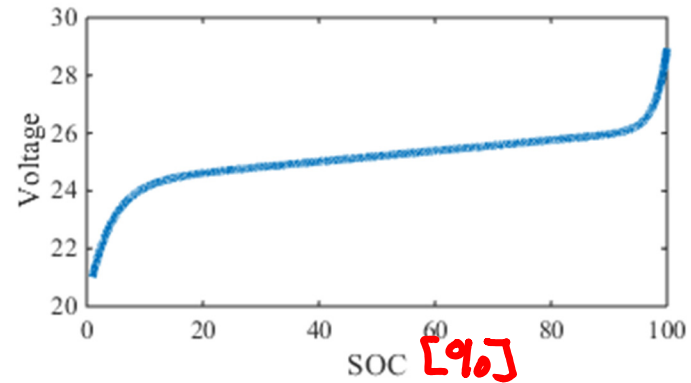
.tran 36000



Model A: SOC and V_{oc}

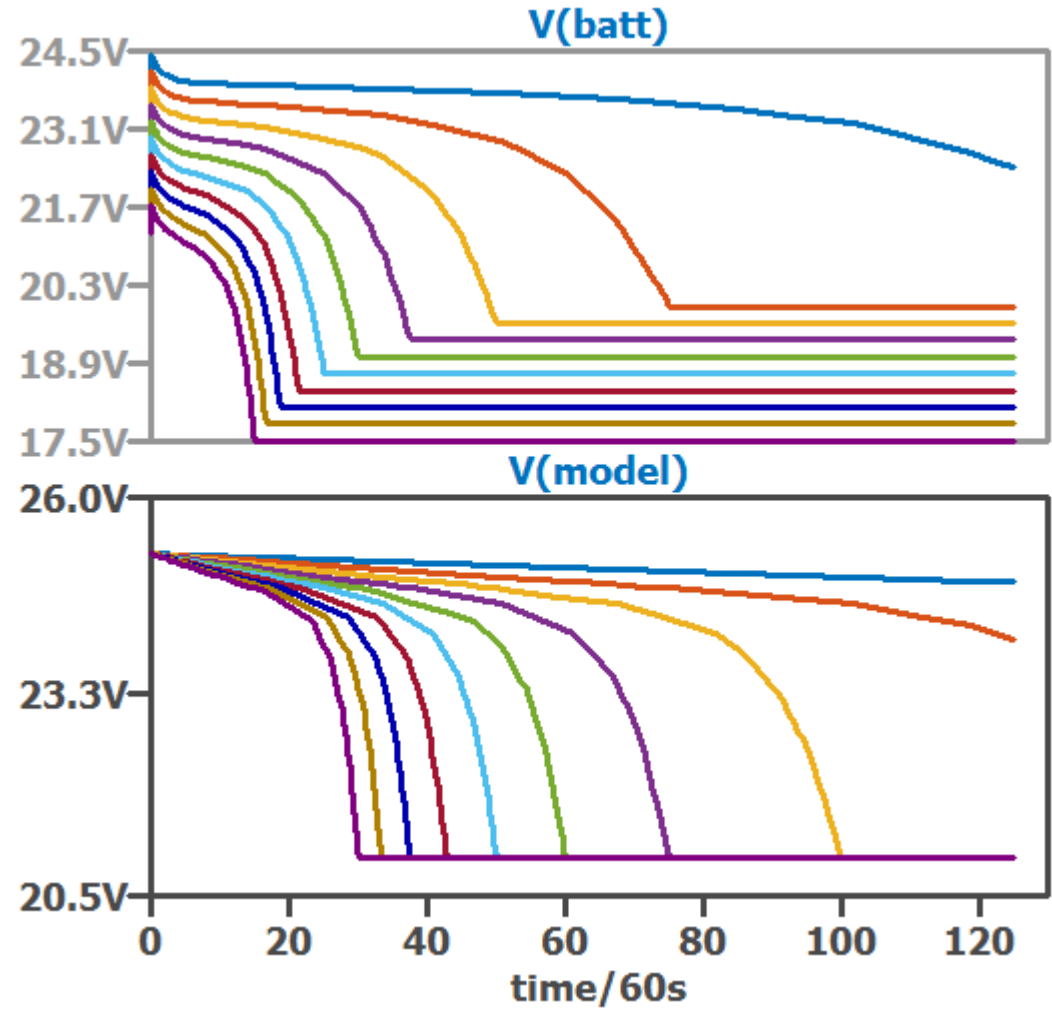
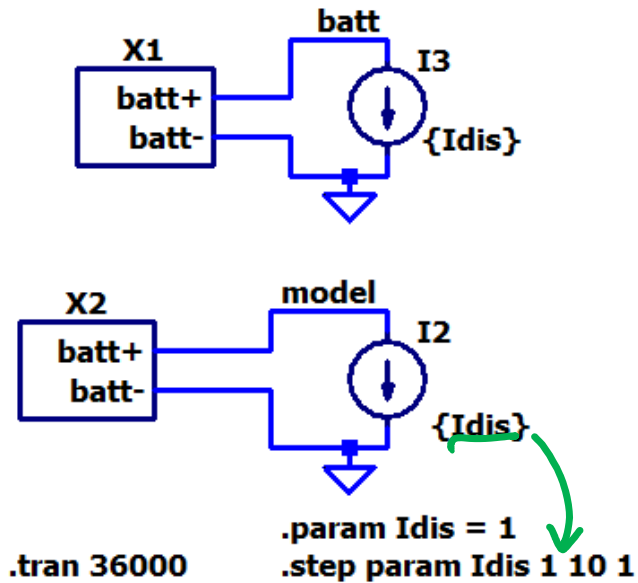


$V_z = V_{z\phi} - \frac{I}{C_{nom}} \int_0^t i_{bat} dt$
 A.S
 $\frac{A \cdot h}{C} = \Delta SOC$
 if I set $C_{nom} = C \cdot 3600$

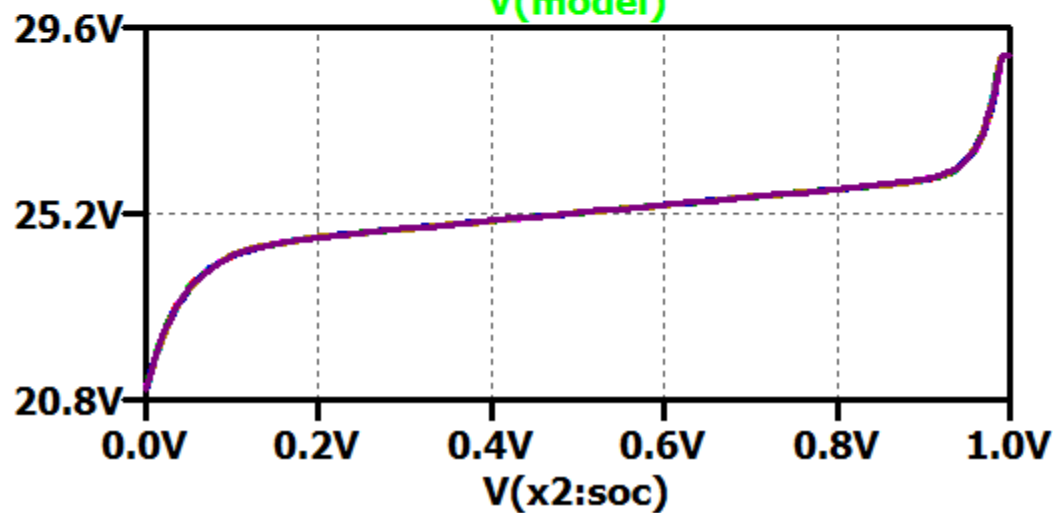
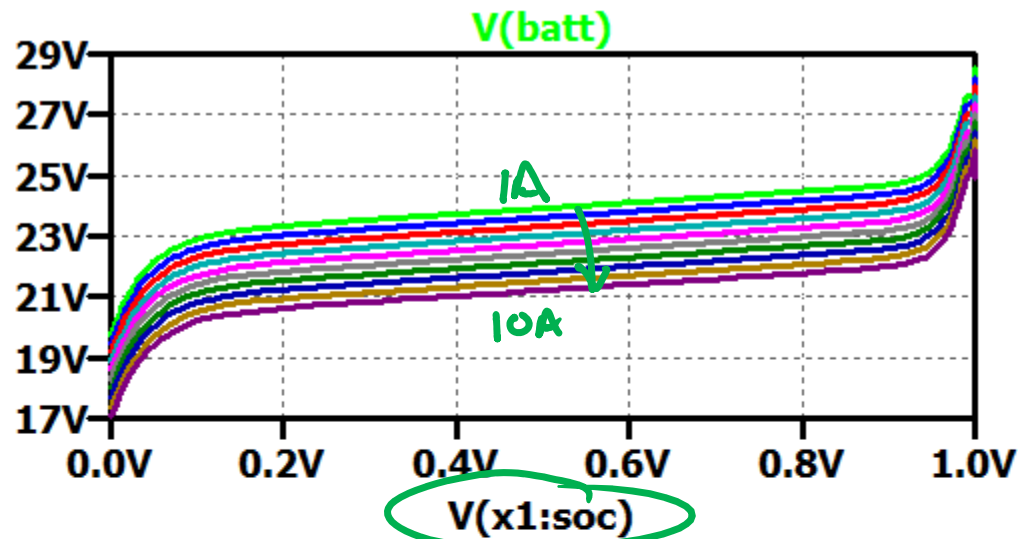
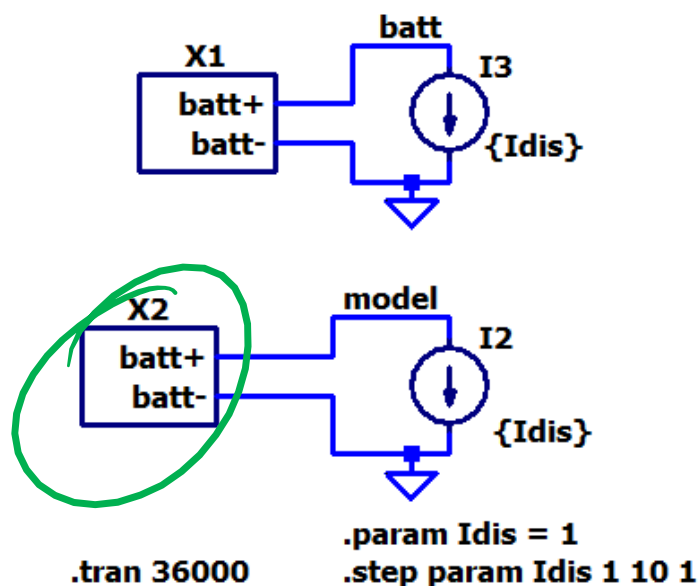


"state-of-charge"

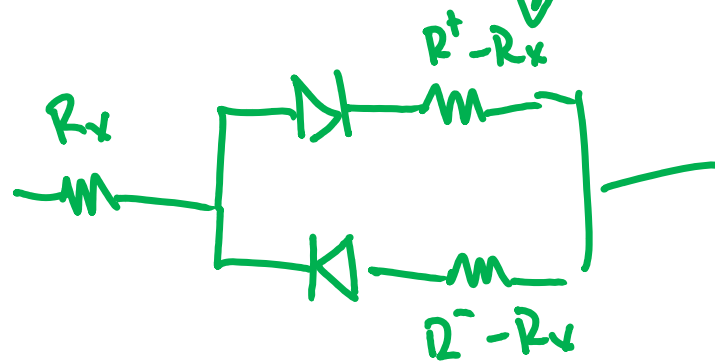
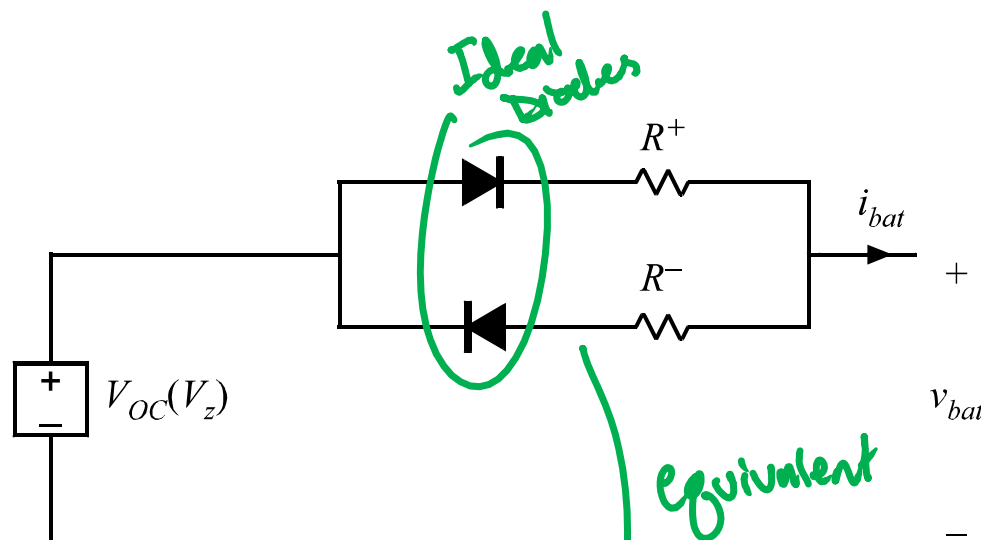
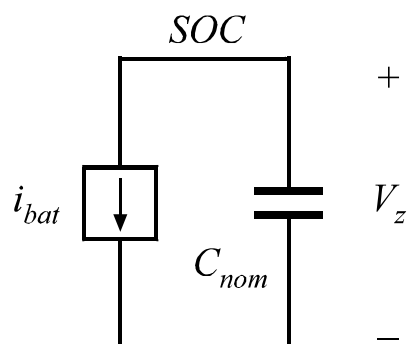
Model B: Series Resistance



Model B: Series Resistance

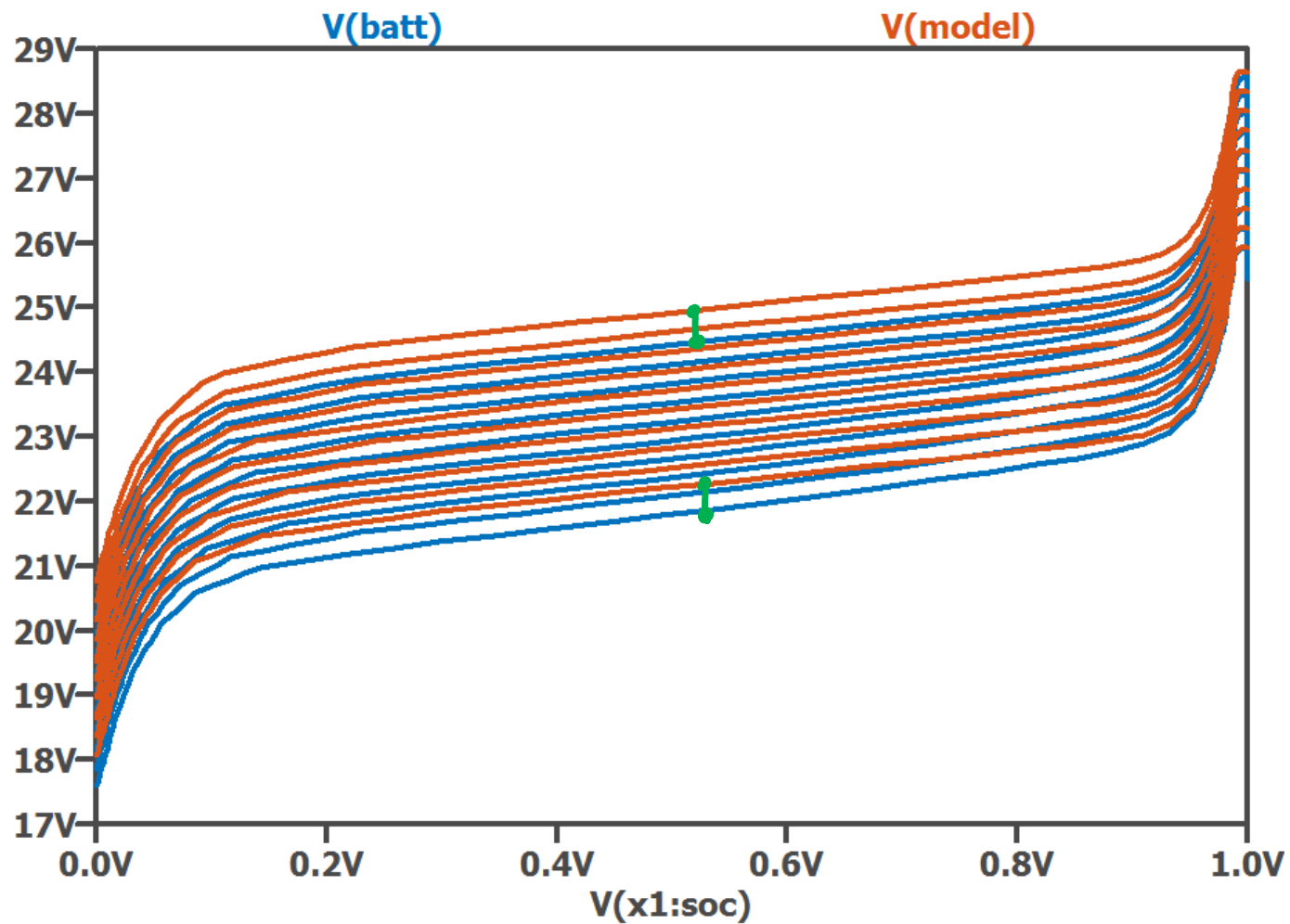


Model B: Series Resistance



if $R_x \leq \min(R^+, R^-)$

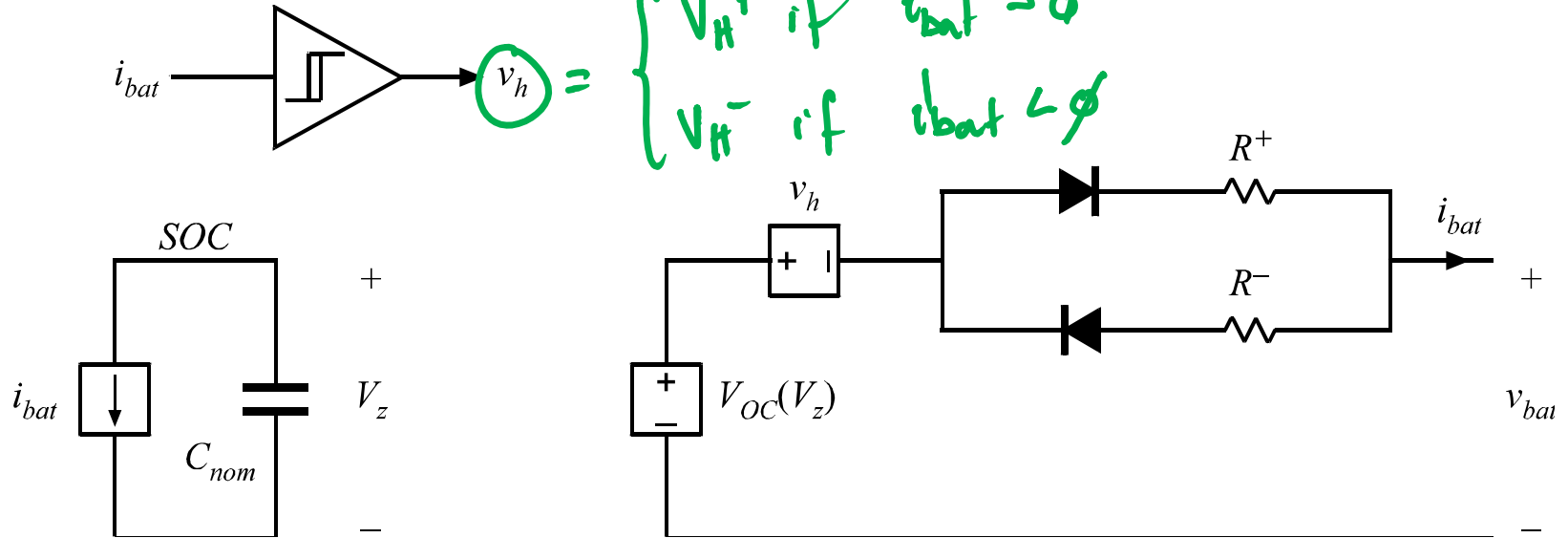
Model B Performance



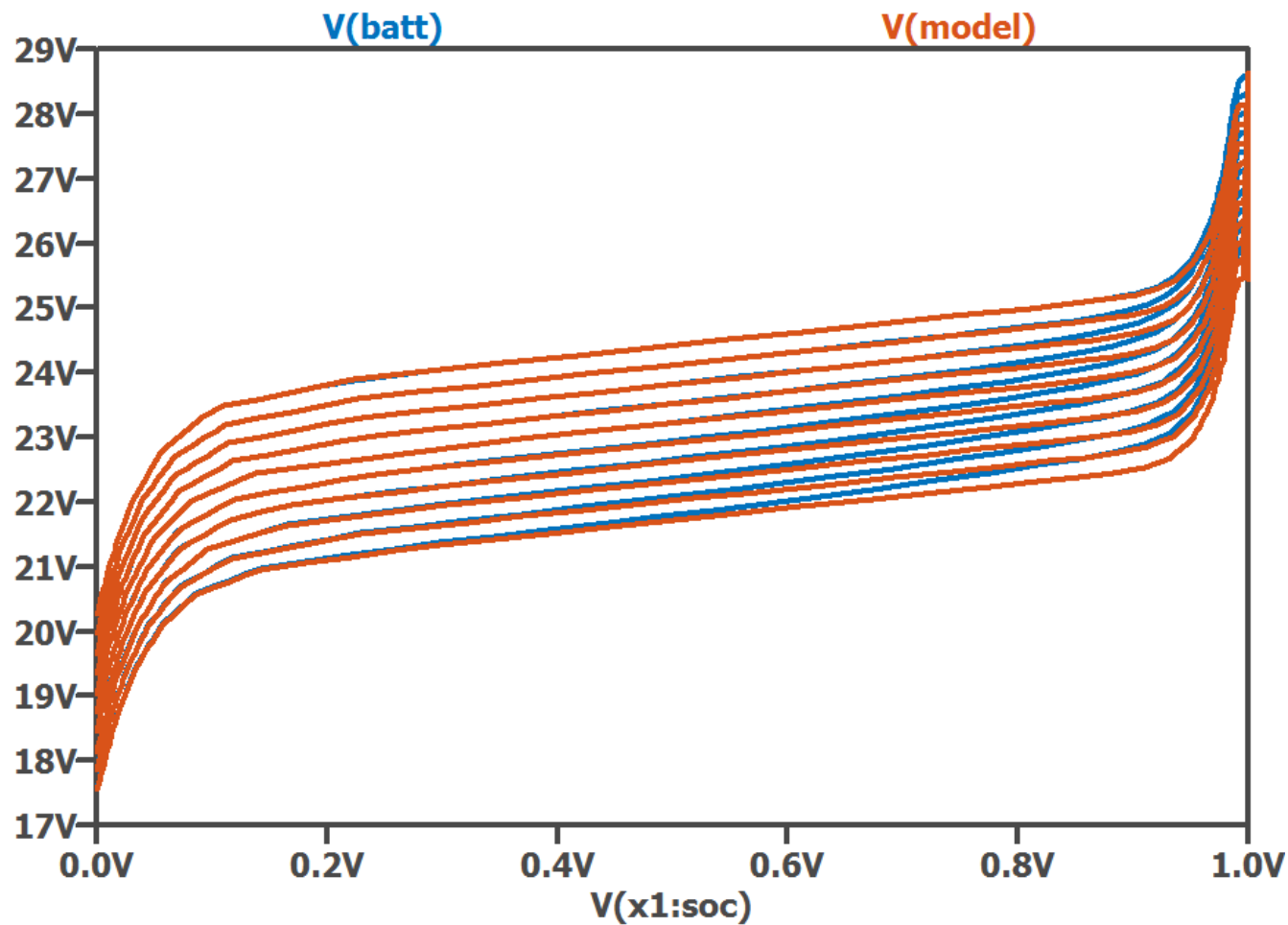
Model C: Zero-state Hysteresis

[Plett 2004]

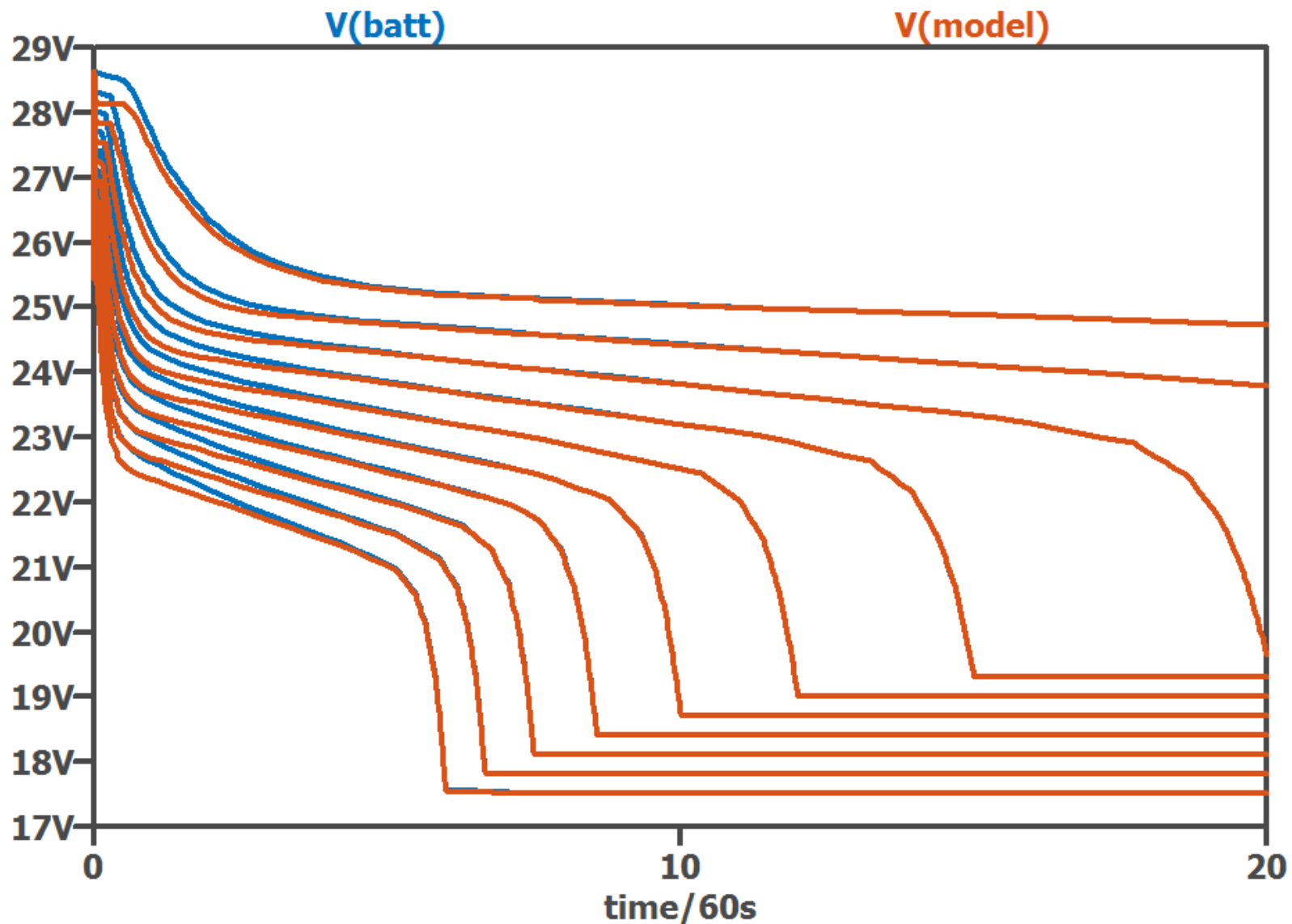
$$v_h = \begin{cases} V_H^+ & \text{if } i_{bat} > 0 \\ V_H^- & \text{if } i_{bat} < 0 \end{cases}$$



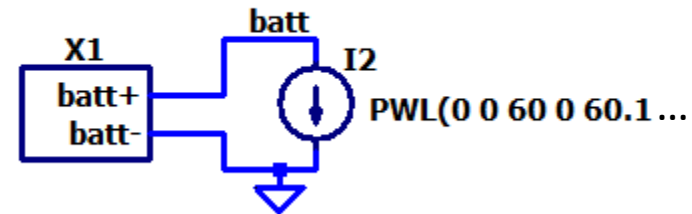
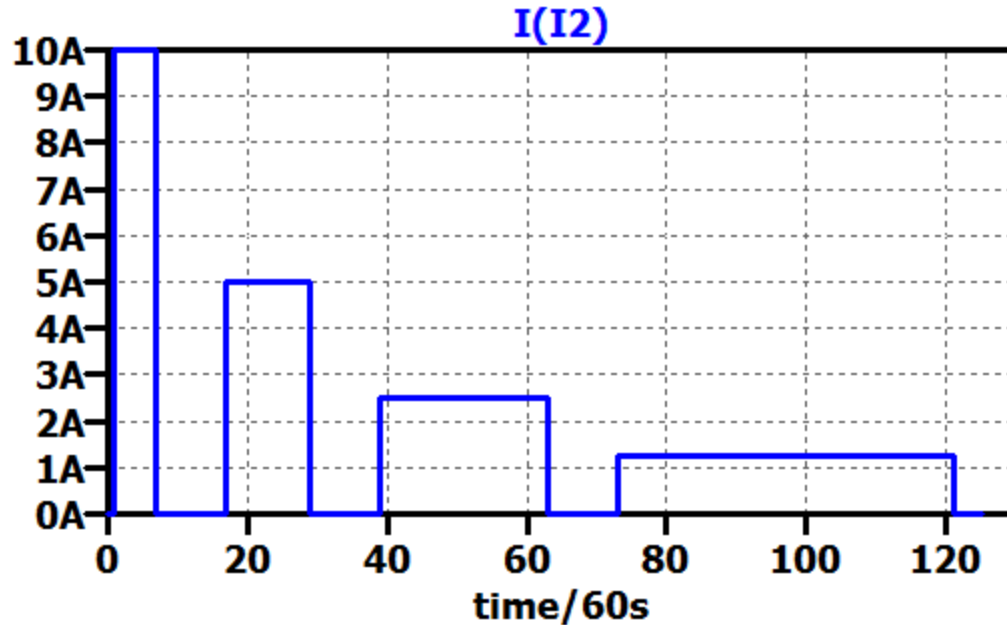
Model C Performance



Model C Performance



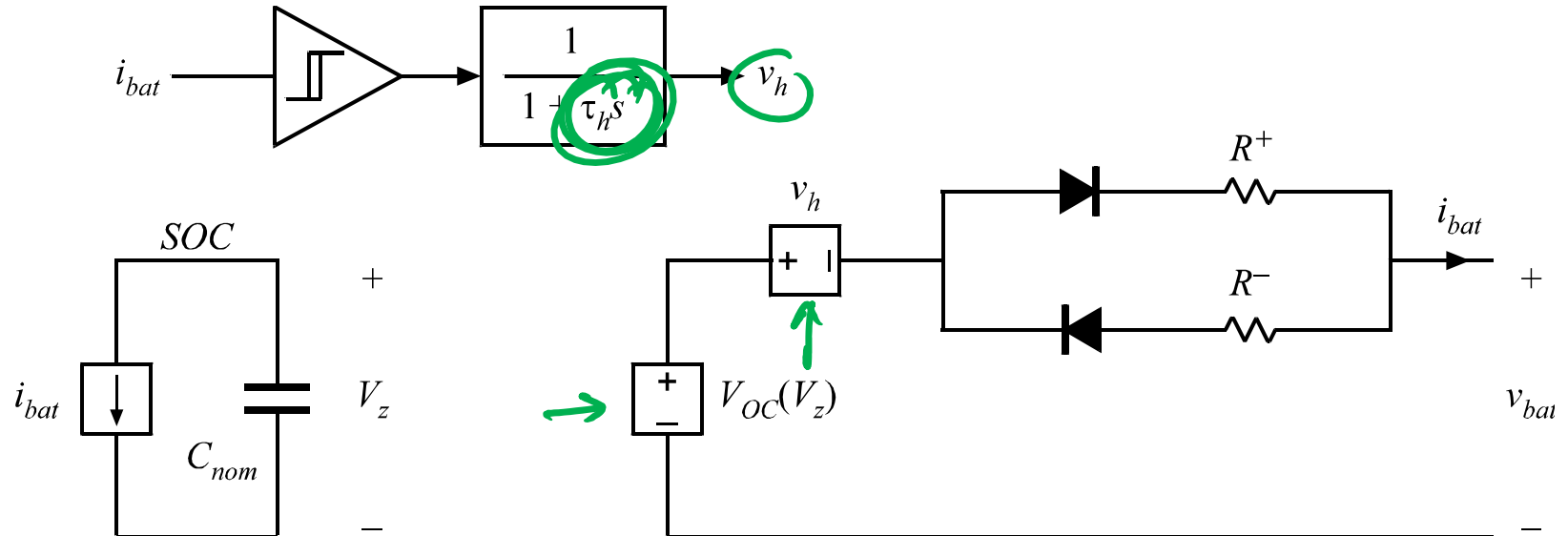
Dynamic Performance



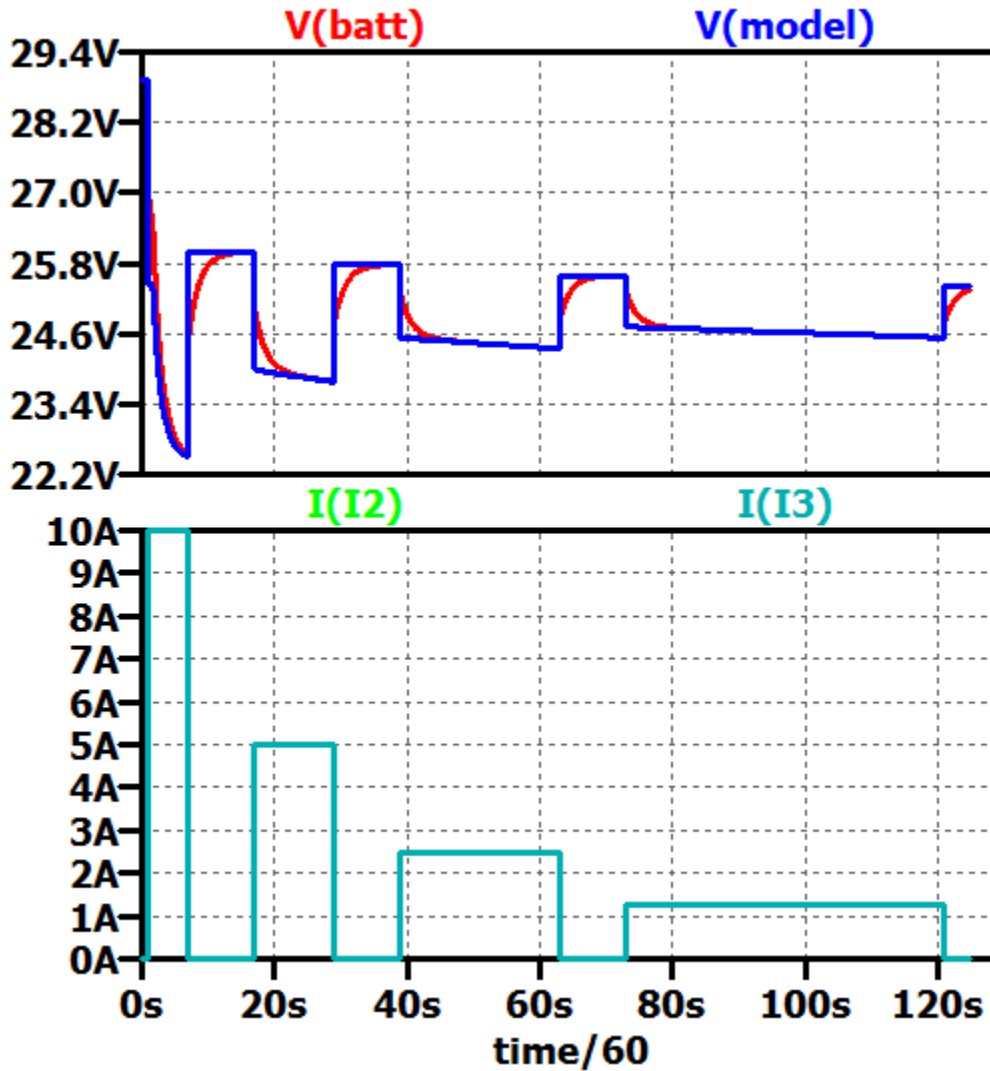
- Dynamic performance characterized by pulse train
- Constant percent of capacity per pulse [%Ahr] → not necessary

Model C1: One-state Hysteresis

[Plett 2004]

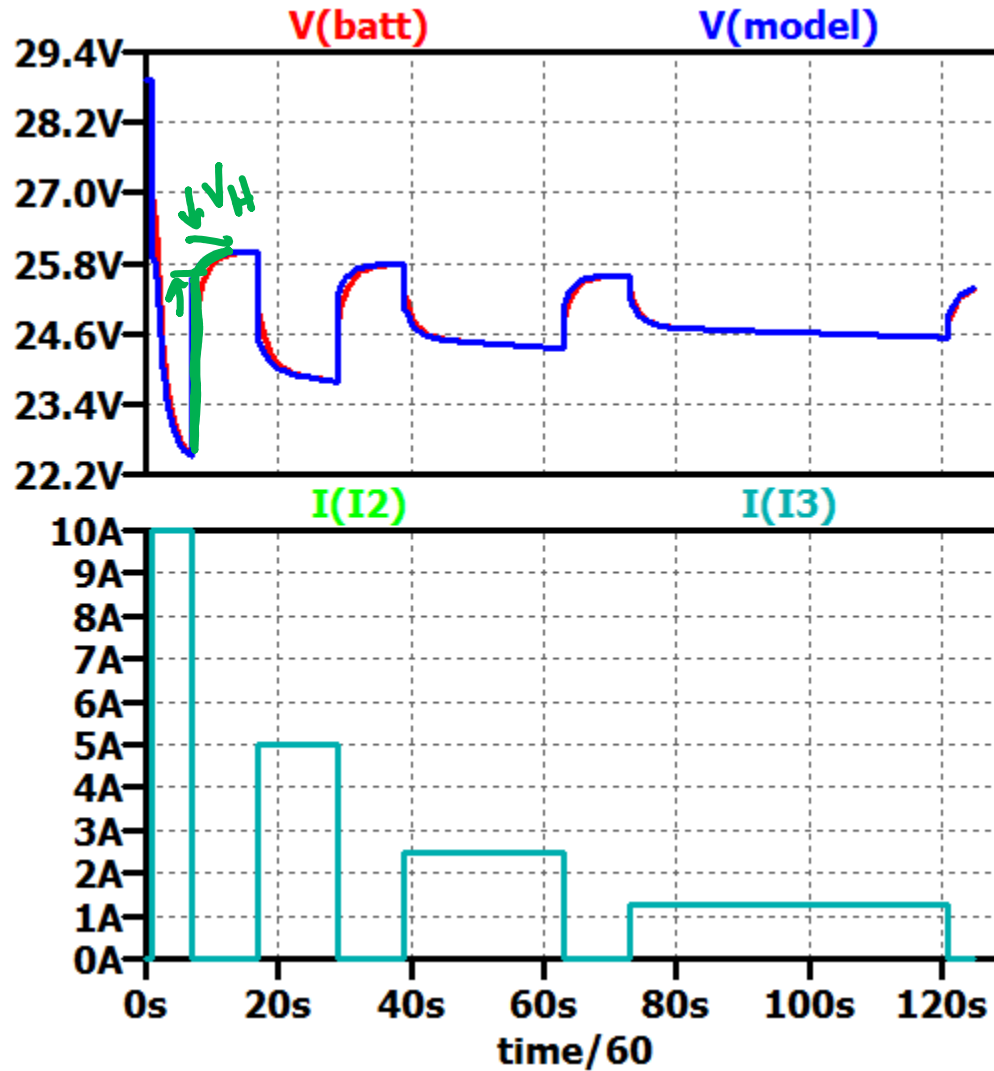


Model C1 Performance



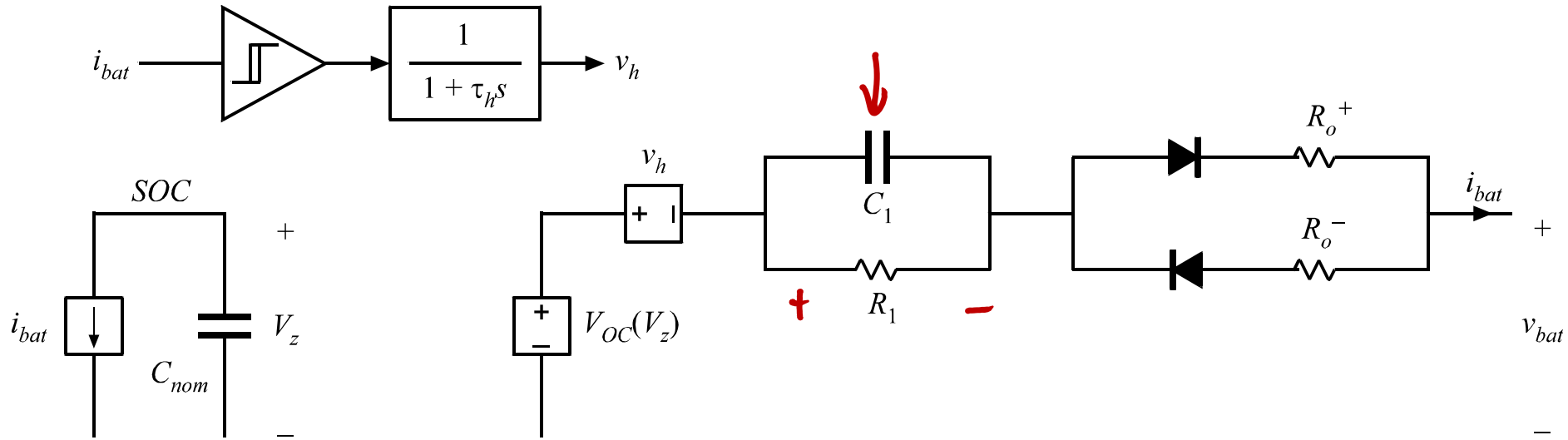
w/out
dynamics of
hysteresis

Model C1 Performance

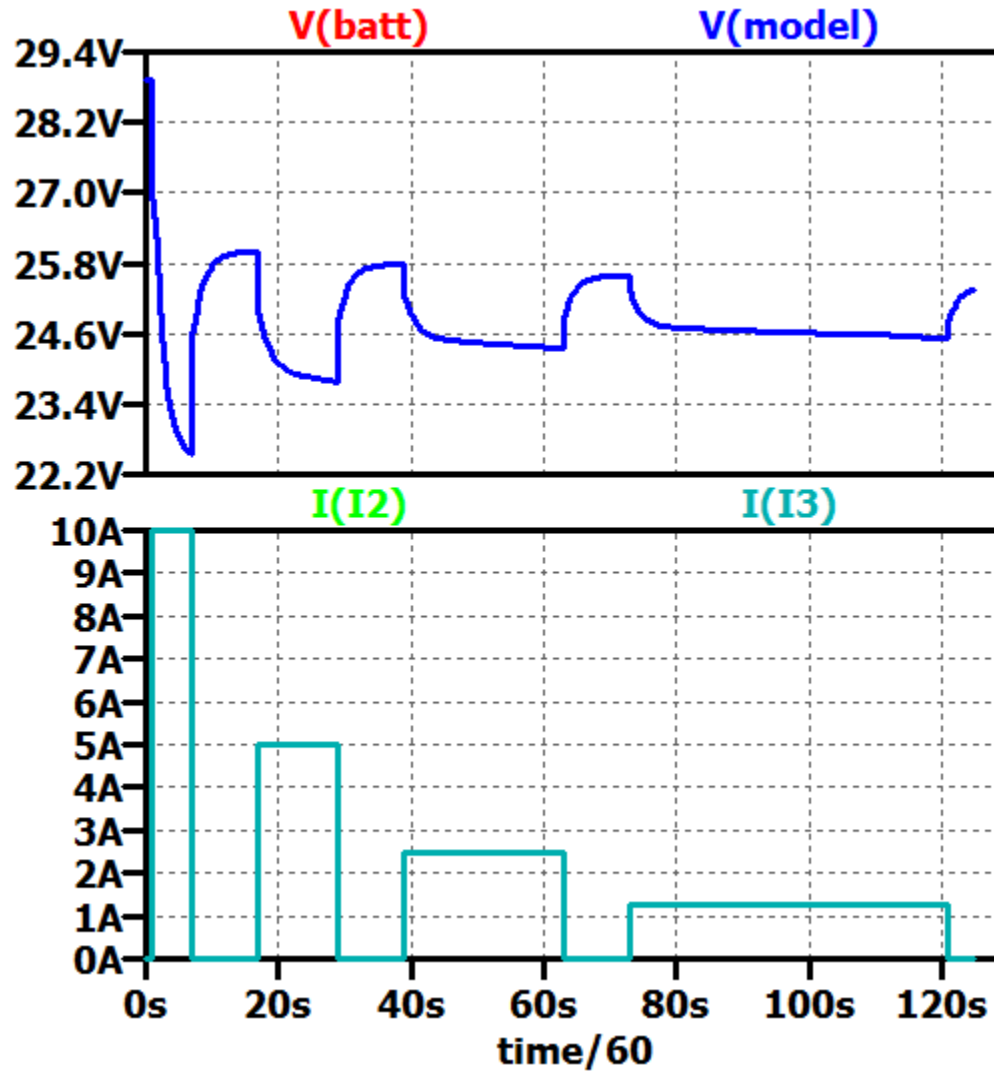


Model D: Diffusion (one-state)

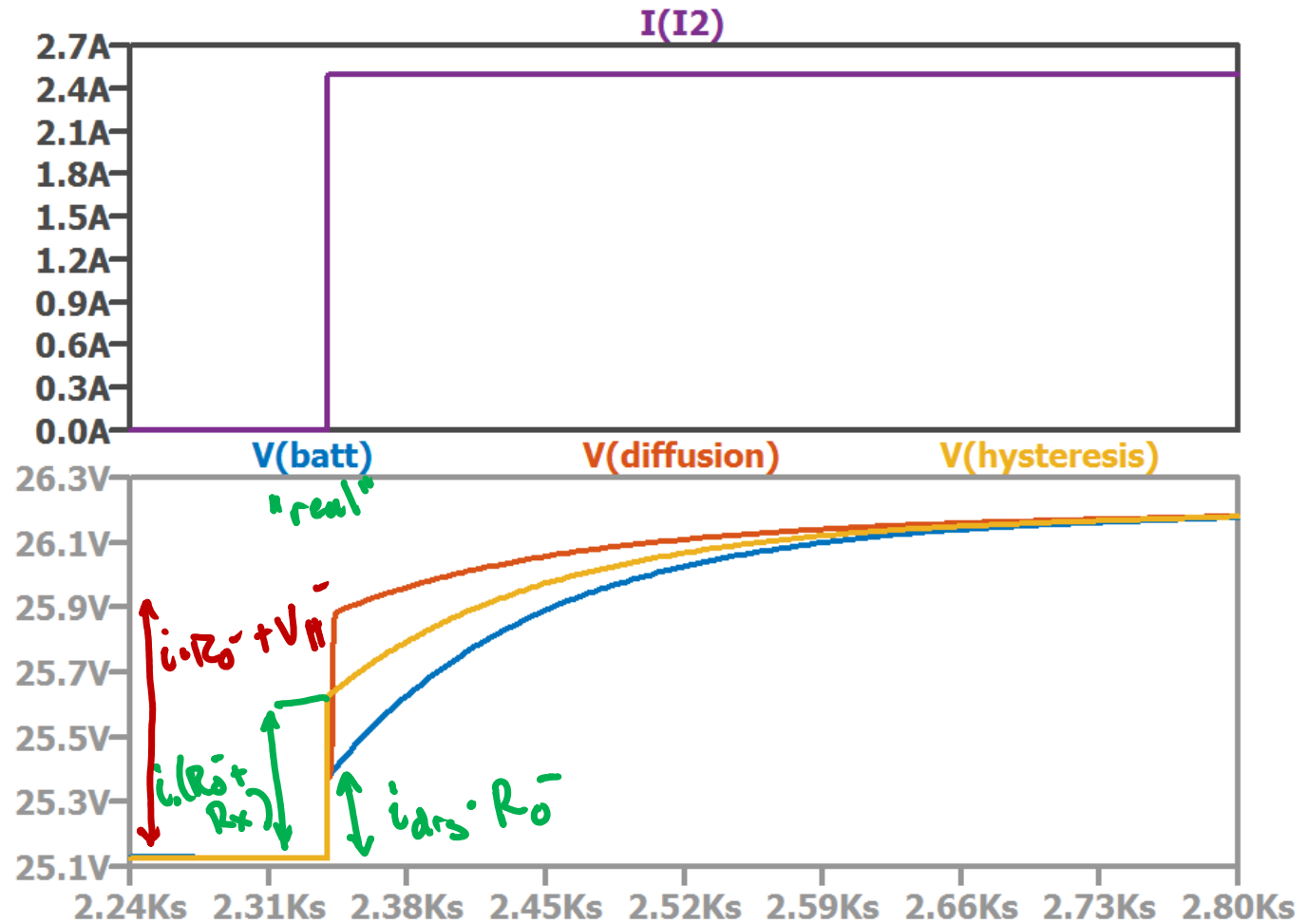
[Plett 2004]



Model D Performance

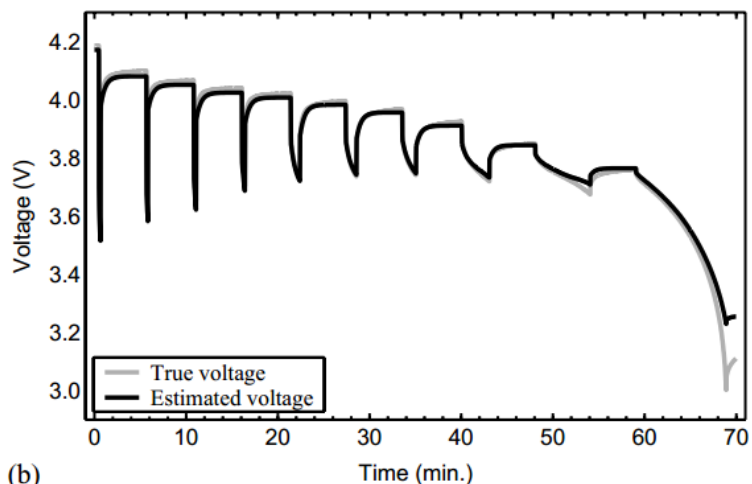


Diffusion Vs Hysteresis

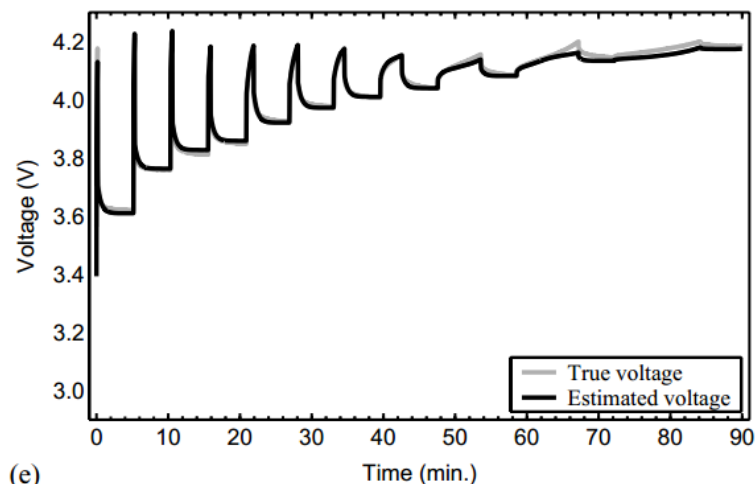


Experimental Results

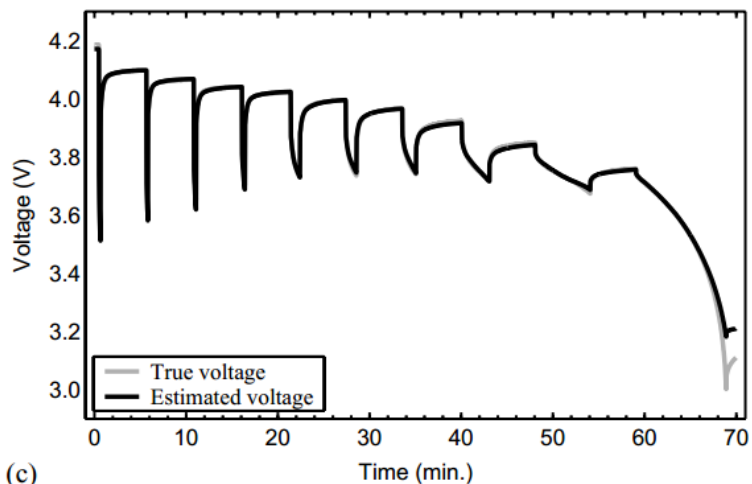
Modeling discharge: ESC, 2 filter states



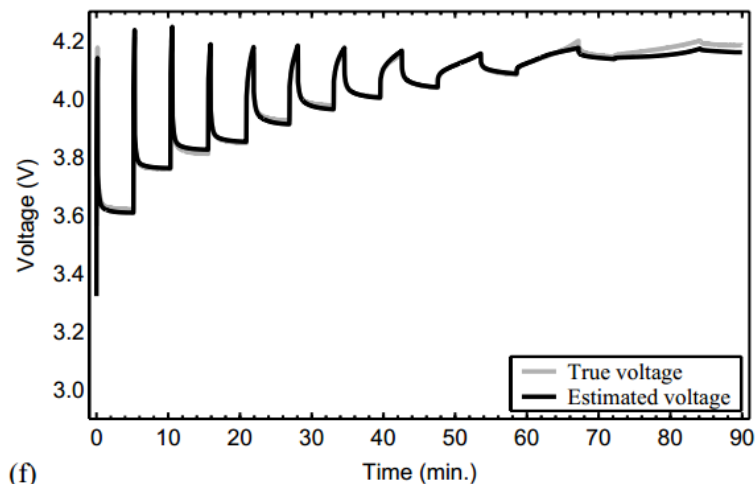
Modeling charge: ESC, 2 filter states



Modeling discharge: ESC, 4 filter states



Modeling charge: ESC, 4 filter states



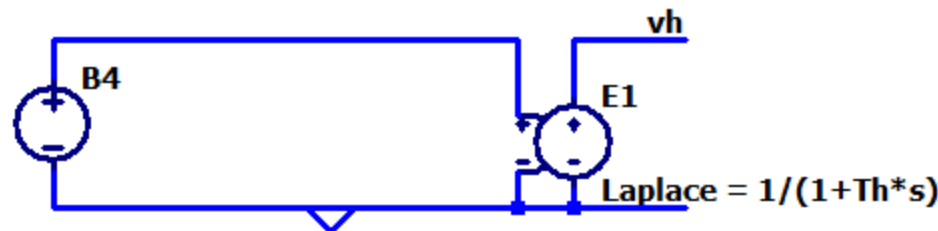
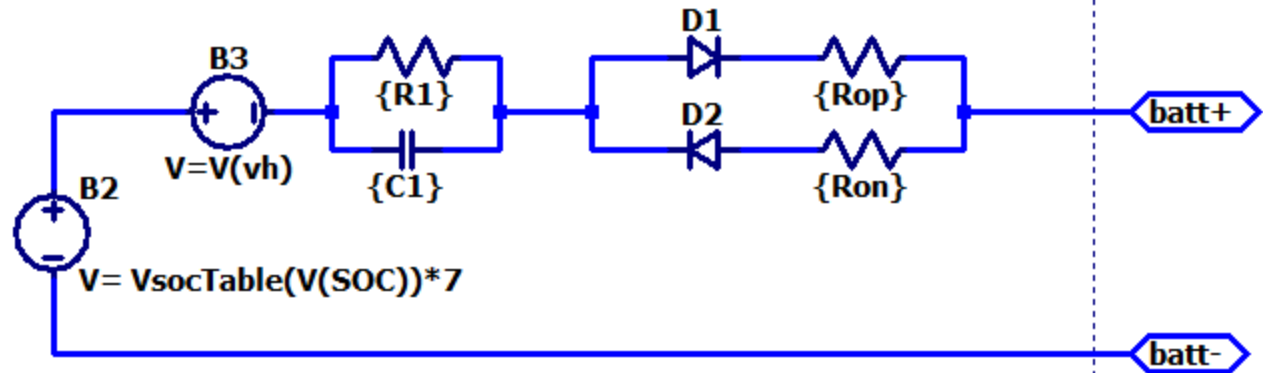
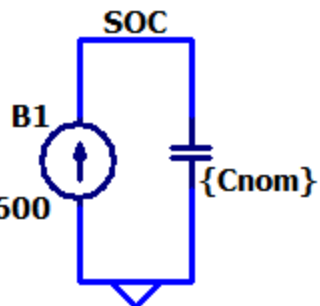
Implementation in LTSpice

.param R1 = 1m C1 = 10n

.model batdiode D(n=.001)
.param Rop = 1m Ron = 1m

.param VSOC0 = .5
.param Cnom = 10

.param Vh = 1 Th = 10



$V = Vh * (\text{IF}(I(B2) < -.1, 1, \text{IF}(I(B2) > .1, -1, 0)))$

.func VsocTable(x) = {table(x,0,3.0021, 0.01, 3.108, 0.02, 3.191, 0.03, 3.257, 0.04, 3.308, 0.05, 3.3...