

Introduction to Battery Modeling

Cell Equivalent-Circuit Models

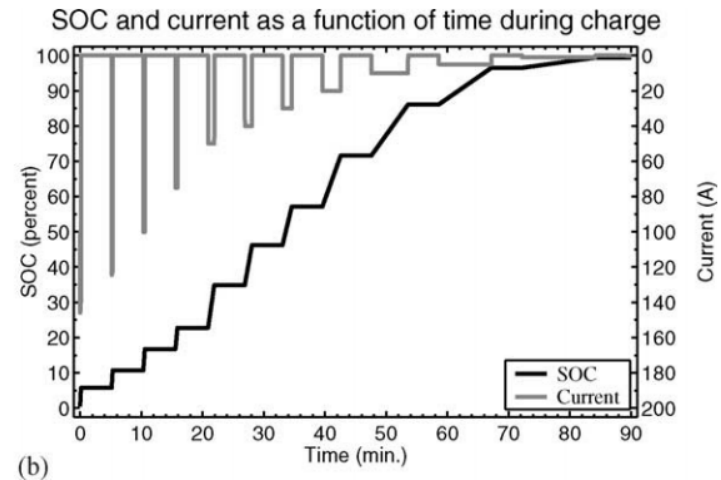
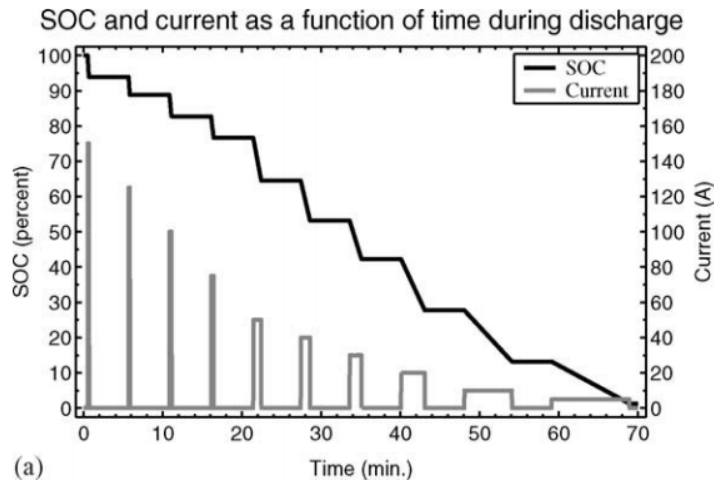
Objective:

- Dynamic circuit model capable of predicting cell voltage in response to charge/discharge current, temperature

Further key techniques discussed in [Plett 2004-Part 2] and [Plett 2004-Part 3]

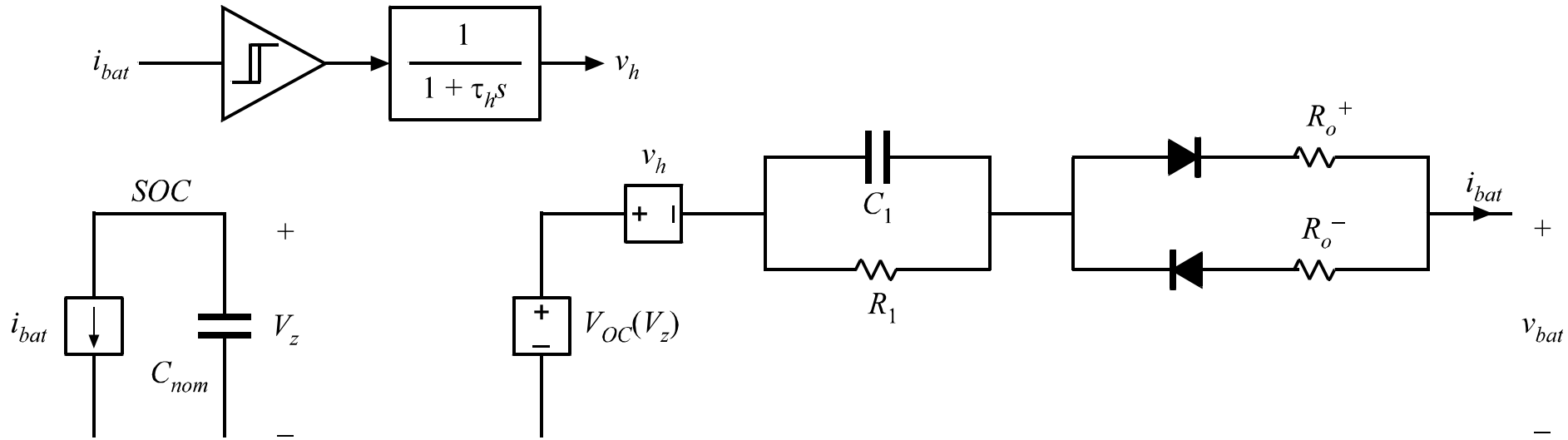
- Model parameters found using least-square estimation or Kalman filter techniques based on experimental test data
- Run-time estimation of state of charge (SOC)

Approach: Pulsed current tests



Model D: Diffusion (one-state)

[Plett 2004]



Battery Nomenclature

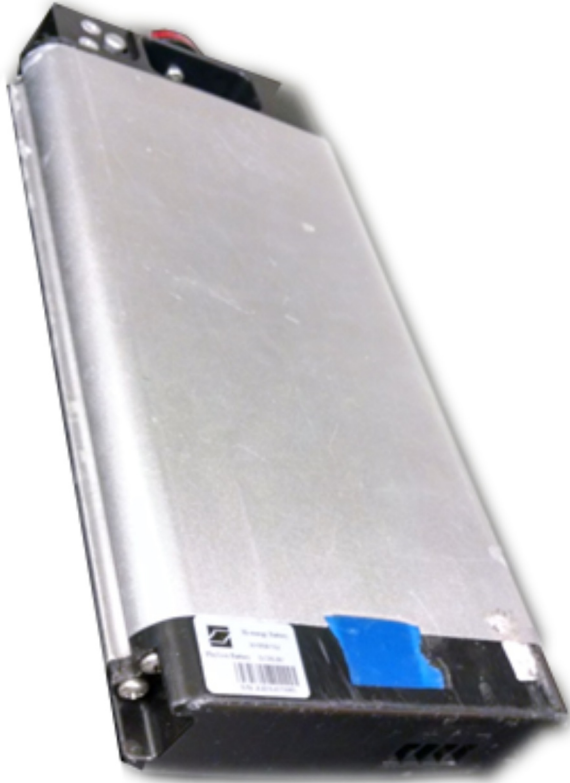
- Known beforehand:

Capacity C [Ah] \rightarrow May degrade over time
Nominal Voltage V_{nom} [V]

Max Discharge Rate } Specified as "C" rate
Max Charge Rate } - what current will completely charge / discharge the battery in 1 hr

ex
For a 10 Ah = C cell,
a 2C discharge rate means 20A max discharge
A 0.5C charge rate means 5A max charge current

Example Battery



Battery packs characterized by arrangement of cells
 " $N_s S N_p P$ "
 $N_s = \#$ of cells in series
 $N_p = \#$ of cells in parallel

ex $7s5p \rightarrow 7$ in series, 5 in parallel
 35 total cells in the pack

Pack voltage determined by $\#$ of cells in series
 Pack capacity determined by $\#$ in parallel

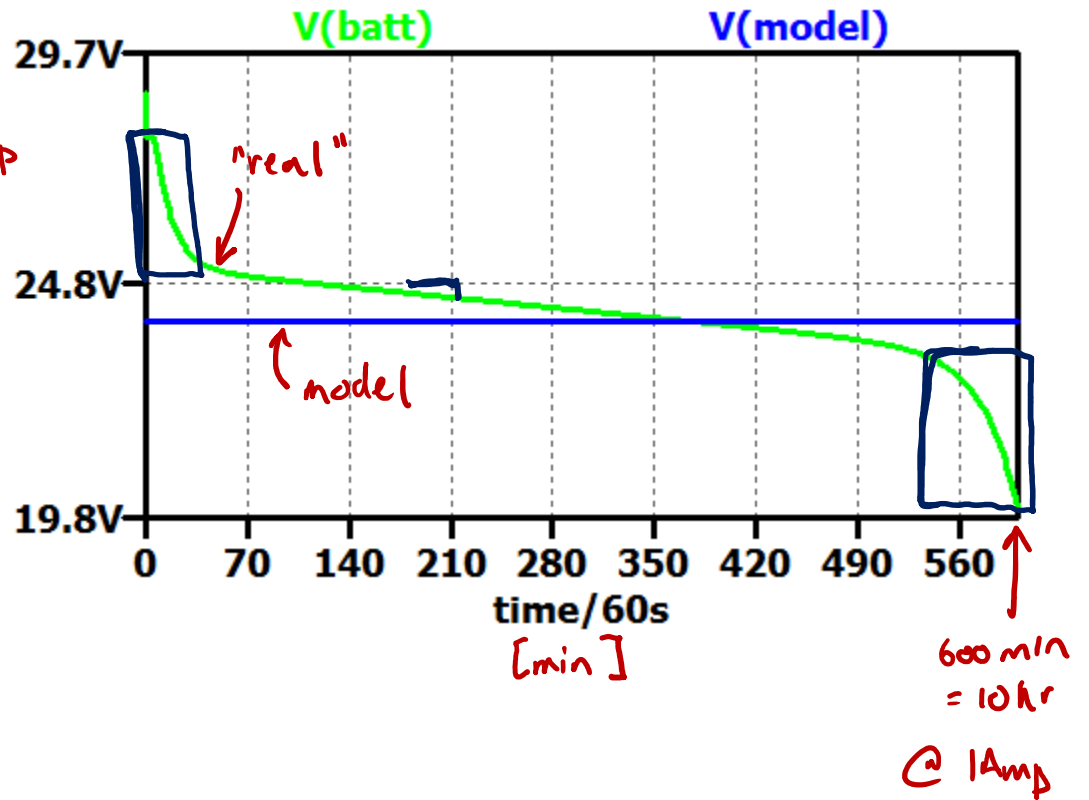
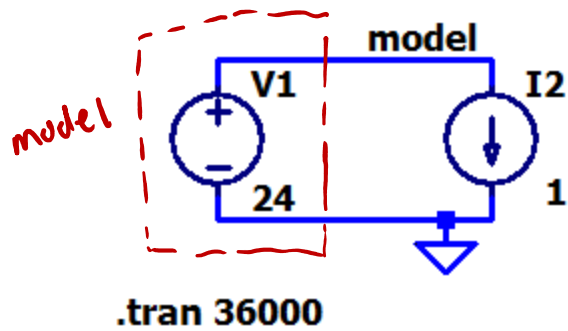
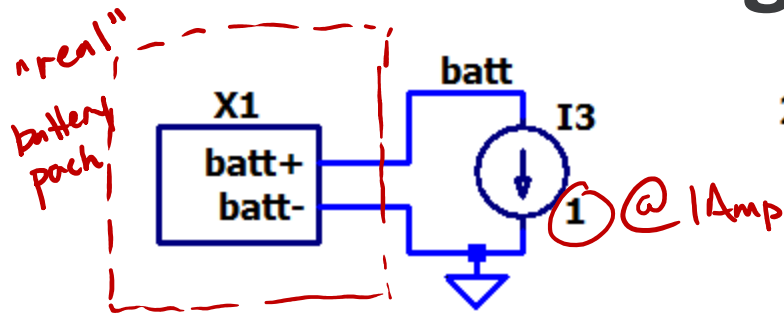
ex cells have

- $V_{nom} = 3.4V$
- $C = 2Ah$
- max charge: $0.2C = 0.8A$
- max discharge: $1.9C = 3.8A$

A $7s5p$ pack will have

- $V_{nom} = 23.8V$
- $C = 10Ah$
- max charge: $0.2C = 4A$
- max discharge: $1.9C = 19A$

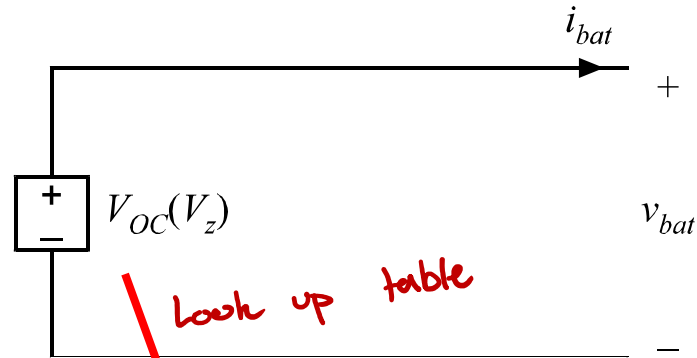
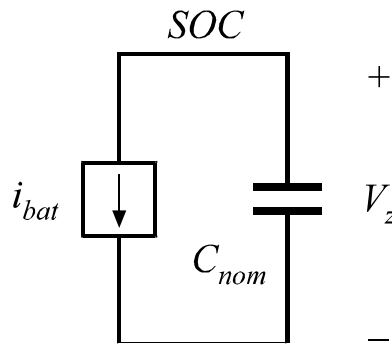
Model 0: Voltage Source



$C = 10Ah$

- Revise model to include charge - dependent voltage

Model A: SOC and V_{oc}



Battery current integrator

$$V_z = V_{z0} - \frac{1}{C_{nom}} \int_0^t i_{bat} dt$$

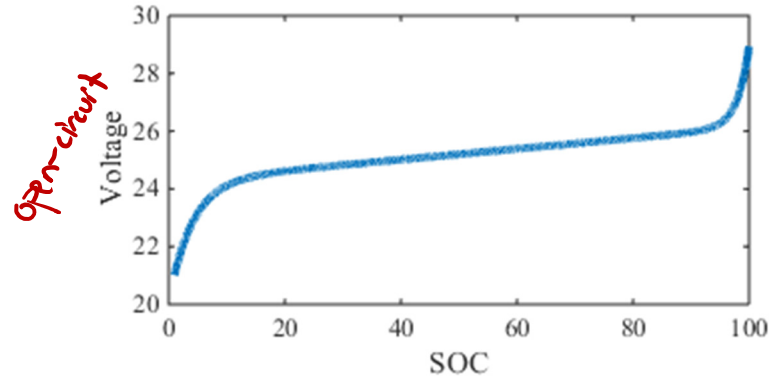
\uparrow i.e. total charge in/out in A·s

scale factor

If we set $C_{nom} = C \cdot 3600 \frac{\text{sec}}{\text{hr}}$

$0 \leq V_z \leq 1 \rightarrow$ proportion of full capacity remaining

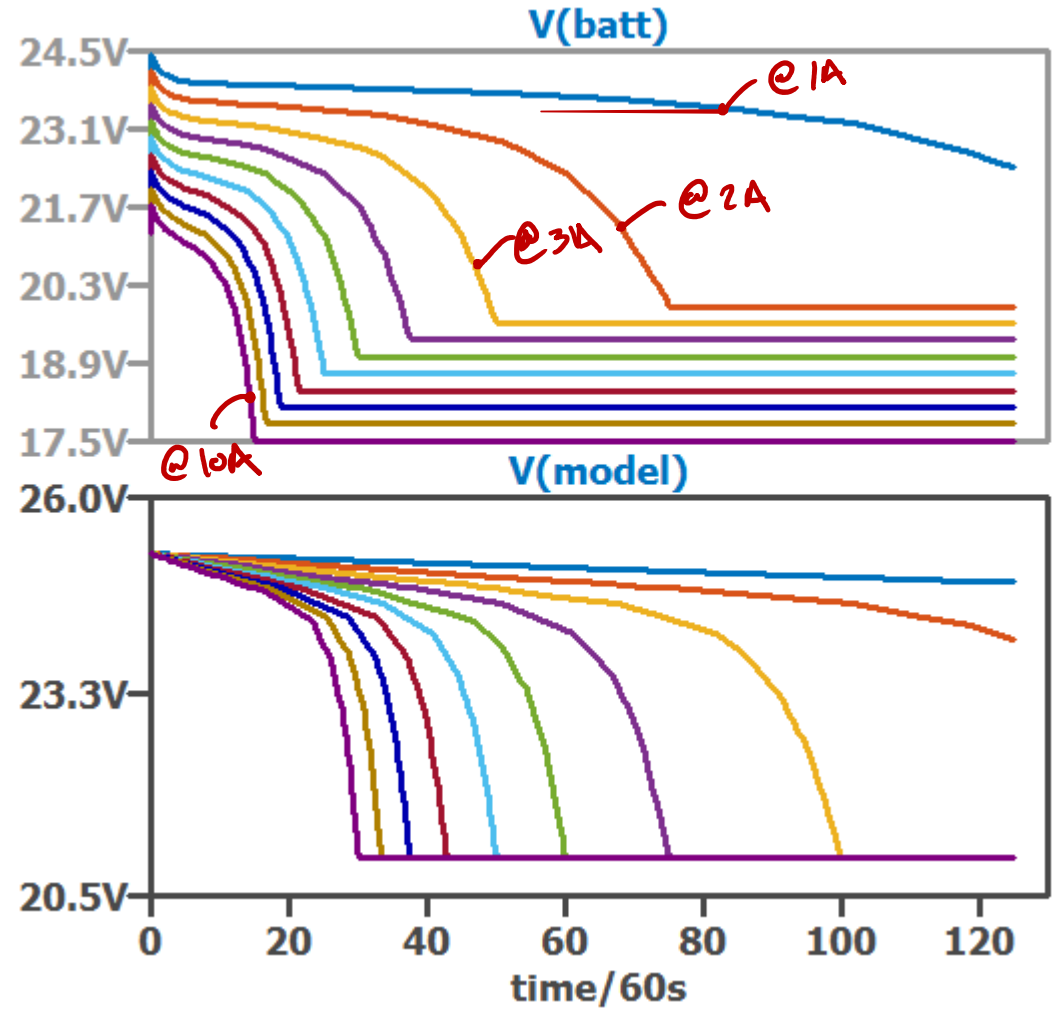
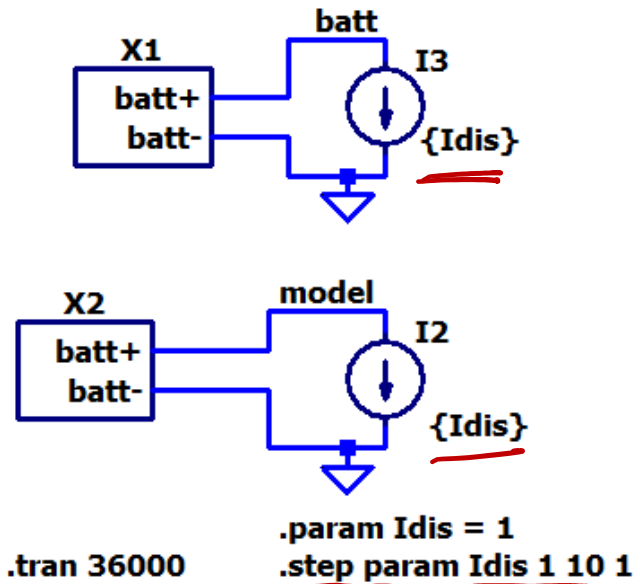
look up table



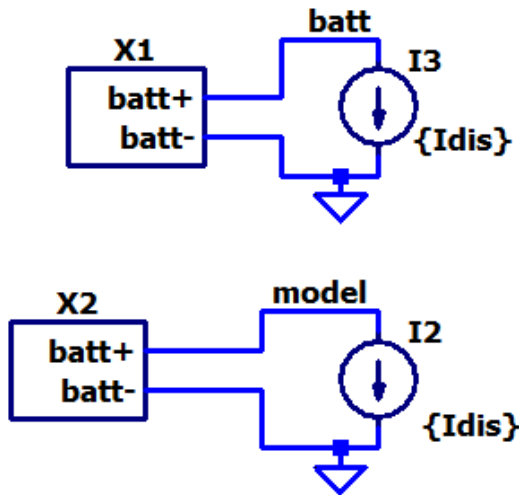
open-circuit

State-of-charge [%]

Model B: Series Resistance



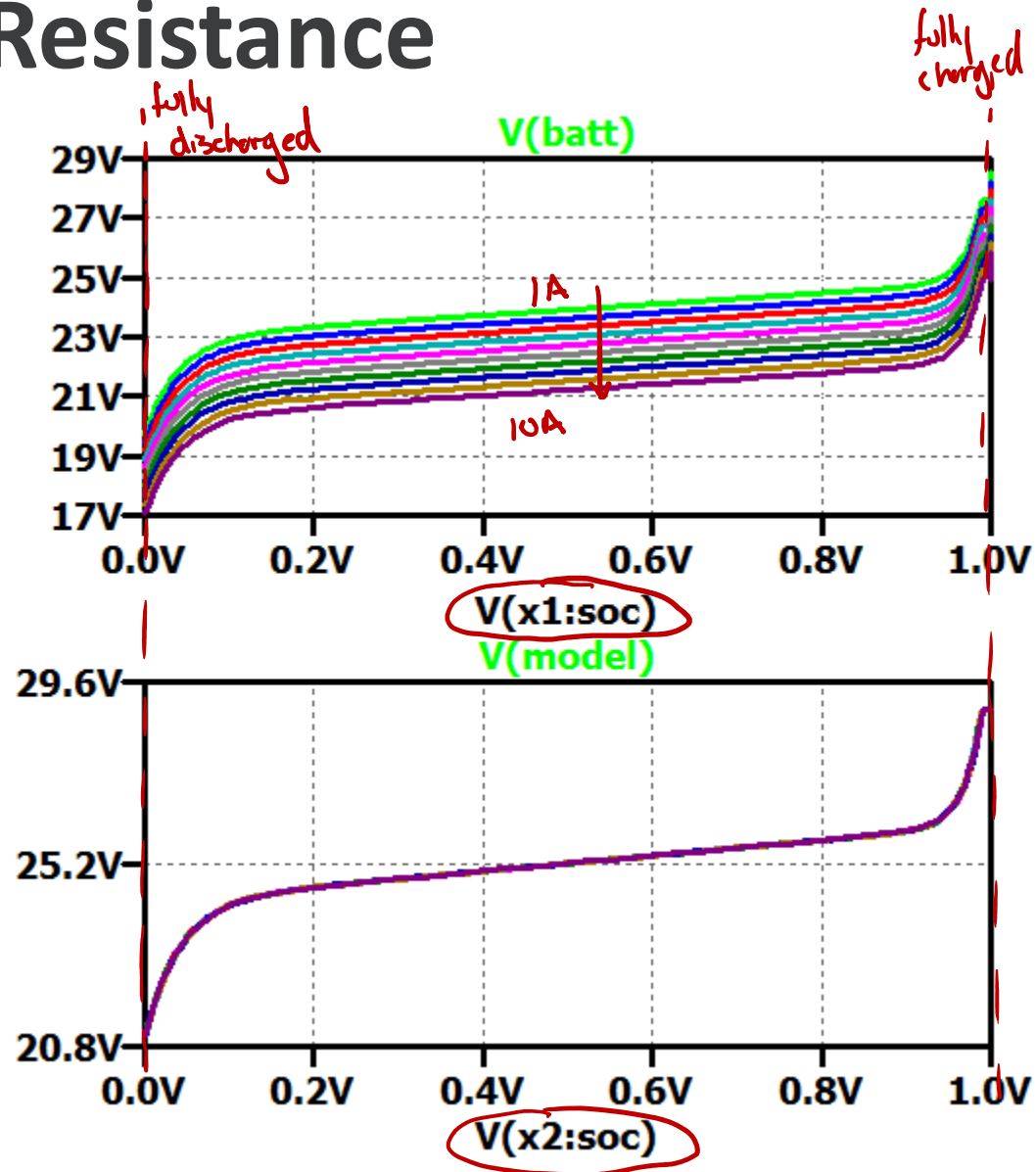
Model B: Series Resistance



```
.tran 36000
.param Idis = 1
.step param Idis 1 10 1
```

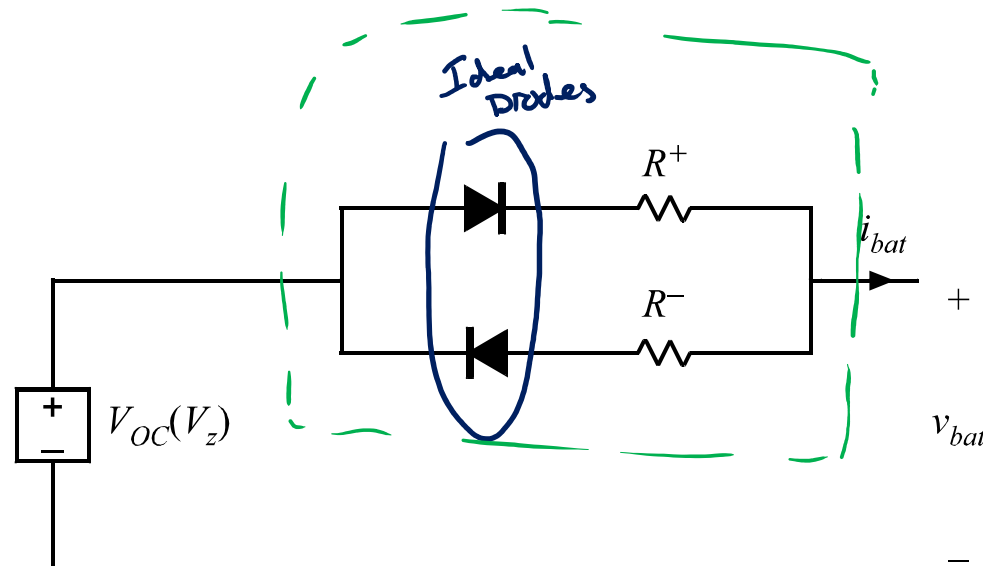
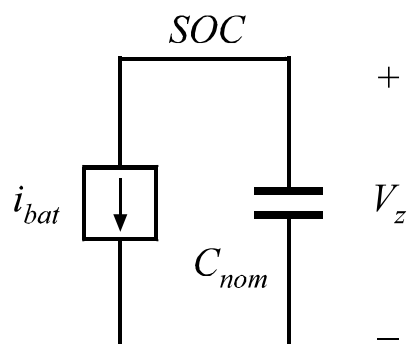
offset in pack voltage proportional to discharging current

$$\Delta V = I_{dis} (R)$$



plotting vs soc instead of time

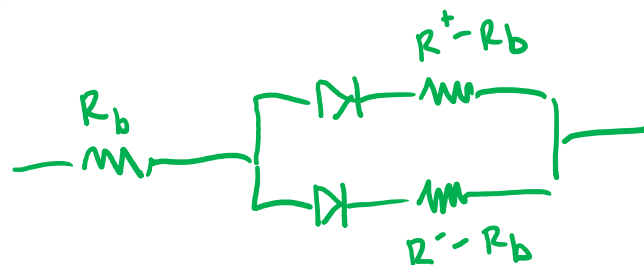
Model B: Series Resistance



R^+ = discharging resistance

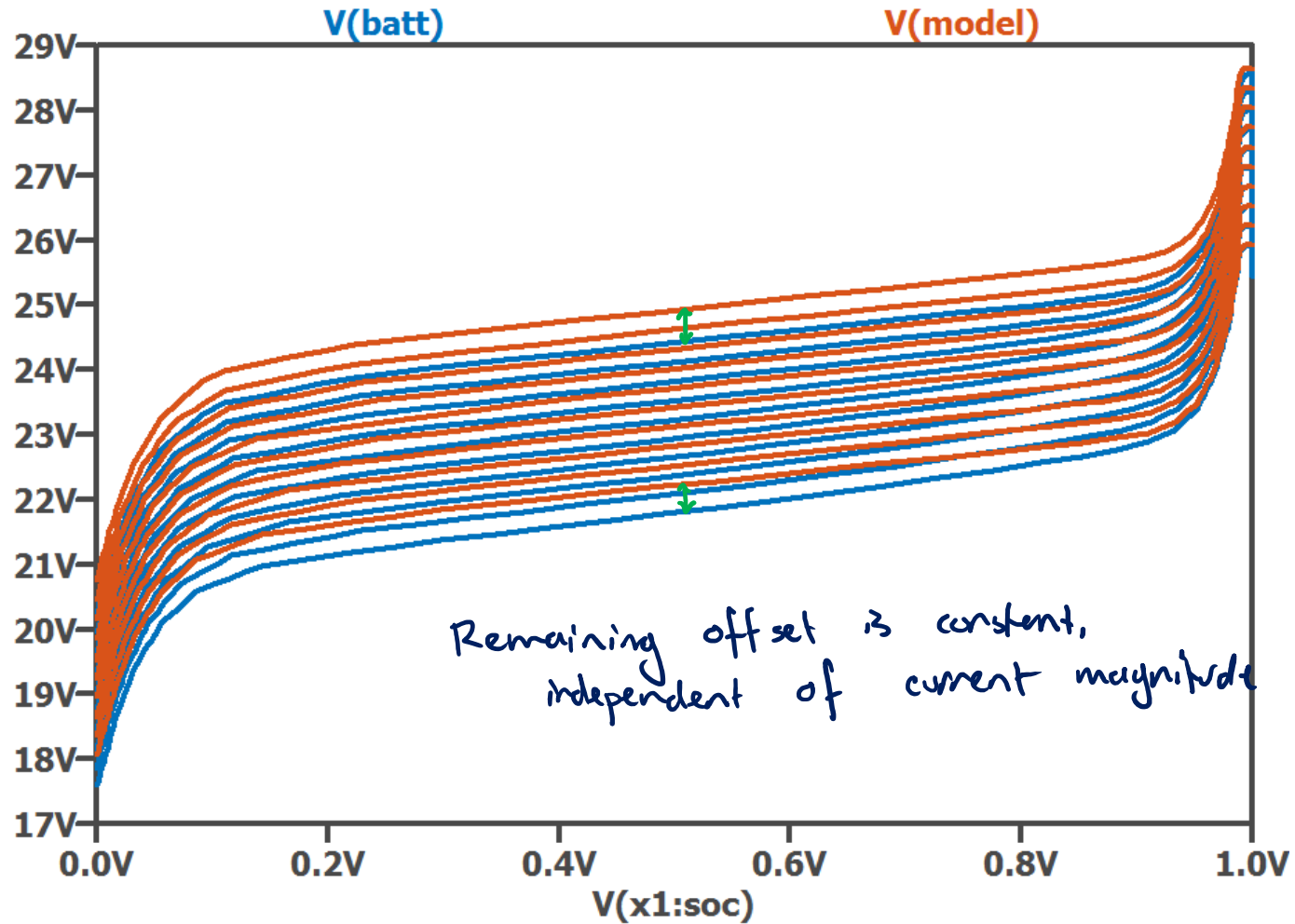
R^- = charging resistance

Equivalent Model

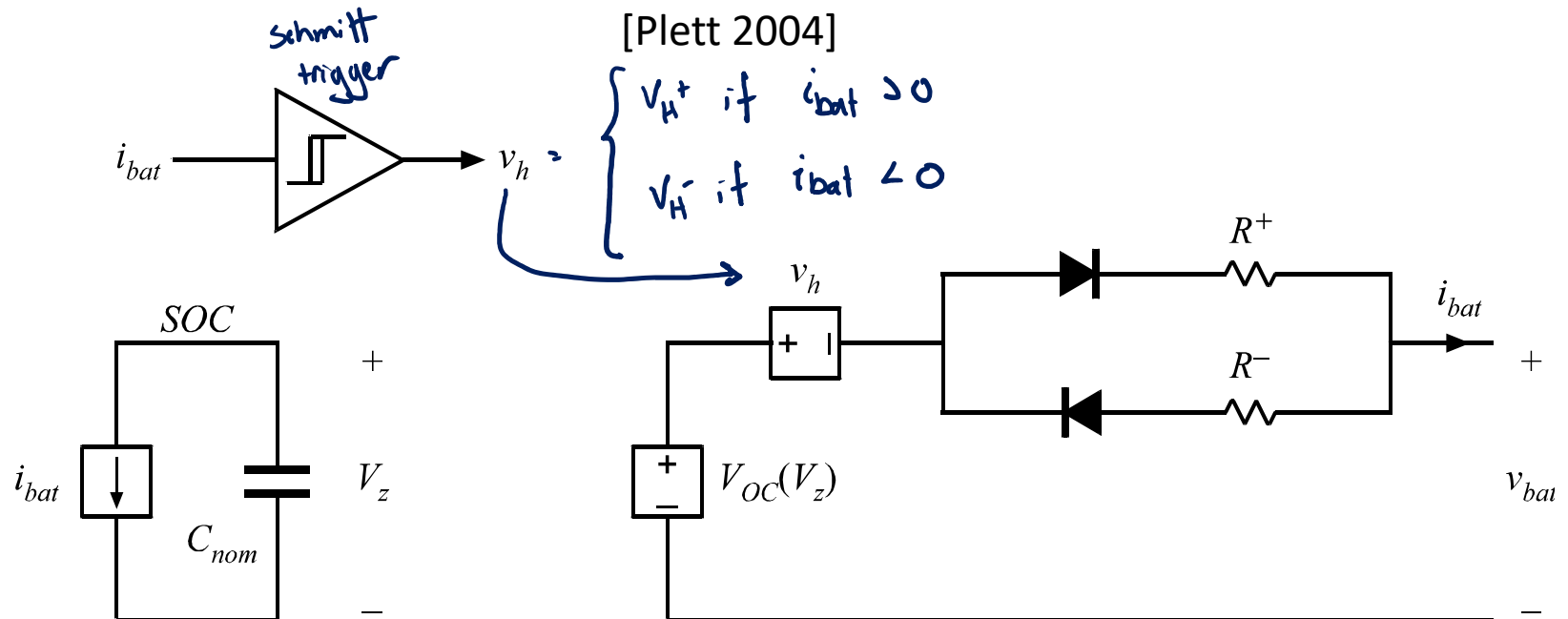


$$R_b \leq \min(R^+, R^-)$$

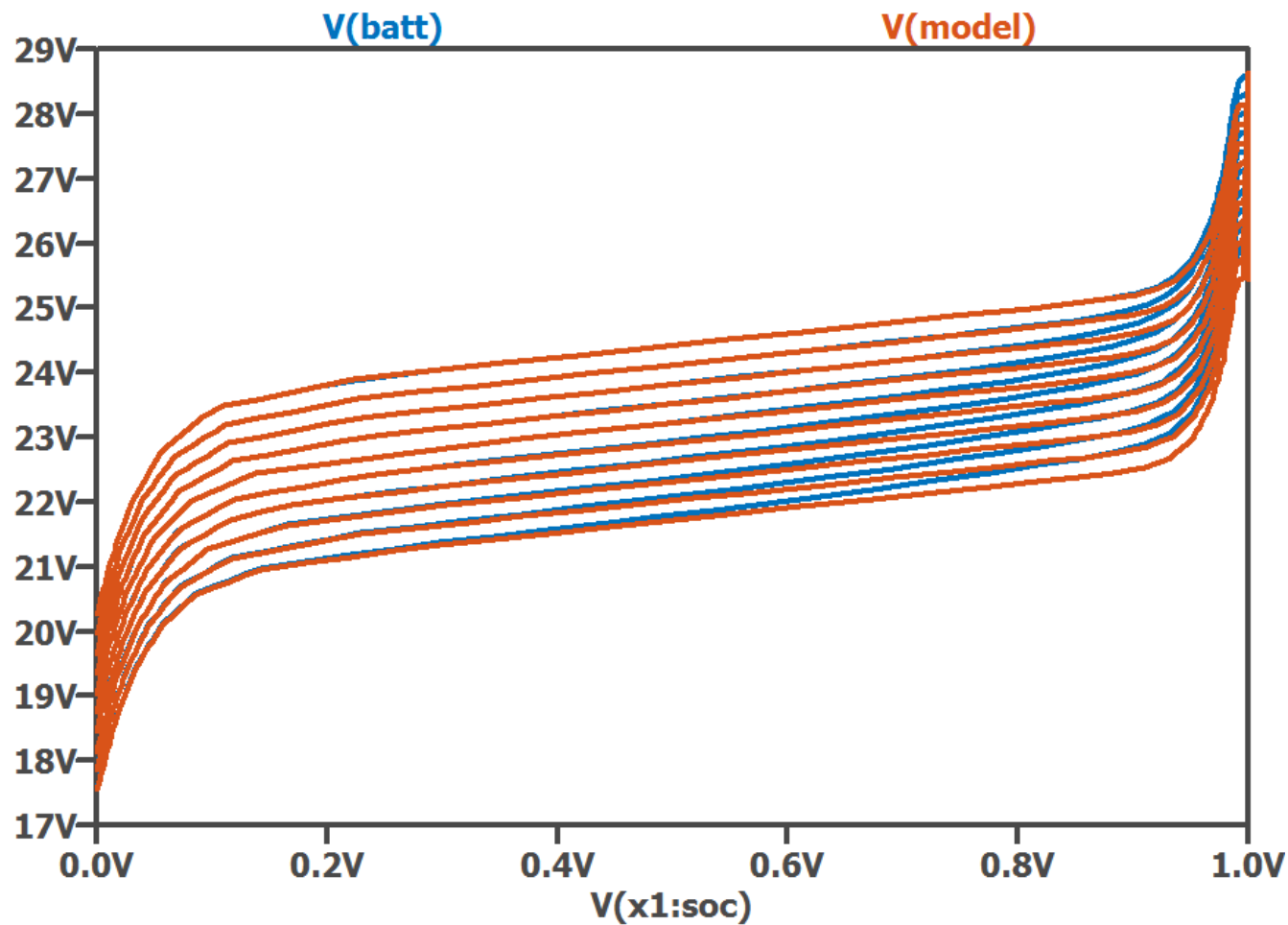
Model B Performance



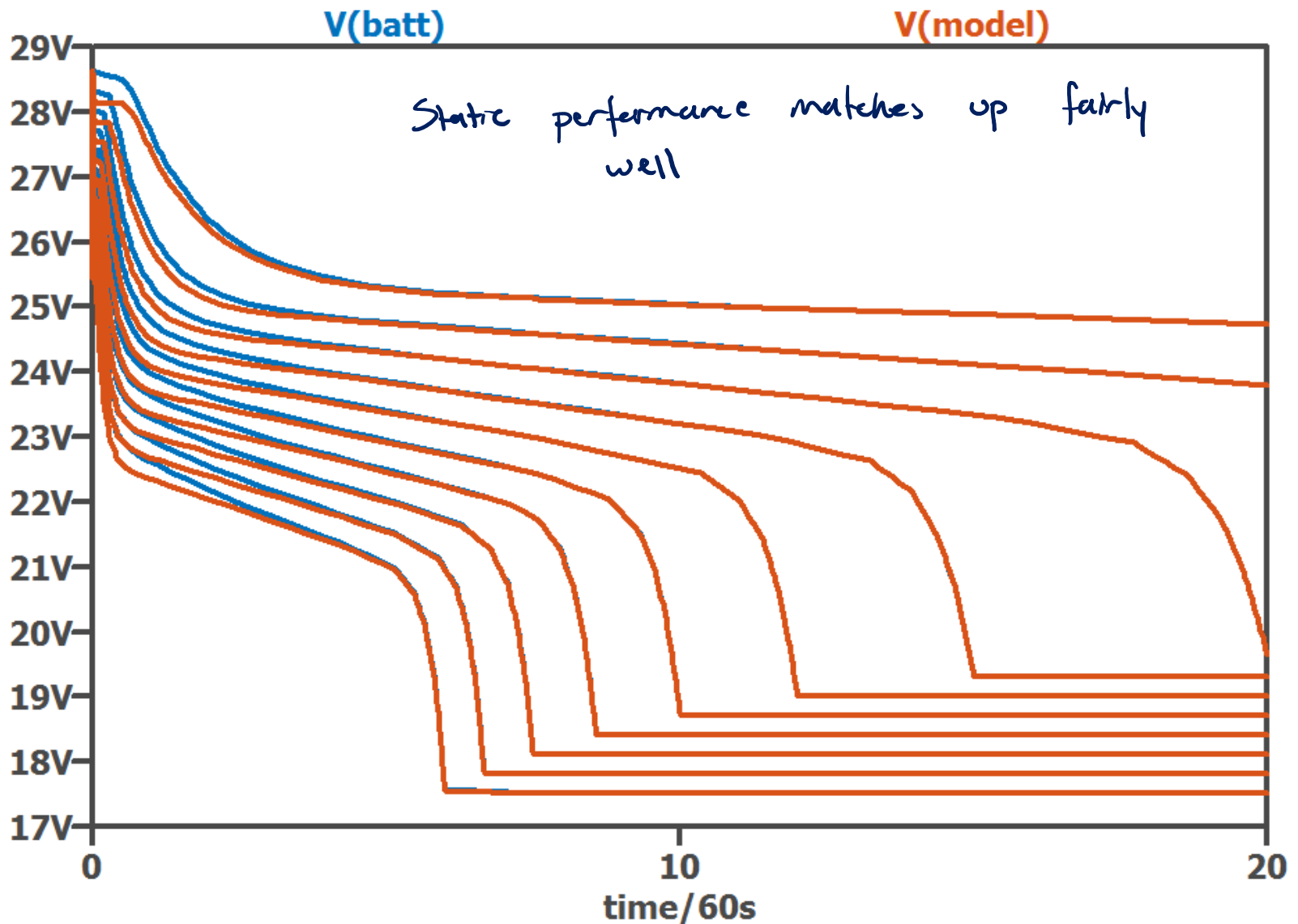
Model C: Zero-state Hysteresis



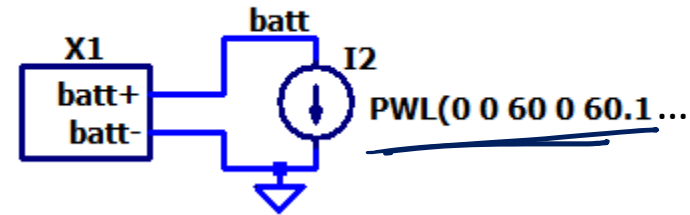
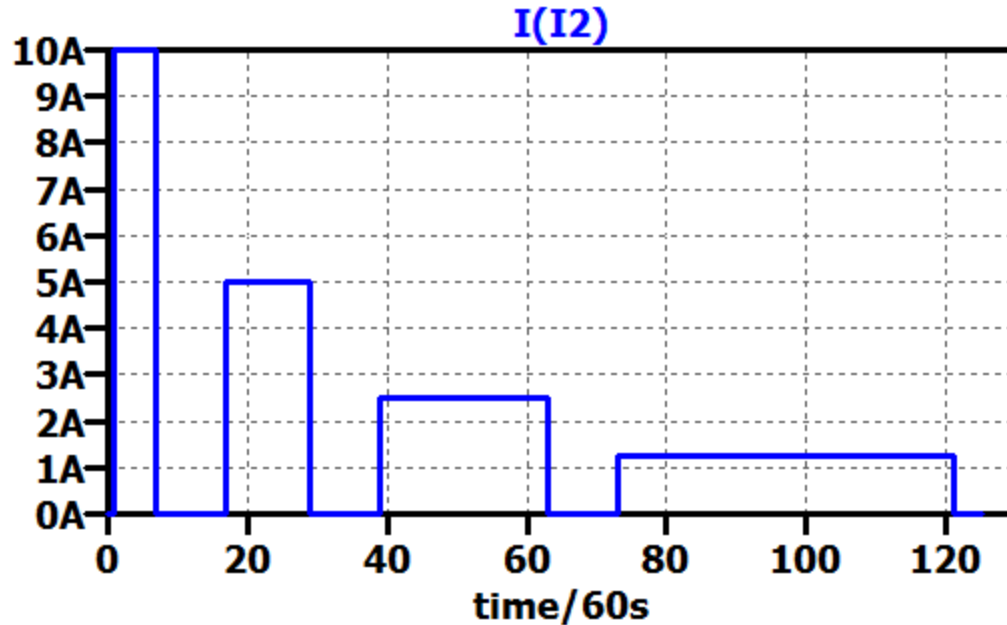
Model C Performance



Model C Performance



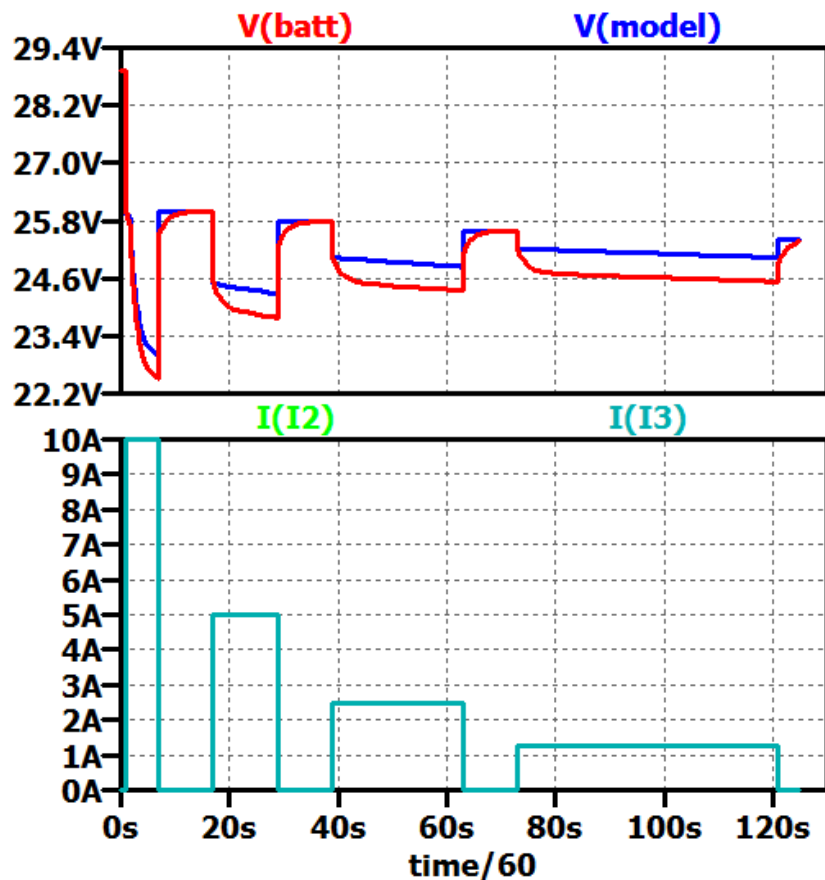
Dynamic Performance



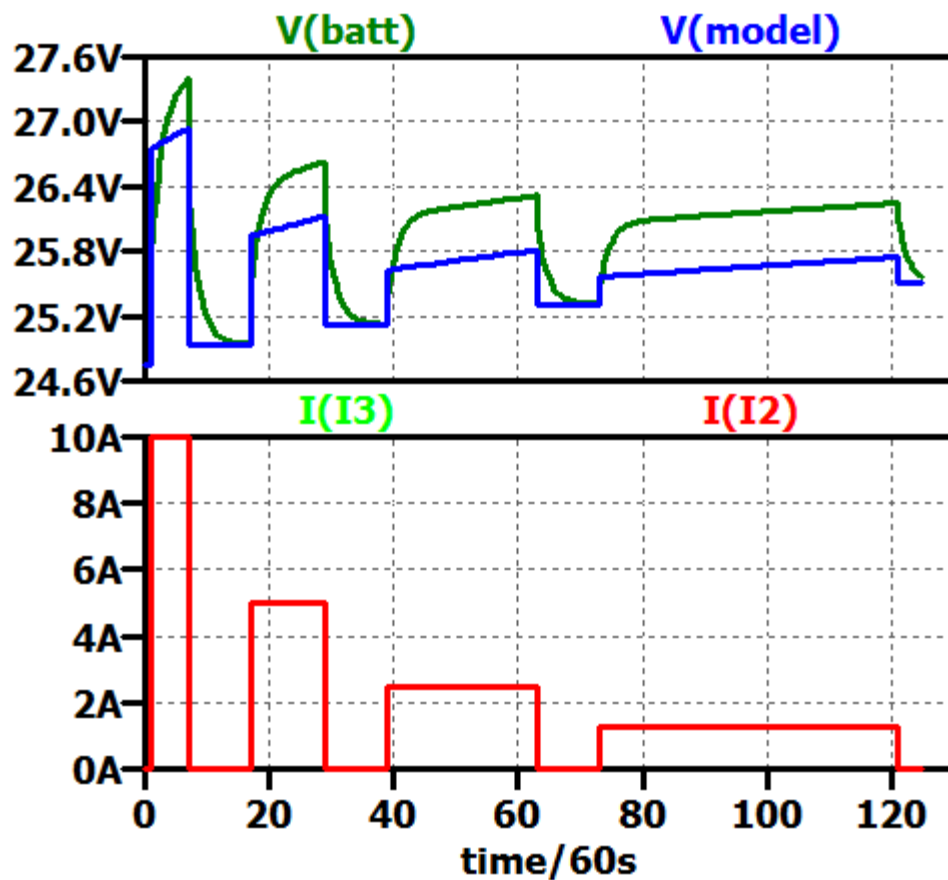
- Dynamic performance characterized by pulse train
- Constant percent of capacity per pulse [%Ahr] → *Not a necessity*

Dynamic Performance

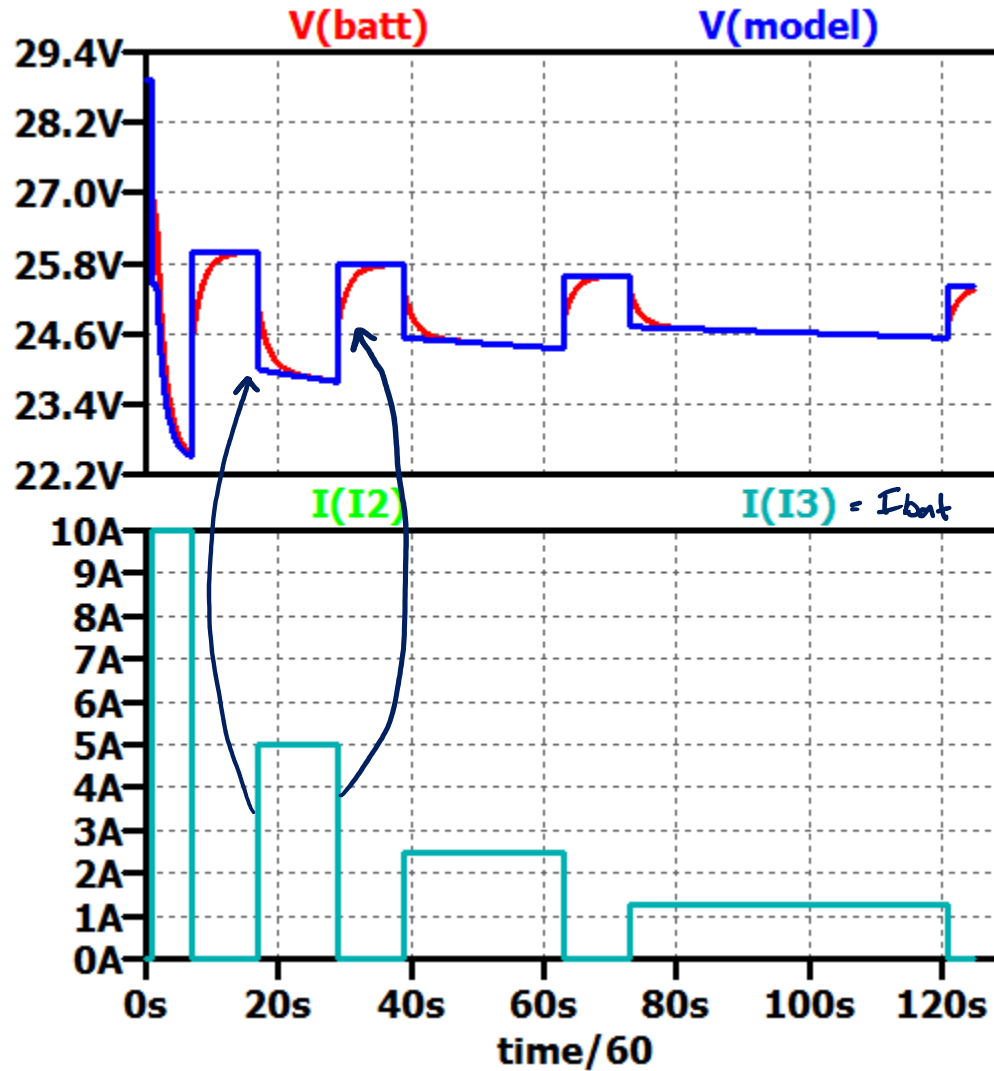
Discharge



Charge

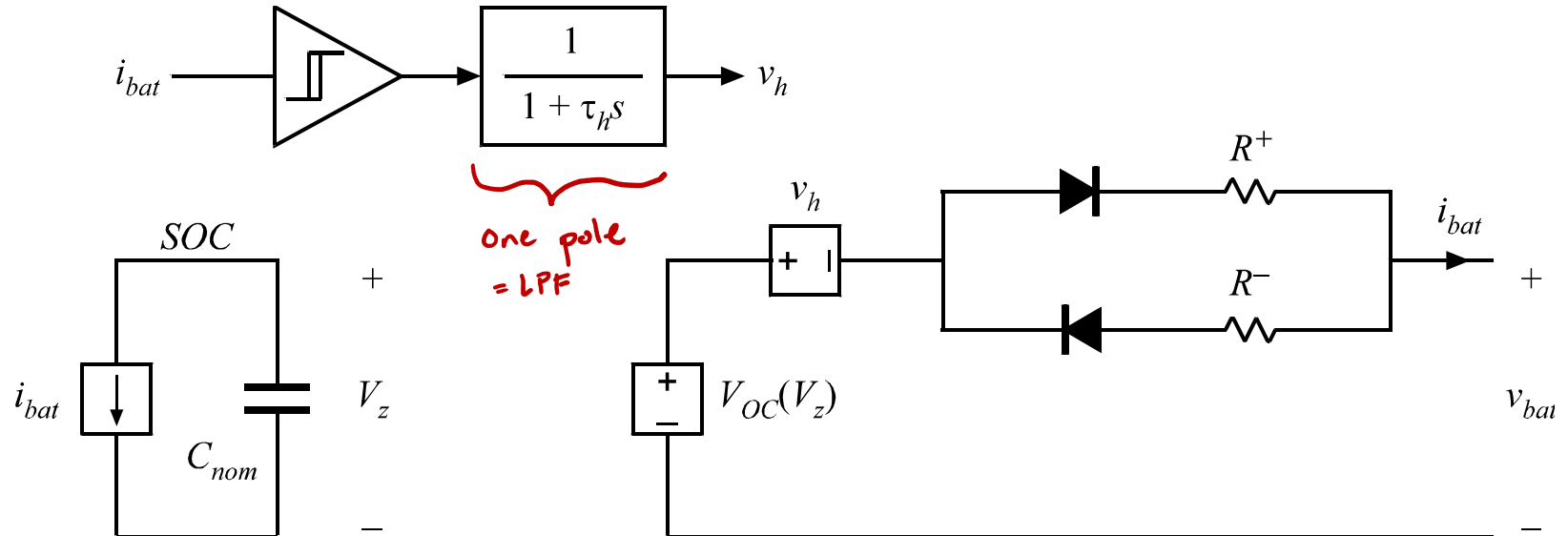


Model C Performance

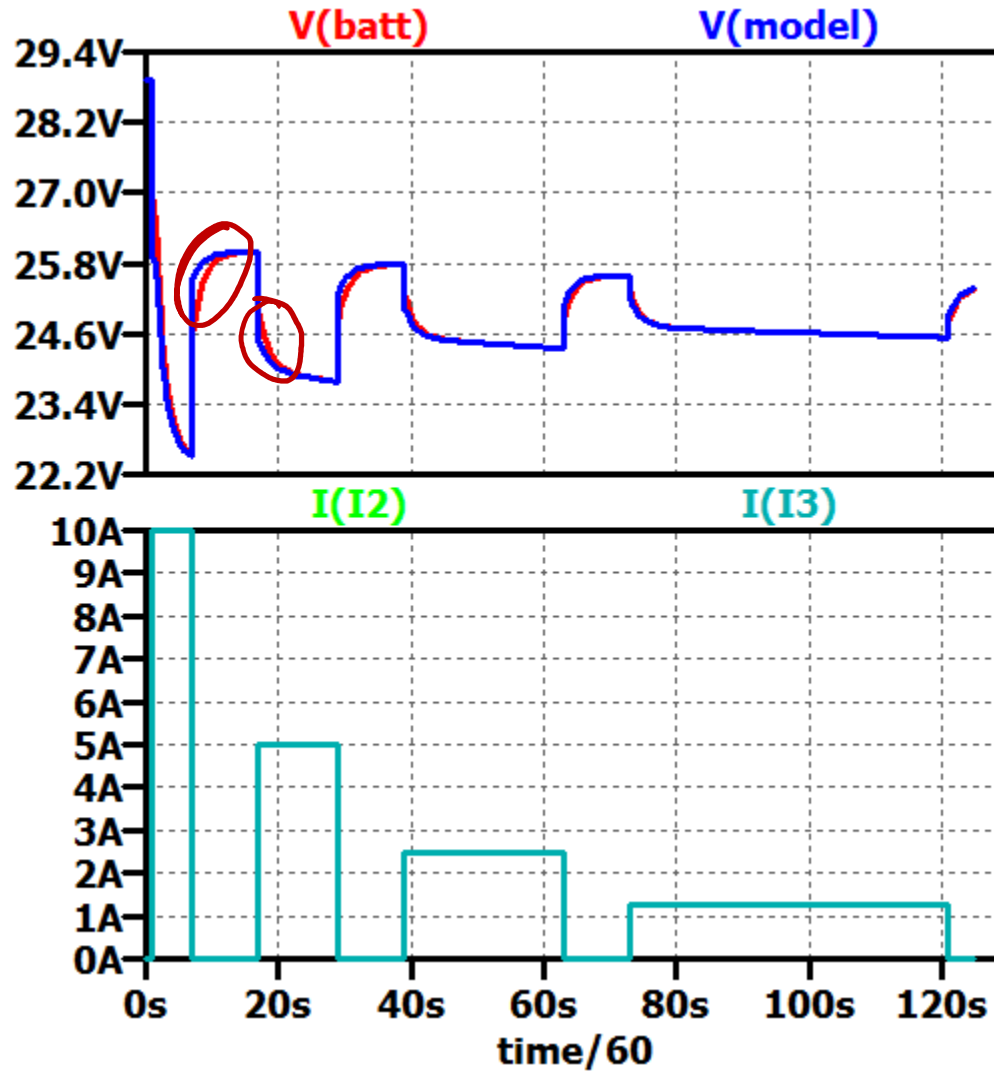


Model C1: One-state Hysteresis

[Plett 2004]

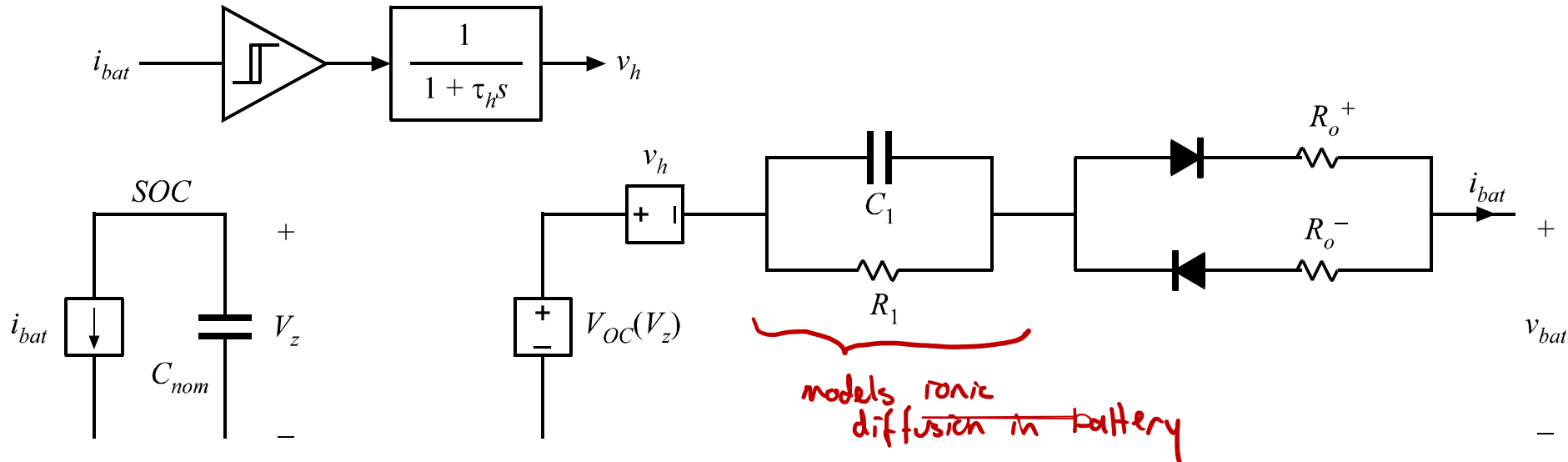


Model C1 Performance



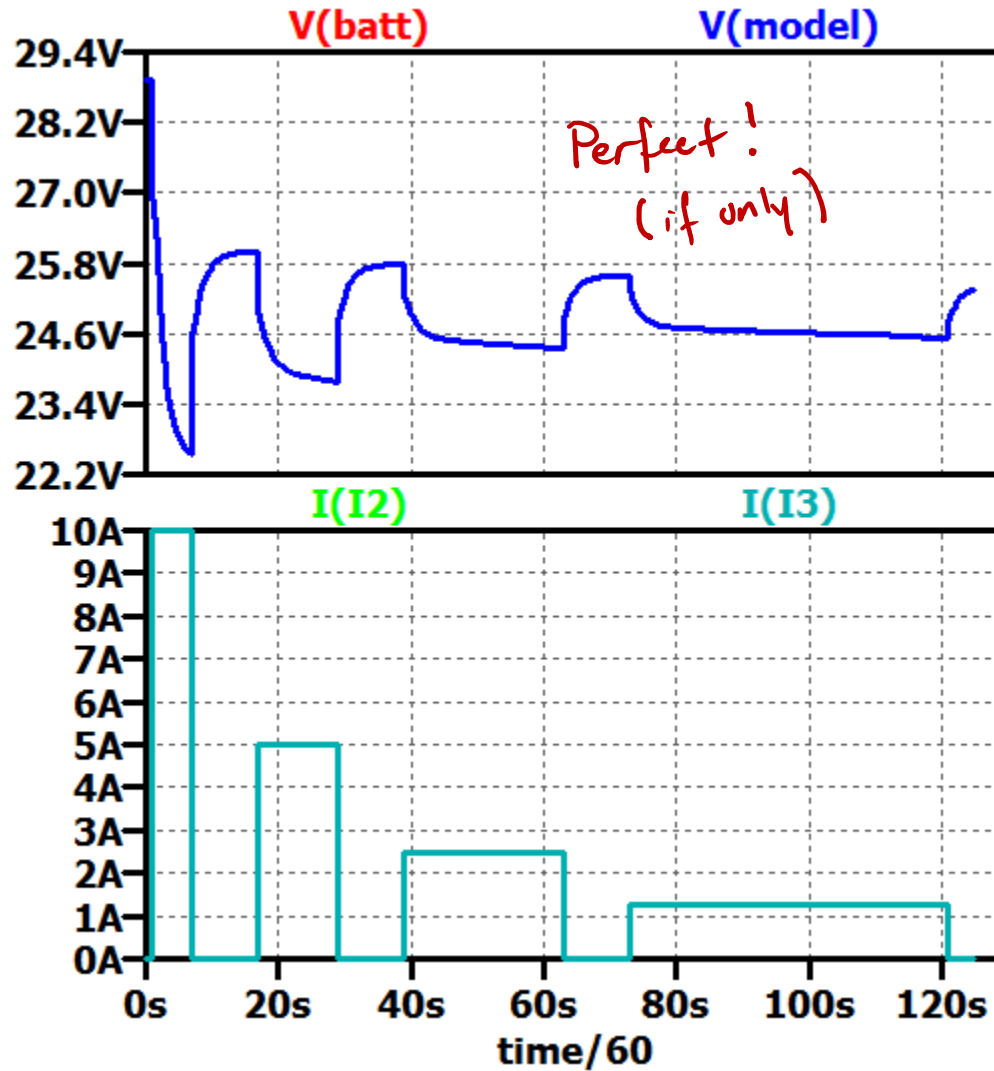
Model D: Diffusion (one-state)

[Plett 2004]



$R_1 \rightarrow$ removed from R^+/R^- so total steady-state resistance doesn't change

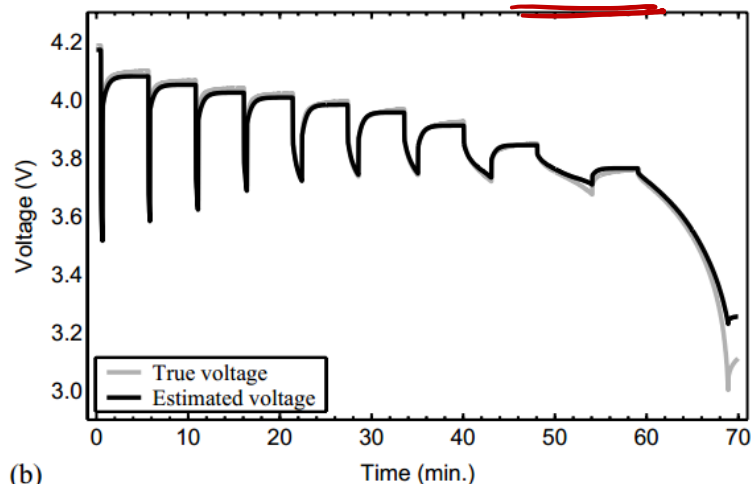
Model D Performance



Experimental Results

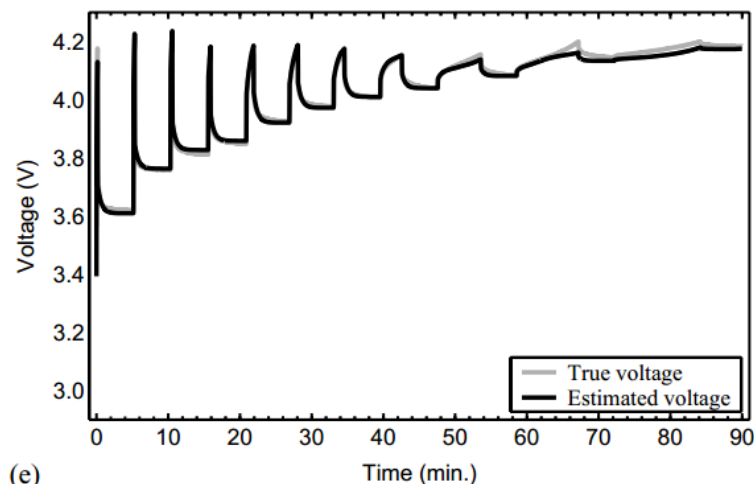
Very good matching

Modeling discharge: ESC, 2 filter states



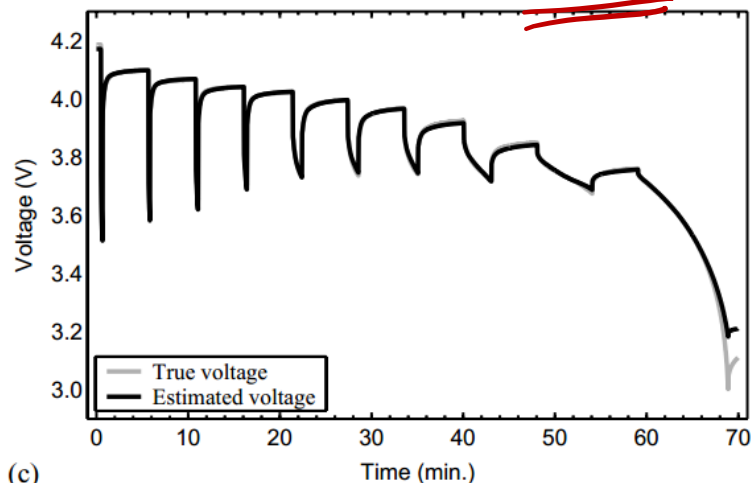
(b)

Modeling charge: ESC, 2 filter states



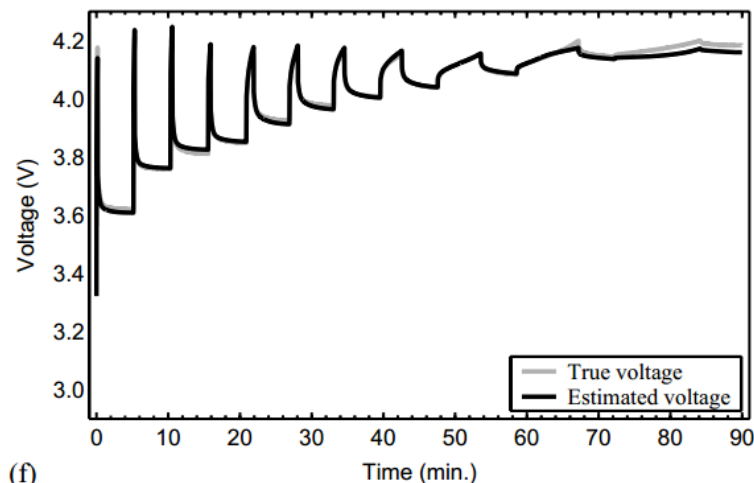
(e)

Modeling discharge: ESC, 4 filter states



(c)

Modeling charge: ESC, 4 filter states



(f)

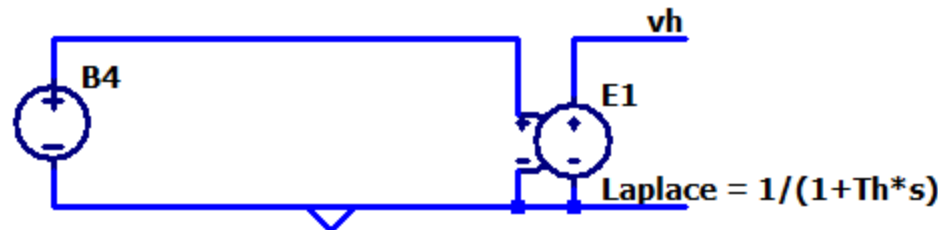
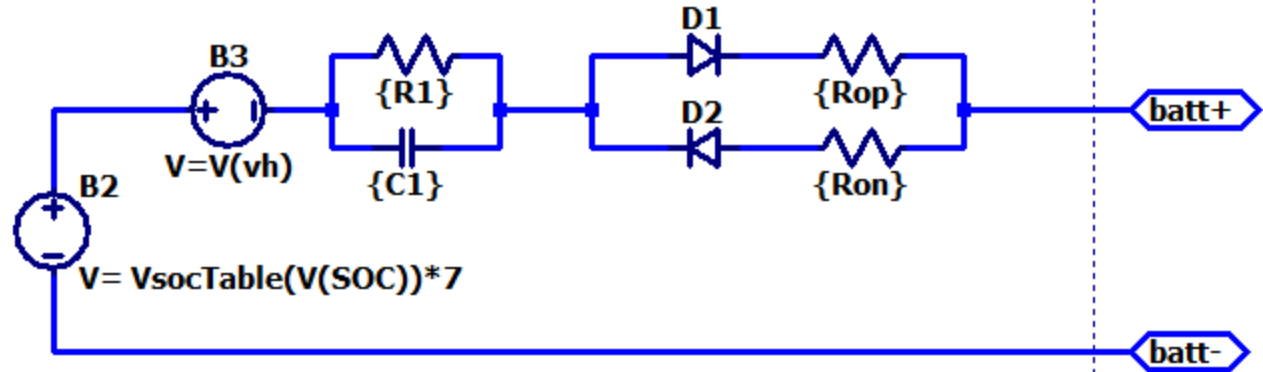
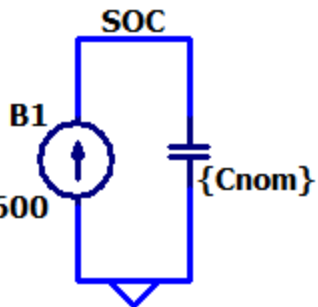
Implementation in LTSpice

.param R1 = 1m C1 = 10n

.model batdiode D(n=.001)
.param Rop = 1m Ron = 1m

.param VSOC0 = .5
.param Cnom = 10

.param Vh = 1 Th = 10



$V = Vh * (IF(I(B2) < -.1, 1, IF(I(B2) > .1, -1, 0)))$

.func VsocTable(x) = {table(x,0,3.0021, 0.01, 3.108, 0.02, 3.191, 0.03, 3.257, 0.04, 3.308, 0.05, 3.3...