Announcements

- HW9 posted
- PCBs ordered for all planning to complete the design challenge
- TNvoice available
  - https://utk.campuslabs.com/eval-home/
  - Currently, 1/6 completed
  - Closes 12/1

The Averaged System

This equation is now the model of a new, equivalent linear system

$$\dot{\boldsymbol{x}}(t) = \boldsymbol{A}\boldsymbol{x}(t) + \boldsymbol{B}u(t)$$

where

$$\boldsymbol{A} = D\boldsymbol{A_1} + D'\boldsymbol{A_2}$$
$$\boldsymbol{B} = D\boldsymbol{B_1} + D'\boldsymbol{B_2}$$

which has averaged behavior over one switching period

This approximation is *perhaps* valid, if

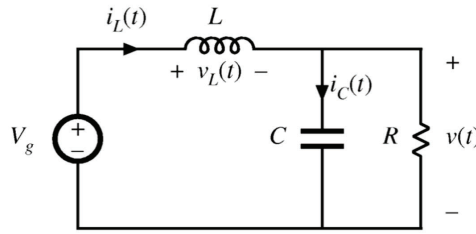
- State waveforms are dominantly linear
- Dynamics of interest are at $f_{bw} \ll f_s$

Buck State Space Averaging

In switch position 1

$$\dot{\boldsymbol{x}}(t) = \boldsymbol{A}_1\boldsymbol{x}(t) + \boldsymbol{B}_1 u(t)$$

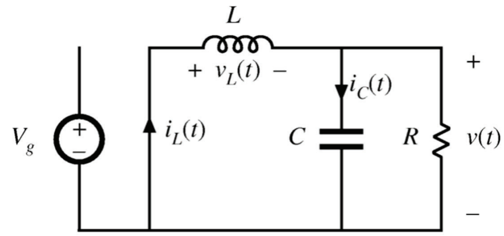
$$\frac{d}{dt}\begin{bmatrix} i_L(t) \\ v_c(t) \end{bmatrix} = \begin{bmatrix} 0 & \frac{-1}{L} \\ \frac{1}{C} & \frac{-1}{RC} \end{bmatrix} \cdot \begin{bmatrix} i_L(t) \\ v_c(t) \end{bmatrix} + \begin{bmatrix} 1/L \\ 0 \end{bmatrix} v_g(t)$$



In switch position 2

$$\dot{\boldsymbol{x}}(t) = \boldsymbol{A}_2\boldsymbol{x}(t) + \boldsymbol{B}_2 u(t)$$

$$\frac{d}{dt}\begin{bmatrix} i_L(t) \\ v_c(t) \end{bmatrix} = \begin{bmatrix} 0 & \frac{-1}{L} \\ \frac{1}{C} & \frac{-1}{RC} \end{bmatrix} \cdot \begin{bmatrix} i_L(t) \\ v_c(t) \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \end{bmatrix} v_g(t)$$



Buck Averaged Model

So, our average model is

$$\langle\dot{\boldsymbol{x}}(t)\rangle = (D\boldsymbol{A}_1 + D'\boldsymbol{A}_2)\langle\boldsymbol{x}(t)\rangle + (D\boldsymbol{B}_1 + D'\boldsymbol{B}_2)\langle u(t)\rangle$$

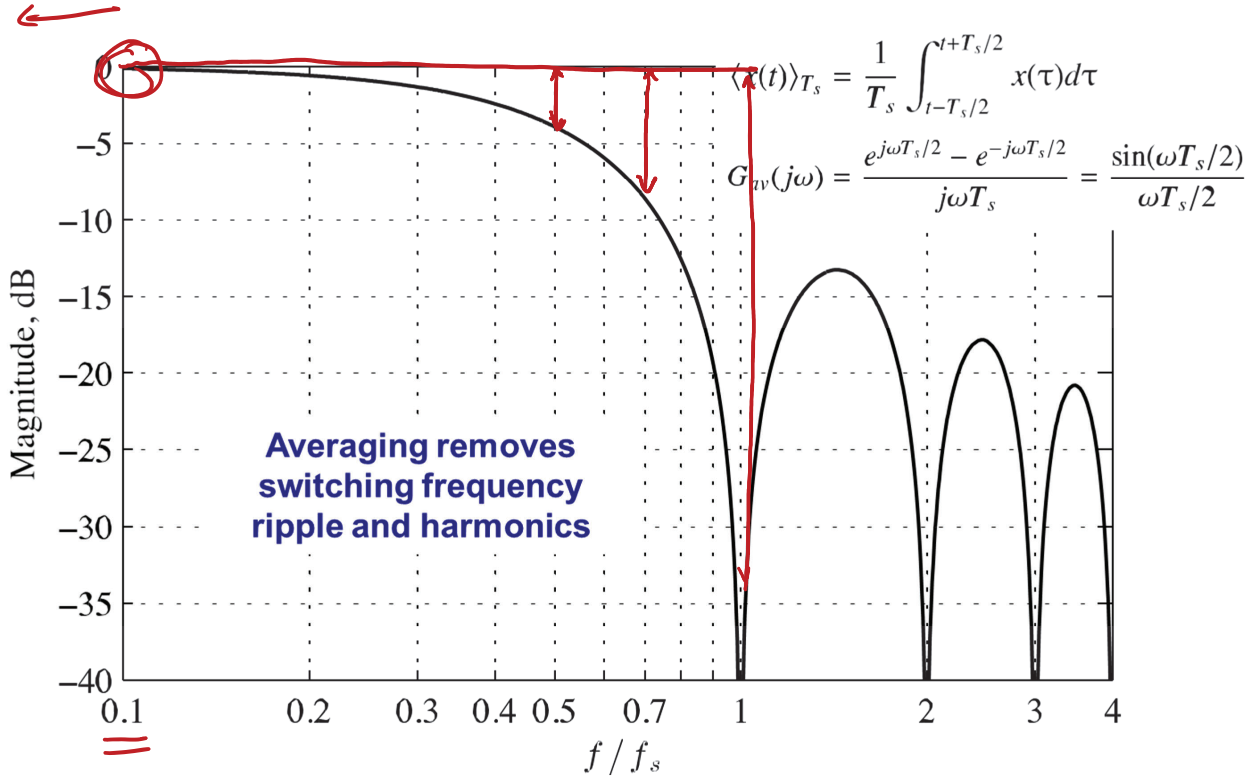
$$\langle\dot{\boldsymbol{x}}(t)\rangle = \left(D\begin{bmatrix} 0 & \frac{-1}{L} \\ \frac{1}{C} & \frac{-1}{RC} \end{bmatrix} + D'\begin{bmatrix} 0 & \frac{-1}{L} \\ \frac{1}{C} & \frac{-1}{RC} \end{bmatrix} \right)\langle\boldsymbol{x}(t)\rangle + \left(D\begin{bmatrix} 1/L \\ 0 \end{bmatrix} + D'\begin{bmatrix} 0 \\ 0 \end{bmatrix} \right) V_g$$

$$\langle\dot{\boldsymbol{x}}(t)\rangle = \begin{bmatrix} 0 & \frac{-1}{L} \\ \frac{1}{C} & \frac{-1}{RC} \end{bmatrix}\langle\boldsymbol{x}(t)\rangle + \begin{bmatrix} D/L \\ 0 \end{bmatrix} V_g$$

Large-signal (steady state)

$$\begin{cases} DV_g - \langle v_c(t)\rangle = L\dfrac{d\langle i_L(t)\rangle}{dt} = 0 & \rightarrow \quad V = DV_g \\ \langle i_L(t)\rangle - \dfrac{\langle v_c(t)\rangle}{R} = C\dfrac{d\langle v_c(t)\rangle}{dt} = 0 & \rightarrow \quad I_L = \dfrac{V}{R} \end{cases}$$

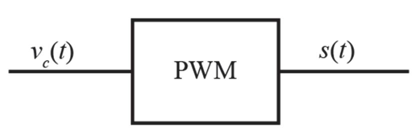
Averaging: Discussion

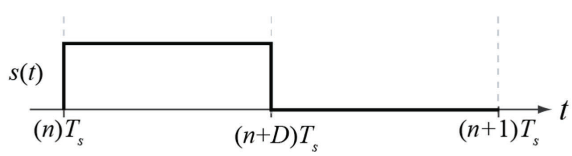


$$\langle x(t)\rangle_{T_s} = \frac{1}{T_s}\int_{t-T_s/2}^{t+T_s/2} x(\tau)d\tau$$

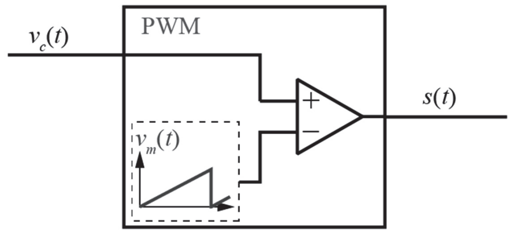
$$G_{av}(j\omega) = \frac{e^{j\omega T_s/2} - e^{-j\omega T_s/2}}{j\omega T_s} = \frac{\sin(\omega T_s/2)}{\omega T_s/2}$$

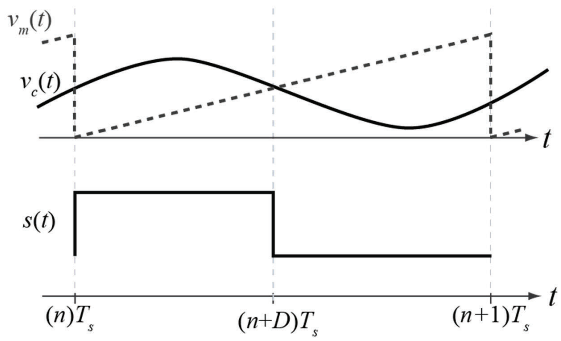
Discrete Time Nature of PWM



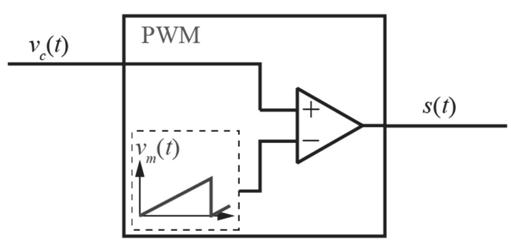


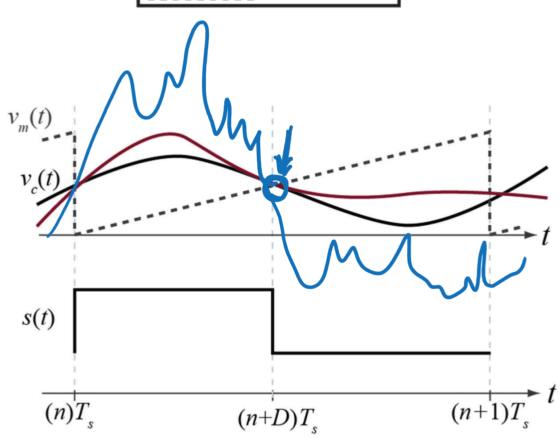
Discrete Time Nature of PWM





Discrete Time Nature of PWM





Historical Perspective

Robert D Middlebrook
PhD, Standford, 1955
CalTech Professor, 1955-1998

Slobodan Cúk
PhD CalTech, 1976
CalTech Prof, 1977-1999

Modelling, analysis, and design of switching converters

Model a switched system as an averaged, time-invariant system with

$$\dot{\boldsymbol{x}}(t) = \boldsymbol{A}\boldsymbol{x}(t) + \boldsymbol{B}u(t)$$

where

$$\boldsymbol{A} = D\boldsymbol{A}_1 + D'\boldsymbol{A}_2$$
$$\boldsymbol{B} = D\boldsymbol{B}_1 + D'\boldsymbol{B}_2$$

Dennis John Packard
PhD, CalTech 1976

Discrete modeling and analysis of switching regulators

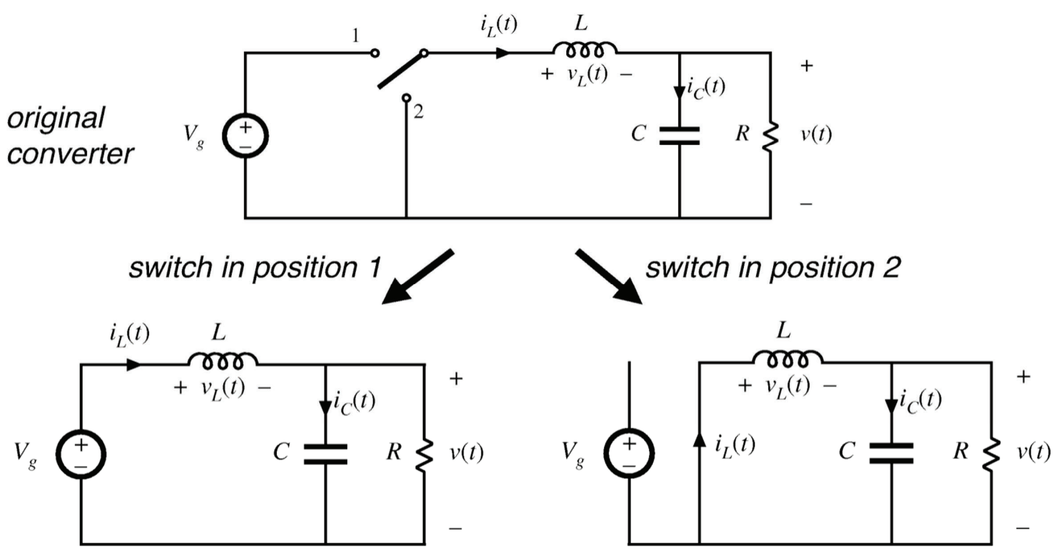
Model a switched system as a discrete-time system with

$$\boldsymbol{x}[n+1] = \boldsymbol{\Phi}\boldsymbol{x}[n] + \boldsymbol{\Psi}U[n]$$

where

$$\boldsymbol{\Phi} = \left(\prod_{i=n_{sw}}^{1} e^{\boldsymbol{A}_i t_i}\right)$$
$$\boldsymbol{\Psi} = \sum_{i=1}^{n_{sw}} \left\{\left(\prod_{k=n_{sw}}^{i+1} e^{\boldsymbol{A}_k t_k}\right)\boldsymbol{A}_i^{-1}\left(e^{\boldsymbol{A}_i t_i} - \boldsymbol{I}\right)\boldsymbol{B}_i\right\}$$

Large Signal Modeling of SMPS



Discrete Time Modeling

- Every subcircuit is a passive, linear circuit
- Passive, linear circuits can be solved in closed-form
  - Can model states at discrete times without averaging
- Only assumptions required
  - Independent inputs are DC or slowly varying

Solution to State Space Equation

Closed form solution to state space equation

$$\dot{\boldsymbol{x}}(t) = \boldsymbol{A}\boldsymbol{x}(t) + \boldsymbol{B}u(t)$$

Multiply both sides by $e^{-\boldsymbol{A}t}$

$$e^{-\boldsymbol{A}t}\dot{\boldsymbol{x}}(t) - e^{-\boldsymbol{A}t}\boldsymbol{A}\boldsymbol{x}(t) = e^{-\boldsymbol{A}t}\boldsymbol{B}u(t)$$

Left-hand side is

$$\frac{d}{dt}\left(e^{-\boldsymbol{A}t}\boldsymbol{x}(t)\right) = e^{-\boldsymbol{A}t}\boldsymbol{B}u(t)$$

Solution to State Space Equation

$$\frac{d}{dt}\left(e^{-At}\boldsymbol{x}(t)\right) = e^{-At}\boldsymbol{B}u(t)$$

Can now be solved by direct integration

$$e^{-At}\boldsymbol{x}(t) - \boldsymbol{x}(0) = \int_0^t e^{-A\tau}\boldsymbol{B}u(\tau)\,d\tau$$

Rearranging

Natural response

forced response

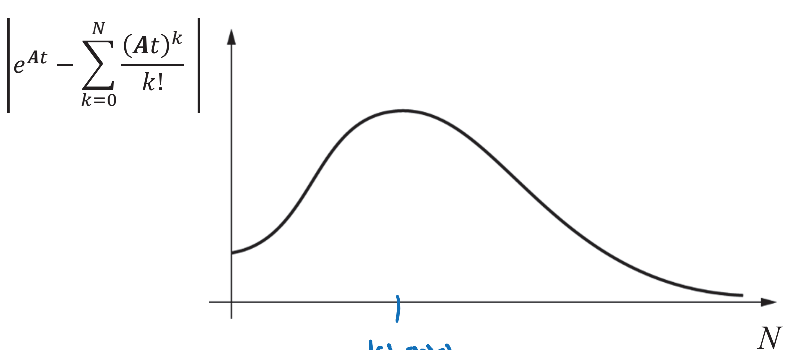
$$\boldsymbol{x}(t) = e^{At}\boldsymbol{x}(0) + \int_0^t \underbrace{e^{-A(t-\tau)}\boldsymbol{B}u(\tau)\,d\tau}_{\text{convolution integral}}$$

Matrix Exponential

Matrix exponential defined by Taylor series expansion

$$e^{At} = I + At + \frac{(At)^2}{2!} + \cdots + \frac{(At)^N}{N!} = \sum_{k=0}^{N}\frac{(At)^k}{k!}$$

Well-known issue with convergence in many cases



10,000 terms

Matlab:

expm( )

– matrix exponential

C. Moler and C. V. Loan, “Nineteen dubious ways to compute the exponential of a matrix,” SIAM Review, vol. 20, pp. 801–836, 1978.

Properties of the Matrix Exponential

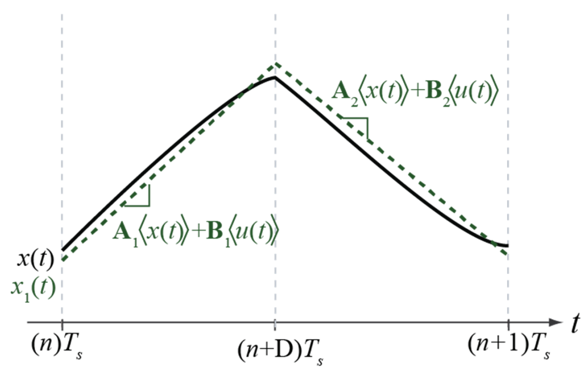
- Matrix exponential always exists
  - i.e. summation will always converge
- Exponential of any matrix is always invertible, with

$$e^{\boldsymbol{A}}e^{-\boldsymbol{A}} = \boldsymbol{I}$$

First Order Taylor Series Expansion

Linear ripple approximation

$$e^{\boldsymbol{A}t} \approx I + \boldsymbol{A}t$$



Valid only if switching frequency much faster than system modes

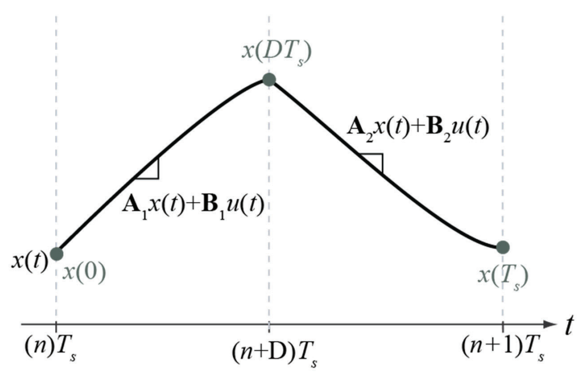
Simplification for Slow-Varying Inputs

$$\boldsymbol{x}(t) = e^{\boldsymbol{A}t}\boldsymbol{x}(0) + \int_0^t e^{-\boldsymbol{A}(t-\tau)}\boldsymbol{B}u(\tau)\,d\tau$$

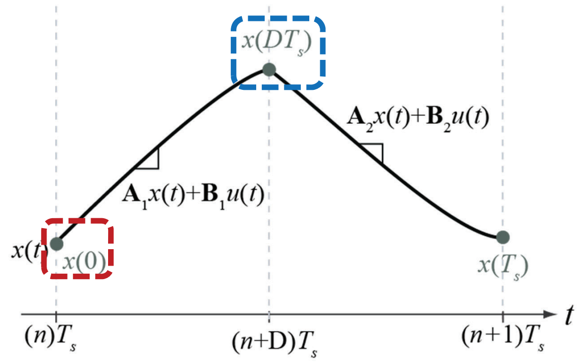
If A is invertible and $u(\tau) \approx U$

$$\boldsymbol{x}(t) = e^{\boldsymbol{A}t}\boldsymbol{x}(0) + \boldsymbol{A}^{-1}(e^{\boldsymbol{A}t} - \boldsymbol{I})\boldsymbol{B}U$$

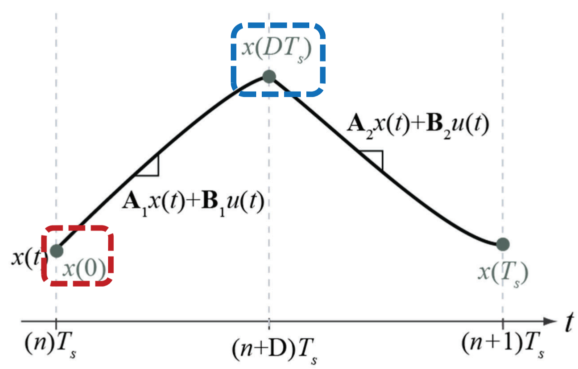
Application to Switching Converter



Application to Switching Converter

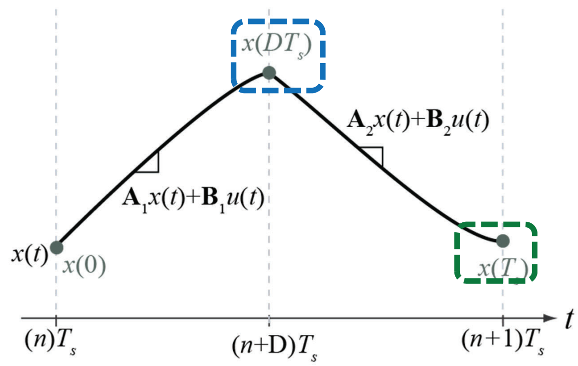


Application to Switching Converter



$$\boxed{\boldsymbol{x}(DT_s)} = e^{\boldsymbol{A}_1 DT_s}\boxed{\boldsymbol{x}(0)} + \boldsymbol{A}_1{}^{-1}(e^{\boldsymbol{A}_1 DT_s} - \boldsymbol{I})\boldsymbol{B}_1 U$$

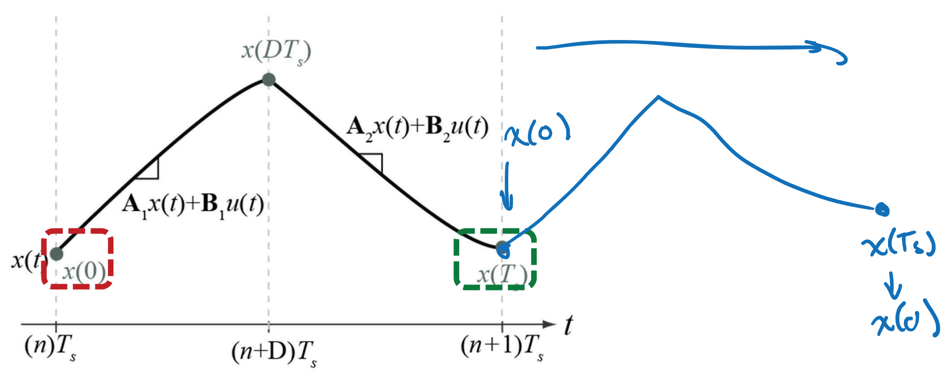
Application to Switching Converter



$$\boldsymbol{x}(DT_s) = e^{\boldsymbol{A}_1 DT_s}\boldsymbol{x}(0) + \boldsymbol{A}_1{}^{-1}(e^{\boldsymbol{A}_1 DT_s} - \boldsymbol{I})\boldsymbol{B}_1 U$$

$$\boxed{\boldsymbol{x}(T_s)} = e^{\boldsymbol{A}_2 D' T_s}\boxed{\boldsymbol{x}(DT_s)} + \boldsymbol{A}_2{}^{-1}(e^{\boldsymbol{A}_2 D' T_s} - \boldsymbol{I})\boldsymbol{B}_2 U$$

Application to Switching Converter



$$\boldsymbol{x}(DT_s) = e^{\boldsymbol{A}_1 DT_s}\boldsymbol{x}(0) + \boldsymbol{A}_1{}^{-1}(e^{\boldsymbol{A}_1 DT_s} - \boldsymbol{I})\boldsymbol{B}_1 U$$

$$\boldsymbol{x}(T_s) = e^{\boldsymbol{A}_2 D' T_s}\boldsymbol{x}(DT_s) + \boldsymbol{A}_2{}^{-1}(e^{\boldsymbol{A}_2 D' T_s} - \boldsymbol{I})\boldsymbol{B}_2 U$$

$$\boxed{\boldsymbol{x}(T_s)} = e^{\boldsymbol{A}_2 D' T_s} e^{\boldsymbol{A}_1 DT_s}\boxed{\boldsymbol{x}(0)} + \boldsymbol{A}_2{}^{-1}(e^{\boldsymbol{A}_2 D' T_s} - \boldsymbol{I})\boldsymbol{B}_2 U + e^{\boldsymbol{A}_2 D' T_s}\boldsymbol{A}_1{}^{-1}(e^{\boldsymbol{A}_1 DT_s} - \boldsymbol{I})\boldsymbol{B}_1 U$$

THE UNIVERSITY OF TENNESSEE KNOXVILLE

General Form

Generally, for n_{sw} separate switching positions

$$\boldsymbol{x}(T_s) = \underbrace{\left(\prod_{i=n_{sw}}^{1} e^{\boldsymbol{A}_i t_i}\right)}_{\Phi} \boldsymbol{x}(0) + \underbrace{\sum_{i=1}^{n_{sw}} \left\{ \left(\prod_{k=n_{sw}}^{i+1} e^{\boldsymbol{A}_k t_k} \right) \boldsymbol{A}_i^{-1} \left(e^{\boldsymbol{A}_i t_i} - \boldsymbol{I} \right) \boldsymbol{B}_i \right\}}_{\Psi} U$$

Equation is in the form of a discrete-time system with

$$\boldsymbol{x}[n+1] = \boldsymbol{\Phi} \boldsymbol{x}[n] + \boldsymbol{\Psi} U[n] \leftarrow \underline{\text{LTI DT system}}$$

Again, the effect of changing modulation (i.e. t_i) is hidden in nonlinear terms

$$\widehat{\boldsymbol{x}}[n+1] = \boldsymbol{\Phi} \widehat{\boldsymbol{x}}[n] + \boldsymbol{\Psi} \hat{u}[n] + \boldsymbol{\Gamma} \hat{d}[n]$$

Find $\boldsymbol{\Gamma}$ by small-signal modeling

Aside: Comparison to Averaged Modeling

$$\boldsymbol{x}(T_s) = \left(\prod_{i=n_{sw}}^{1} e^{\boldsymbol{A}_i t_i}\right) \boldsymbol{x}(0) + \sum_{i=1}^{n_{sw}} \left\{ \left(\prod_{k=n_{sw}}^{i+1} e^{\boldsymbol{A}_k t_k} \right) \boldsymbol{A}_i^{-1} \left(e^{\boldsymbol{A}_i t_i} - \boldsymbol{I} \right) \boldsymbol{B}_i \right\} U$$

Approximate with straight-line waveforms, $e^{\boldsymbol{A}t} \approx I + \boldsymbol{A}t$

$$\boldsymbol{x}(T_s) = \left(\boldsymbol{I} + \sum_{i=n_{sw}}^{1} \boldsymbol{A}_i t_i + \cdots \right) \boldsymbol{x}(0) + \sum_{i=1}^{n_{sw}} \left\{ \left(\boldsymbol{I} + \sum_{k=n_{sw}}^{i+1} \boldsymbol{A}_k t_k + \cdots \right) t_i \boldsymbol{B}_i \right\} U$$

Neglect all terms with product of two ore more t_i

$$\boldsymbol{x}(T_s) = \left(\boldsymbol{I} + \sum_{i=1}^{n_{sw}} \boldsymbol{A}_i t_i \right) \boldsymbol{x}(0) + \sum_{i=1}^{n_{sw}} (t_i \boldsymbol{B}_i) \, U$$

Continuous time conversion

$$\dot{\boldsymbol{x}}_{DT}(t) = \frac{\boldsymbol{x}(T_s) - \boldsymbol{x}(0)}{T_s} = \overbrace{\sum_{i=1}^{n_{sw}} \left(\boldsymbol{A}_i \frac{t_i}{T_s} \right) \boldsymbol{x} + \sum_{i=1}^{n_{sw}} \left(\boldsymbol{B}_i \frac{t_i}{T_s} \right) U}^{= \text{average model}}$$

Aside: Discrete vs Averaged Modeling

So, averaged and discrete time formulations are equivalent if

- Ripple in states is
    1. Dominantly straight-line, so $e^{\boldsymbol{A}_i t_i} \approx (\boldsymbol{I} + \boldsymbol{A}_i t_i)$
    2. Low frequency, such that $t_i t_j \ll \|\boldsymbol{A}_i \boldsymbol{A}_j\|$