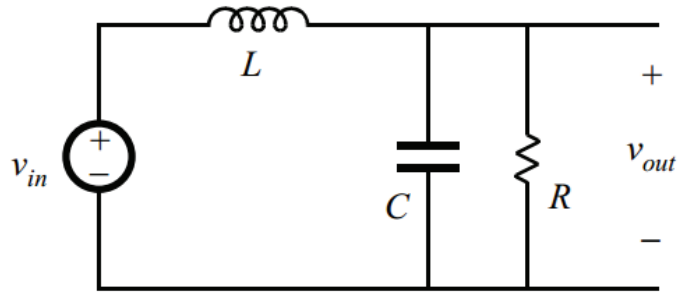
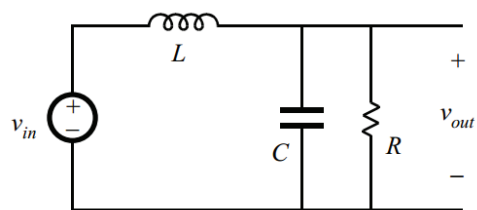


# Resonant Circuits



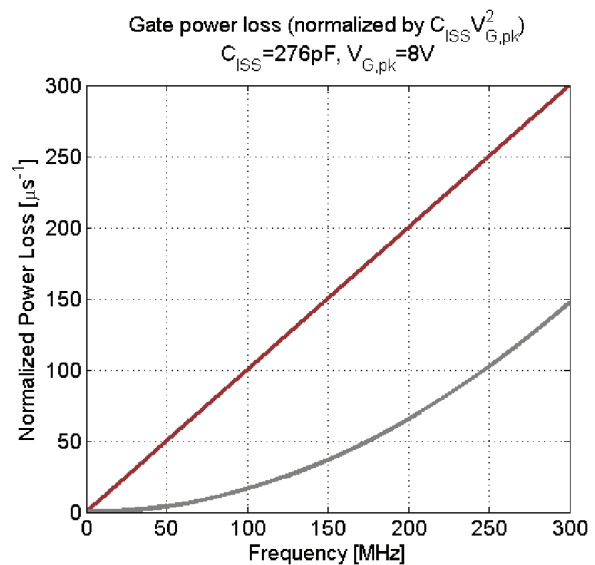
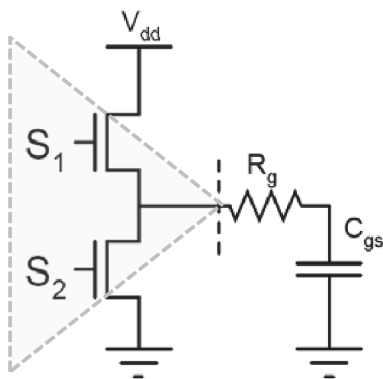
## Resonant Circuit Analysis



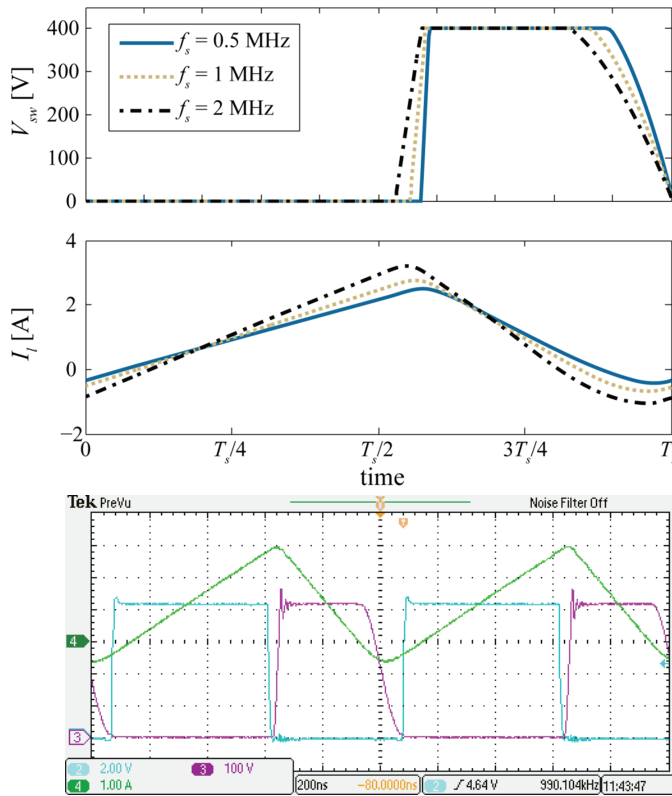
# Soft Switching

- Advantages
  - Reduced switching loss
  - Possible operation at higher switching frequency
  - Lower EMI
- Disadvantages
  - Increased current and/or voltage stresses due to circulating current
  - Higher peak and rms current values
  - Complexity of analysis and modeling

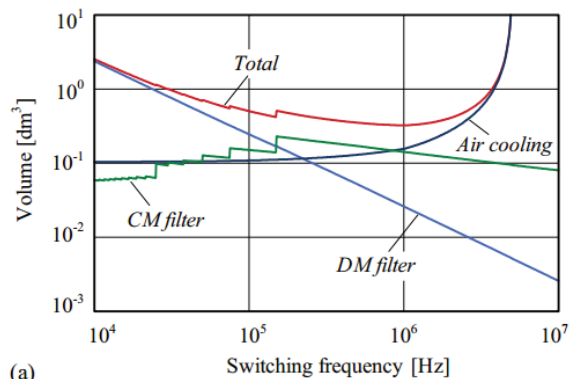
## Limitations: Gate Drive



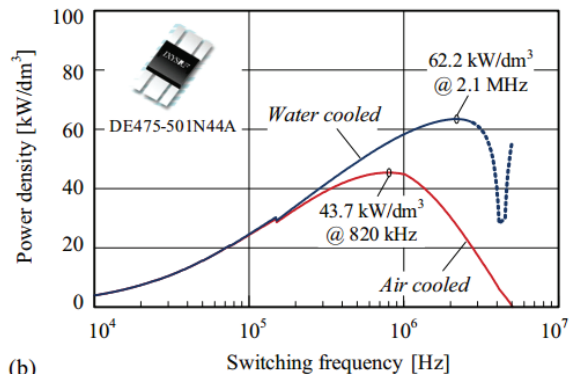
# Limitations: $t_d/T_s$



# Limitations: Thermal

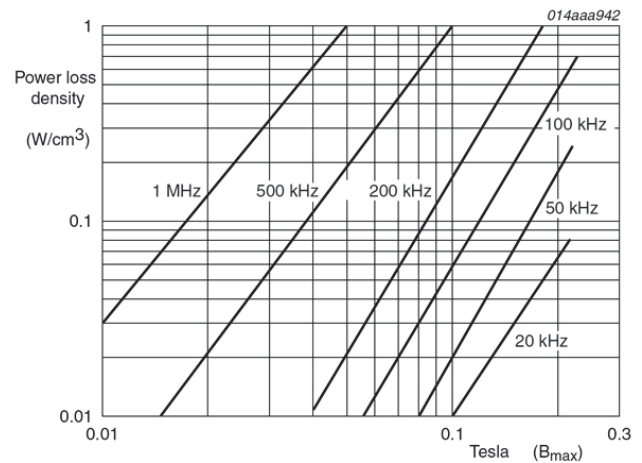
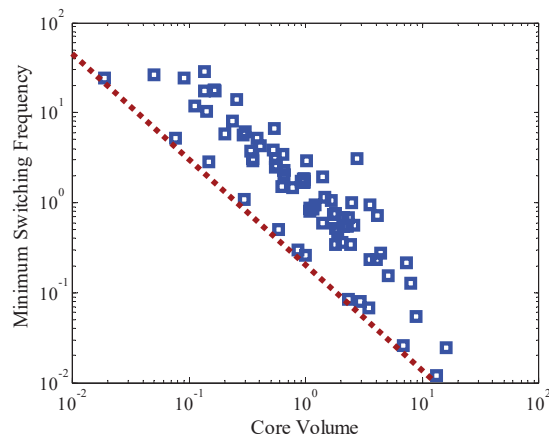


(a)

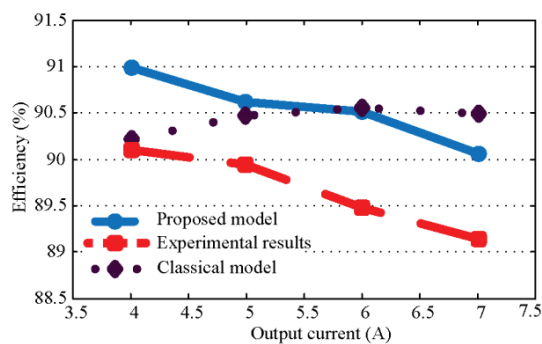
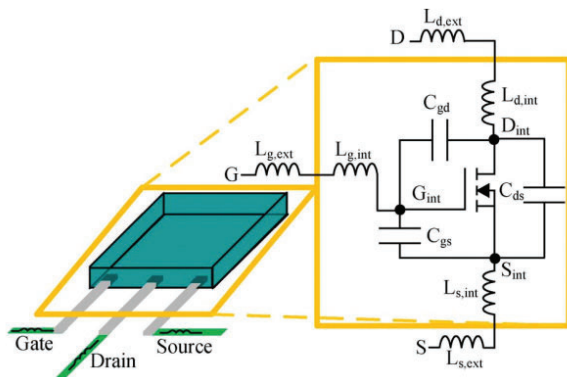


(b)

# Limitations: Magnetics Design



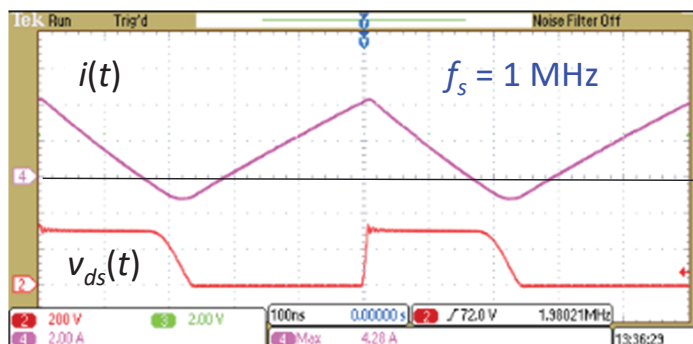
# Limitations: Circuit Modeling



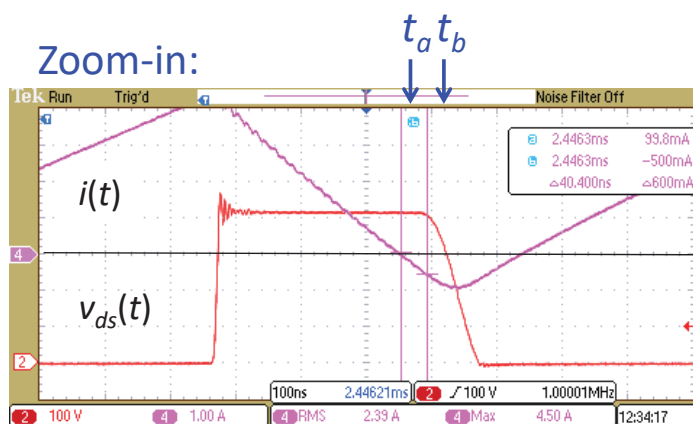
150-to-400V, 150W Boost

## EXPERIMENTAL EXAMPLE

### ZVS with Si diode

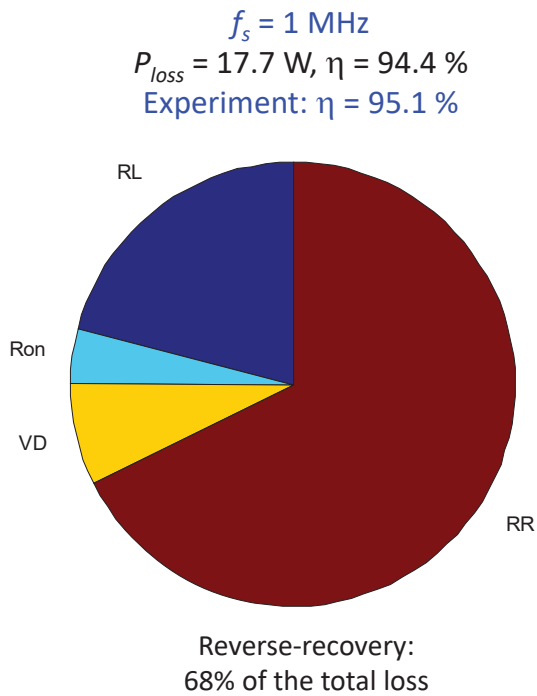
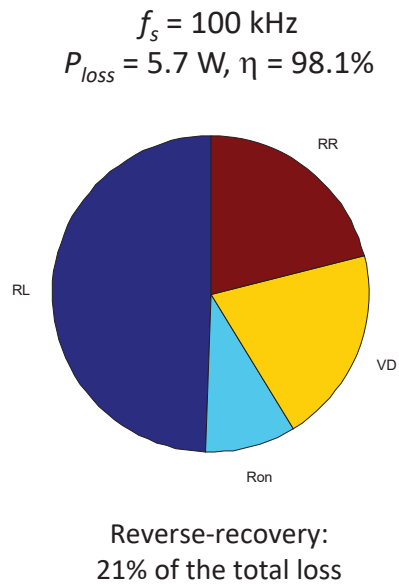


Zoom-in:

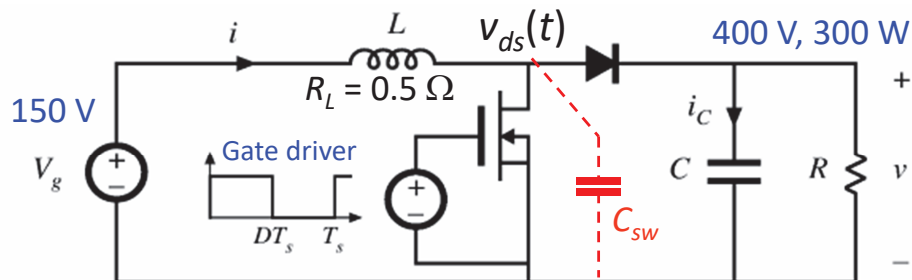


- ZVS turn-ON
  - Eliminated losses due to  $C_{sw}$  discharge during turn-ON transient
  - Eliminated losses due to MOSFET  $di_F/dt$  during turn-ON transient
- Diode reverse recovery still impacts the waveforms and losses
- Increased current ripple
  - Increased conduction losses (by >30%)
  - Increased  $dv_{ds}/dt$  upon turn-OFF, MOSFET turn-OFF speed is more important

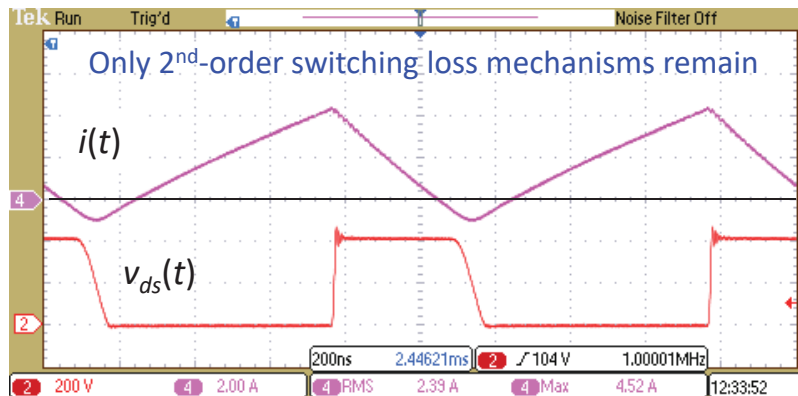
# Loss Breakdown: Soft-Switched Si Boost



## Soft-switched SiC diode



SiC diode, "soft-switched" operation



$f_s = 1 \text{ MHz}$

### MOSFET

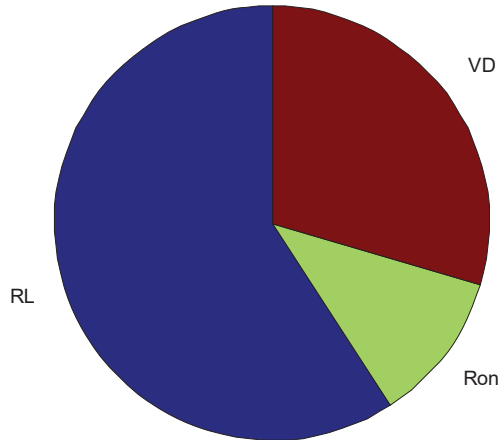
- $di_T/dt = 200 \text{ A}/\mu\text{s}$
- $C_{ds,eq} = 45 \text{ pF}$
- $R_{on} = 0.15 \Omega$

### SiC diode

- $t_{rr} = 0, Q_{rr} = 0$
- $2C_{d,eq} - C_{d,eq} = 64 \text{ pF}$
- $V_D = 1.8 \text{ V}$

# Soft-switched Boost with SiC diode

Conduction losses only, 2<sup>nd</sup>-order switching losses not included in the model



VD 100 kHz or 1 MHz  
98.5% efficiency  
 $P_{loss} = 4.5 \text{ W}$

Experiments:

98.7% at 1 MHz  
98.0% at 2 MHz

Power supply technology limits become dominated by:

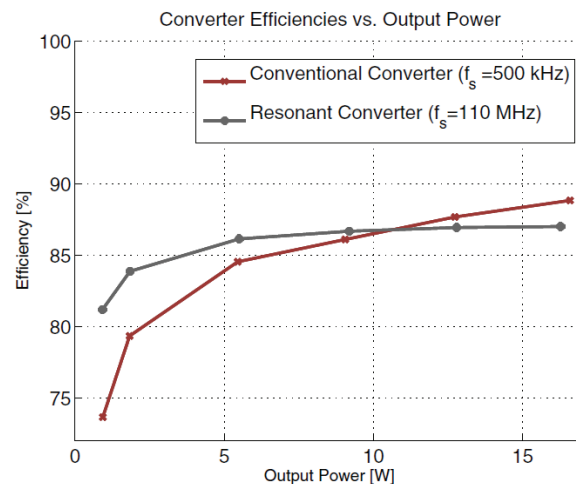
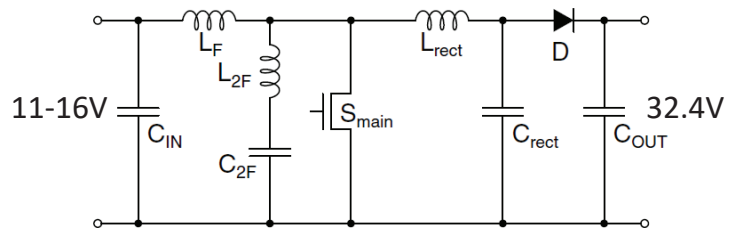
- Magnetics
- 2<sup>nd</sup>-order switching loss mechanisms, e.g. gate-drive losses, parasitic inductances (layout and packaging)
- Gate-drive circuitry and controllers to support high-frequency operation

## VHF power electronics [11]

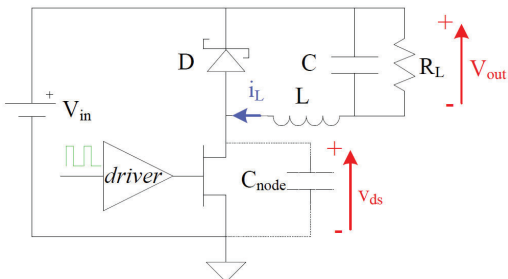
Component	Resonant Design Value	Type
$L_F$	33 nH	Coilcraft 1812SMS
$L_{2F}$	12.5 nH	Coilcraft A04TG
$L_{rect}$	22 nH	1812SMS
$C_{2F}$	39 pF	ATC100A
$C_{rect}$	10 pF	ATC100A
$C_{out}$	75 $\mu\text{F}$	Multilayer Ceramics
$C_{in}$	22 $\mu\text{F}$	Multilayer Ceramics
$S_{main}$		Freescale MRF6S9060
$D$		Fairchild S310

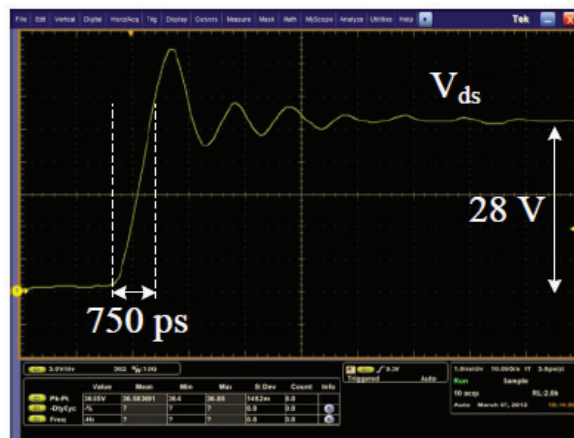
Component	Conventional Design Value	Type
$L_{boost}$	10 $\mu\text{H}$	Coilcraft D03316T-103ML
$C_{out}$	75 $\mu\text{F}$	Multilayer Ceramics
$C_{in}$	22 $\mu\text{F}$	Multilayer Ceramics
$S_{main}$		LT1371HV
$D$		Fairchild S310



# WBG Devices



Standard hard-switched PWM operation at 50 MHz  
 $dv_{ds}/dt$  dominated by probe (4 pF) capacitance



TriQuint TGF2023-02  
 12W, DC-to-18 GHz  
 RF/microwave HEMT

FOM for switching applications

$$C_{ds}R_{on} \approx 1 \Omega\text{pF}$$

$$Q_gR_{on} \approx 10 \Omega\text{pC}$$

Emerging GaN HEMT devices may enable completely new RF-based design approaches in power electronics

M. Rodríguez, G. Stahl, D. Costinett and D. Maksimović, "Simulation and characterization of GaN HEMT in high-frequency switched-mode power converters,"



## Topics Covered

- **Course Topics**
  - High Frequency Power Conversion
    - Switching losses and device selection
    - Resonance in power electronics
    - Soft switching (ZVS and ZCS)
    - Magnetics design
  - Non-resonant soft switching converters
    - Constant frequency control
    - State-plane analysis
    - Resonant switches
    - Modeling and Simulation
    - Discrete time models
  - Resonant Converters
    - Resonant converter topologies
    - Sinusoidal analysis
    - AC-modeling and frequency modulation
    - State-plane analysis
  - Applications and practical issues of high frequency converters