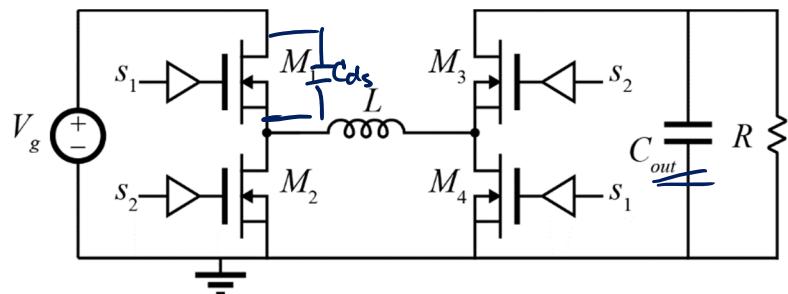
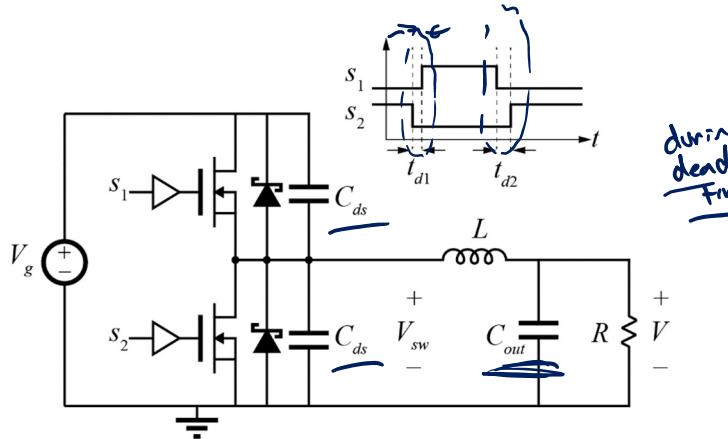
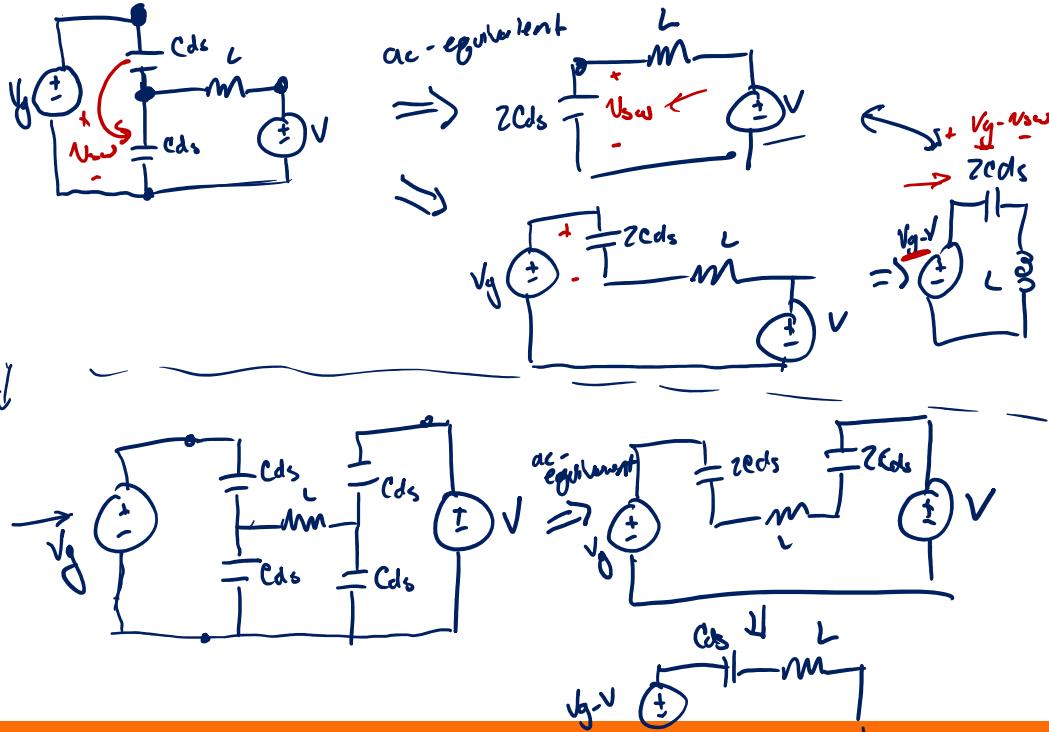


# Time-Domain Analysis of Switching Transitions

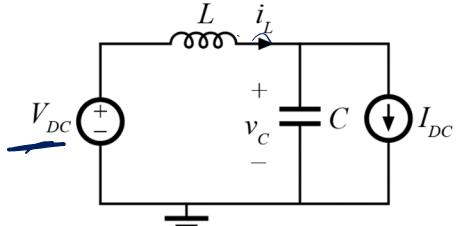


(1) Assume  $C_{out}$  is a filter element with small  $V_g - V_{sw}$  ripple

(2) Assume  $C_{ds}$  is linear



# Resonant Circuit Solution



Initial Conditions:  
 $v_c(t=0) = V_0$   
 $i_L(t=0) = I_0$

$$\begin{aligned} \textcircled{1} \quad C \frac{dv_c}{dt} &= i_L - I_{DC} \\ \textcircled{2} \quad L \frac{di_L}{dt} &= V_{DC} - v_c \end{aligned} \quad \left. \begin{array}{l} \text{ } \\ \text{ } \end{array} \right\} \rightarrow L \frac{d}{dt} \left( C \frac{dv_c}{dt} + I_{DC} \right) = V_{DC} - v_c$$
$$= LC \frac{d^2 v_c}{dt^2} + V_C - V_{DC} = 0$$

$$v_c = \begin{cases} A \sin(\omega t) + B \cos(\omega t), & \text{homogeneous} \\ \underline{v_c = V_{DC}}, & \text{particular} \end{cases}$$

$$v_c(t) = V_{DC} + \underbrace{(V_0 - V_{DC})}_{\text{particular}} \cos\left(\frac{t}{\sqrt{LC}}\right) + \underbrace{(I_0 - I_{DC})}_{\text{homogeneous}} \sqrt{\frac{L}{C}} \sin\left(\frac{t}{\sqrt{LC}}\right)$$

$$i_L(t) = I_{DC} + (I_0 - I_{DC}) \cos\left(\frac{t}{\sqrt{LC}}\right) + (V_{DC} - V_0) \sqrt{\frac{C}{L}} \sin\left(\frac{t}{\sqrt{LC}}\right)$$

# Normalization and Notation

Notation:  $\omega_0 = \frac{1}{\sqrt{LC}} = 2\pi f_0$        $R_0 = \sqrt{L/C}$

$$v_c(t) = V_{DC} + (V_0 - V_{DC}) \cos(\omega_0 t) + R_0(I_0 - I_{DC}) \sin(\omega_0 t)$$

$$i_L(t) = I_{DC} + (I_0 - I_{DC}) \cos(\omega_0 t) + \frac{1}{R_0} (V_{DC} - V_0) \sin(\omega_0 t)$$

Normalization:

$$m(t) = \frac{v(t)}{\sqrt{V_{base}}} \quad \text{where } \sqrt{V_{base}} \rightarrow \text{anything you want (constant)}$$

(some choices better than others)

$$\Rightarrow j^{(+)} = \frac{i^{(+)}}{I_{base}} \quad I_{base} = \frac{\sqrt{V_{base}}}{R_0}$$

$$\underline{\theta} = \omega t$$

$$V_{base} = V_{pc}$$

$$\underline{I_{base}} = \frac{V_{pc}}{R_0}$$

$$\left\{ \begin{array}{l} v_c(t) = V_{DC} + (V_0 - V_{DC}) \cos(\omega_0 t) + R_0(I_0 - I_{DC}) \sin(\omega_0 t) \end{array} \right.$$

$$\left. \begin{array}{l} i_L(t) = I_{DC} + (I_0 - I_{DC}) \cos(\omega_0 t) + \frac{1}{R_0}(V_{DC} - V_0) \sin(\omega_0 t) \end{array} \right.$$

$$\left\{ \begin{array}{l} m_c(\theta) = \frac{v_c(t)}{V_{pc}} = M_{pc} + (\underline{M_0 - M_{pc}}) \cos \theta + \underline{R_0 \frac{I_0 - I_{pc}}{V_{DC}}} \sin \theta \\ j_c(\theta) = \frac{i_L(t)}{I_{base}} = \underline{j_{pc}} + (\underline{\jmath_0 - \jmath_{pc}}) \cos \theta + (\underline{M_{pc} - M_0}) \sin \theta \end{array} \right.$$

$$A = M_0 - M_{pc}$$

$$B = \jmath_0 - \jmath_{pc}$$

$$\left\{ \begin{array}{l} m_c(\theta) = M_{pc} + A \cos \theta + B \sin \theta \end{array} \right.$$

$$\left. \begin{array}{l} j_c(\theta) = \jmath_{pc} + B \cos \theta - A \sin \theta \end{array} \right.$$

Try looking at  $(m_c(\theta) - M_{pc})^2 + (j_c(\theta) - \jmath_{pc})^2 =$

$$= A^2 \cos^2 \theta + B^2 \sin^2 \theta + 2AB \cos \theta \sin \theta + B^2 \cos^2 \theta + A^2 \sin^2 \theta - 2AB \cos \theta \sin \theta$$

$$= A^2 (\cos^2 \theta + \sin^2 \theta) + B^2 (\sin^2 \theta + \cos^2 \theta)$$

$$= A^2 + B^2 = (M_0 - M_{pc})^2 + (\jmath_0 - \jmath_{pc})^2$$

$$R_0 \frac{I_0 - I_{pc}}{V_{pc}} = (\jmath_0 - \jmath_{pc})$$

$$(M_{DC} = 1)$$

$$(m_c(\theta) - M_{pc})^2 + (j_c(\theta) - J_{pc})^2 = (M_0 - M_{pc})^2 + (J_0 - J_{pc})^2$$

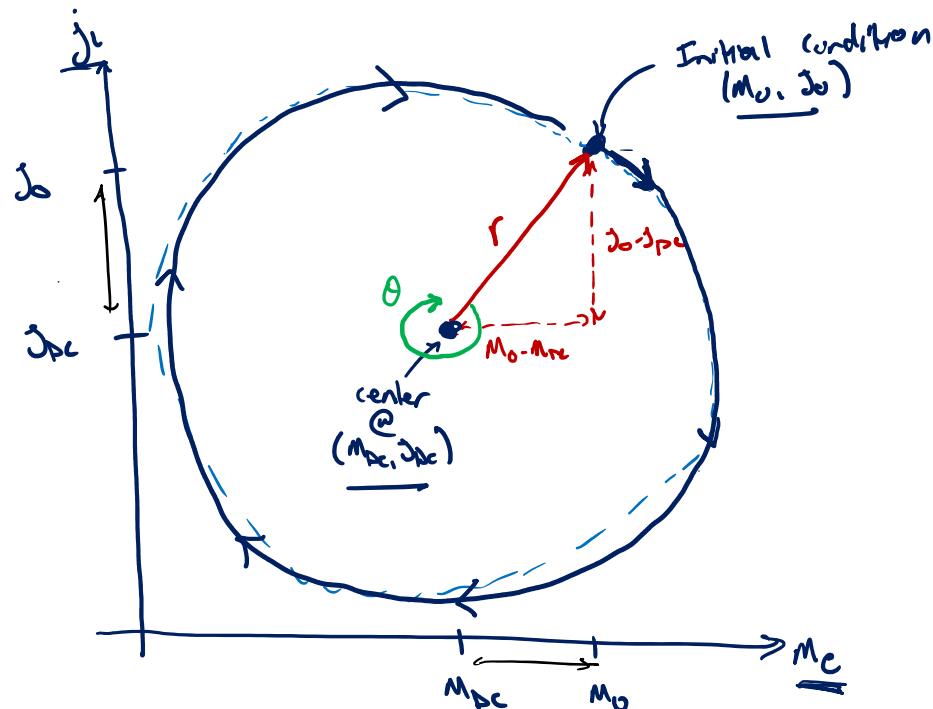
This is the equation for a circle  $x^2 + y^2 = r^2$   $r = \sqrt{(M_0 - M_{pc})^2 + (J_0 - J_{pc})^2}$

Is a defined direction associated with the state plane

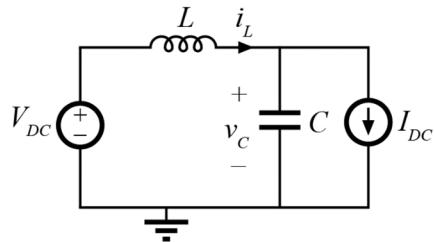
- Defined by I.C. or first derivatives of  $j_c$  &  $m_c$

### State Plane

- Transforms diff EQ solution into trig solution
- Limited to 1-L, 1-C subcircuits



# State Plane Analysis



$$V_{base} = \underline{\quad}$$

$$I_{base} = \frac{V_{base}}{R_0}$$

DC solution:

$$v_c = V_{DC}$$

$$\rightarrow m_c = M_{DC}$$

$$i_i = I_{DC}$$

$$\rightarrow j_i = J_{DC}$$

Initial Conditions:

$$v_c(0) = V_0$$

$$\rightarrow$$

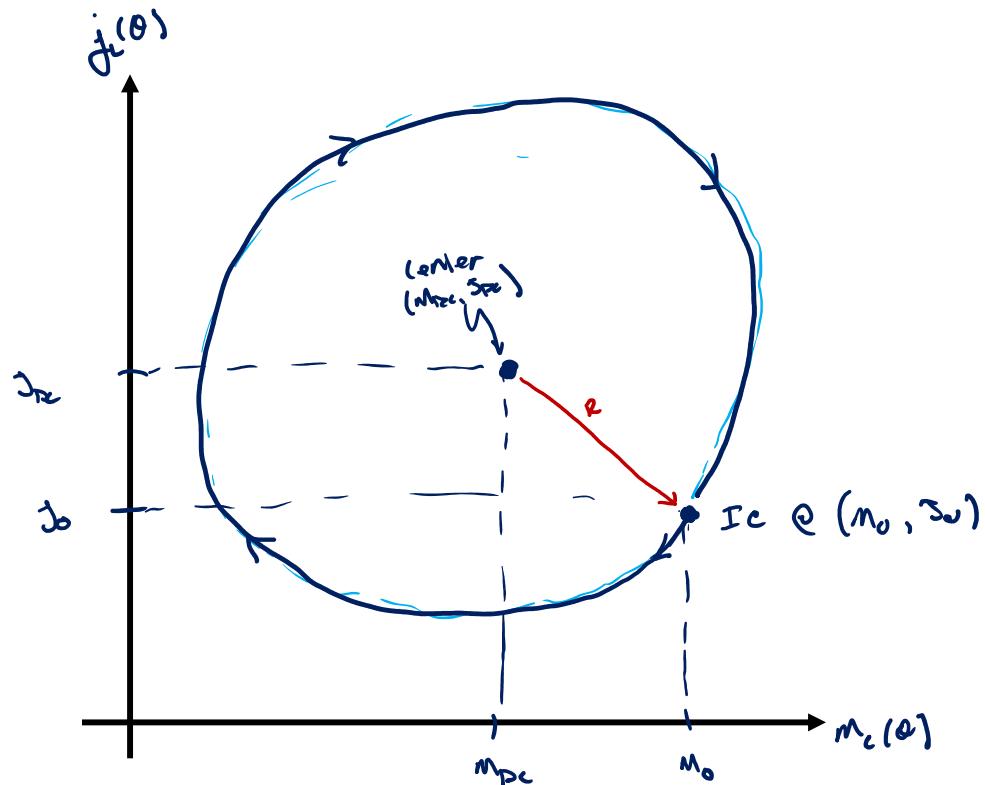
$$m_c = M_0$$

$$i_i(0) = I_0$$

$$\rightarrow$$

$$j_i = J_0$$

Direction from  $I_C$  on first derivatives



[1] R. Oruganti and F. C. Lee, "Resonant Power Processors, Part I – State Plane Analysis", Industry Applications, IEEE Tran. on, vol. 21, no. 6, nov 1985.

[2] D. P. Atherton, Nonlinear Control Engineering. London: Van Nostrand Reinhold, 1982, Ch. 2.

# Example Analysis

What is  $i_{\text{cpl}}$ ?

$$\dot{\phi}_{\text{cpl}} = \frac{i_{\text{cpl}}}{I_{\text{base}}} = \frac{i_{\text{cpl}}}{J_{\text{base}}/R_0}$$

$$\dot{\phi}_{\text{cpl}} = \dot{\phi}_{\text{pc}} + r$$

$$j_{\text{cpl}} = \dot{\phi}_{\text{pc}} + \sqrt{(M_0 - M_{\text{pc}})^2 + (J_0 - J_{\text{pc}})^2}$$

$$i_{\text{cpl}} = I_{\text{pc}} + \frac{J_{\text{base}}}{R_0} \sqrt{(M_0 - M_{\text{pc}})^2 + (J_0 - J_{\text{pc}})^2}$$

When does  $i_{\text{cpl}}$  occur?

$$\theta = \omega_0 t \quad t = \frac{\theta}{\omega_0}$$

$$\theta_{\text{pc}} = \frac{\pi}{2} + \tan^{-1} \left( \frac{J_{\text{pc}} - J_0}{M_{\text{pc}} - M_0} \right)$$

$$t_{\text{ph}} = \frac{\pi}{2\omega_0} + \frac{1}{\omega_0} \tan^{-1} \left( \frac{J_{\text{pc}} - J_0}{M_{\text{pc}} - M_0} \right)$$

