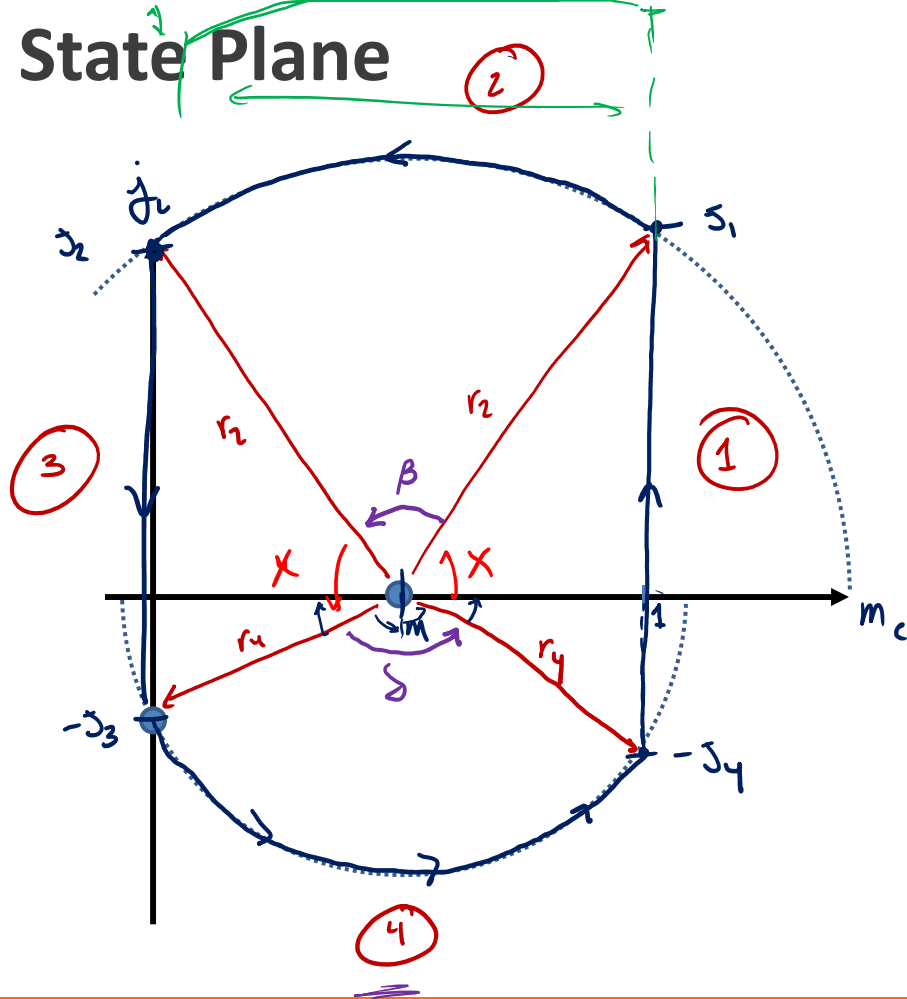


Sync-Buck Complete State Plane



usually easy to obtain if buck converter has $I_{out} \rightarrow \phi$

ZVS Conditions:

② $m - r_2 \leq \phi \rightarrow m - \sqrt{s_1^2 + (1-m)^2} \leq \phi$
 if $m < 1/2$, $s_1 = \phi$ works

④ $m + \sqrt{m^2 + s_3^2} \geq 1$
 if $m > 1/2$, $s_3 = 0$ works

State Plane Solution: Intervals 1 & 2

① → Non-resonant subinterval : look at waveforms & relate I_1 & I_4

$$\left(\frac{1}{\omega_{base}}\right) \frac{V_0 - V}{L} t_1 = I_1 + I_4 \left(\frac{1}{\omega_{base}}\right)$$

$$\frac{R_0}{L} = \frac{\sqrt{4}c}{L} = \sqrt{\frac{1}{LC}} = \frac{1}{\sqrt{LC}} = \omega_0$$

$$(1-m) \frac{R_0}{L} t_1 = J_1 + J_4$$

$$(1-m) \theta_1 = J_1 + J_4$$

② → Resonant subinterval : 2 equations } relate radius @ beginning & end of period
solve angle of the circular segment

$$\left. \begin{aligned} r_2^2 &= J_1^2 + (1-m)^2 \\ r_2 &= J_2^2 + m^2 \end{aligned} \right\}$$

$$J_1^2 + (1-m)^2 = J_2^2 + m^2$$

$$\beta = \pi - \tan^{-1}\left(\frac{J_1}{1-m}\right) - \tan^{-1}\left(\frac{J_2}{m}\right)$$

State Plane Solution: Intervals 3 & 4

$$\textcircled{3} \quad \frac{v}{L} t_3 = I_2 + I_3$$

$$M \theta_3 = J_2 + J_3$$

$$\textcircled{4} \quad J_3^2 + M^2 = J_4^2 + (1-M)^2 = r_4^2$$

$$\delta = \pi - \tan^{-1}\left(\frac{J_3}{M}\right) - \tan^{-1}\left(\frac{J_4}{1-M}\right)$$

State Plane Solution: Averaging Step

$$I_{out} = \frac{1}{T_s} \int_0^{T_s} i_{out}(t) dt = \frac{1}{T_s} \int_0^{T_s} i_c(t) dt$$

$$= \frac{1}{T_s} \left[\int_0^{t_1} i_c(t) dt + \int_{t_1}^{t_1+t_2} i_c(t) dt + \int_{t_1+t_2}^{t_1+t_2+t_3} i_c(t) dt + \int_{t_1+t_2+t_3}^{T_s} i_c(t) dt \right]$$

$$= \frac{1}{T_s} \left[\frac{I_1 - I_4}{2} t_1 + \cancel{g_{L2}} + \frac{I_2 - I_3}{2} t_3 + \cancel{g_{L4}} \right]$$

$$g_{L2} = \int_{(2)} i_L dt = \int_{(2)} i_c dt = C_{sw} \Delta N_{sw} \omega_s \int_{(2)} = \underline{-C_{sw} V_g}$$

$$g_{L4} = \int_{(4)} i_L dt = \int_{(4)} i_c dt = \underline{C_{sw} V_g}$$

$$I_{out} = \frac{F}{2\pi} \left[\frac{I_1 - I_4}{2} \theta_1 + \frac{I_2 - I_3}{2} \theta_3 \right]$$

$$\left(\frac{1}{I_{base}} \right) I_{out} = \frac{1}{T_s} \left[\frac{I_1 - I_4}{2} t_1 + \frac{I_2 - I_3}{2} t_3 \right] \left(\frac{1}{I_{base}} \right) \left(\frac{\omega_s}{\omega} \right)$$

$$\text{Define } F = \frac{t_s}{T_s} = \frac{\omega_s}{\omega}$$

Normalized Period

$$t_1 + t_2 + t_3 + t_4 = T_s$$

$$\theta_1 + \beta + \theta_3 + \delta = \frac{\omega_0}{f_0} = \frac{2\pi}{F}$$

total:

8 equations



unknowns: ζ_1 ζ_2 ζ_3 ζ_4 } $\textcircled{8}$
 θ_1 β θ_3 δ }

Design of hardware $\&$ op point

M , J_{out} , F

L $\&$ C_{sw}
