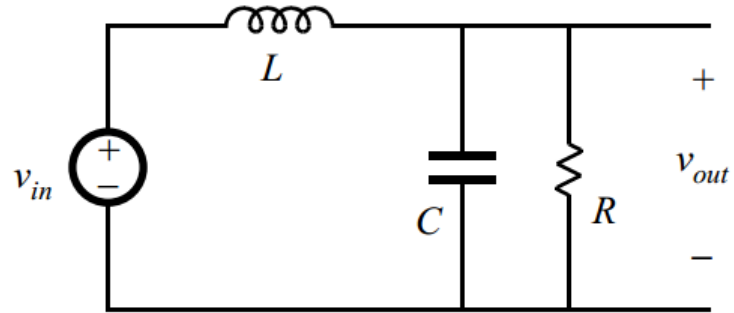
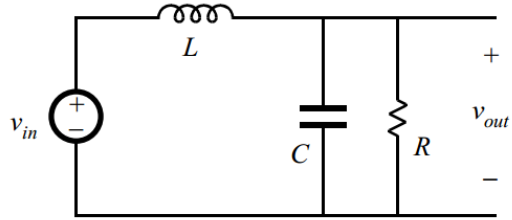


Resonant Circuits



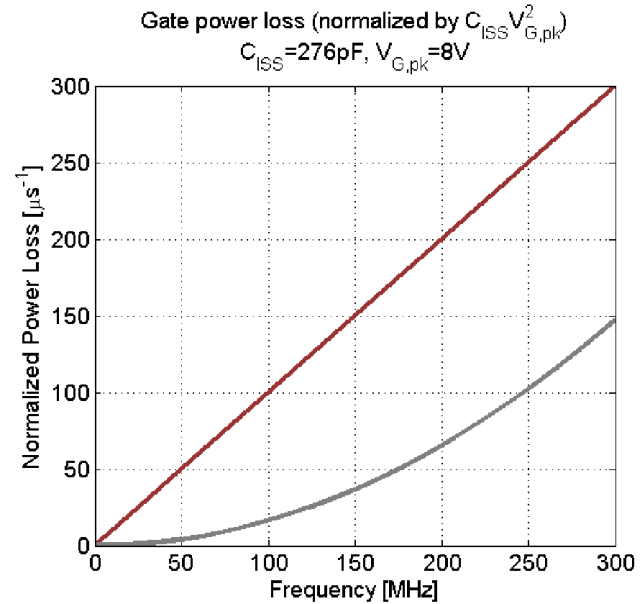
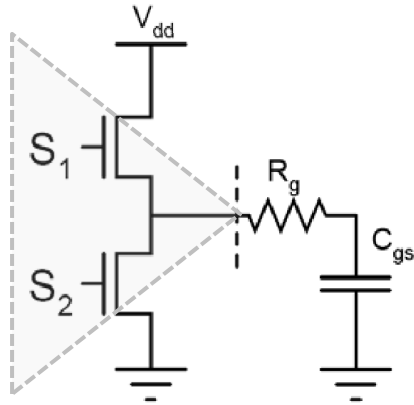
Resonant Circuit Analysis



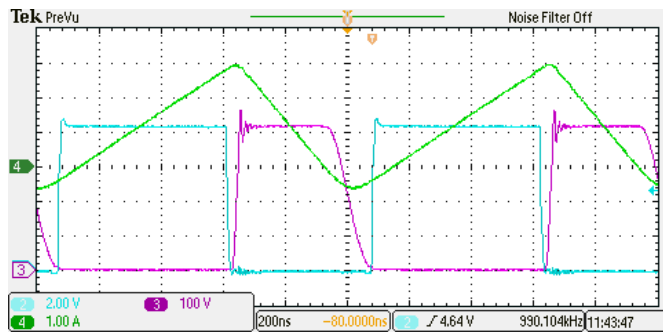
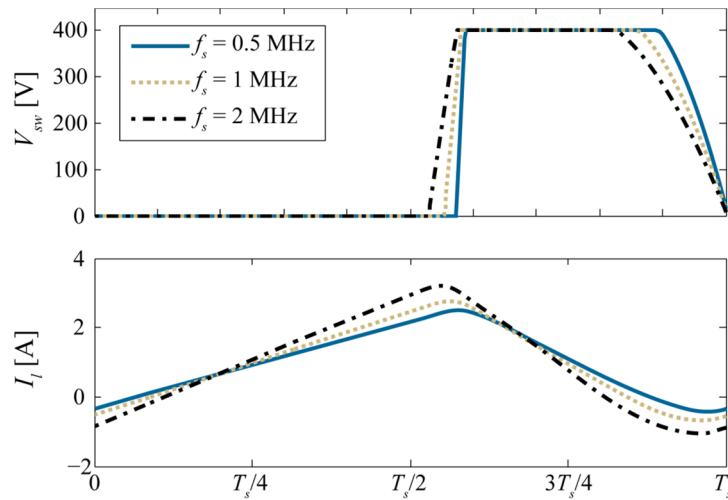
Soft Switching

- Advantages
 - Reduced switching loss
 - Possible operation at higher switching frequency
 - Lower EMI
- Disadvantages
 - Increased current and/or voltage stresses due to circulating current
 - Higher peak and rms current values
 - Complexity of analysis and modeling

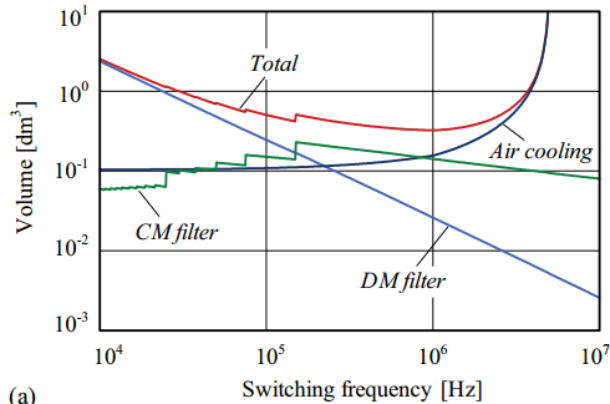
Limitations: Gate Drive



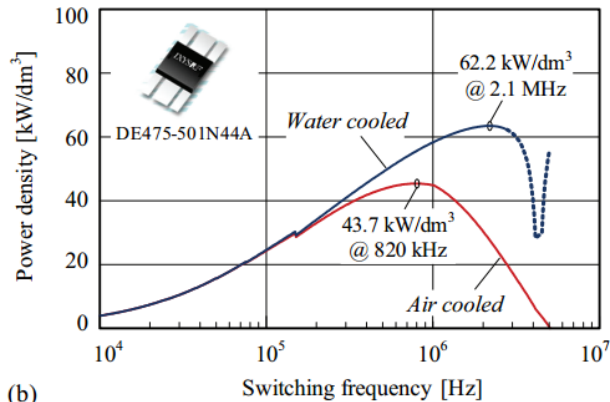
Limitations: t_d/T_s



Limitations: Thermal

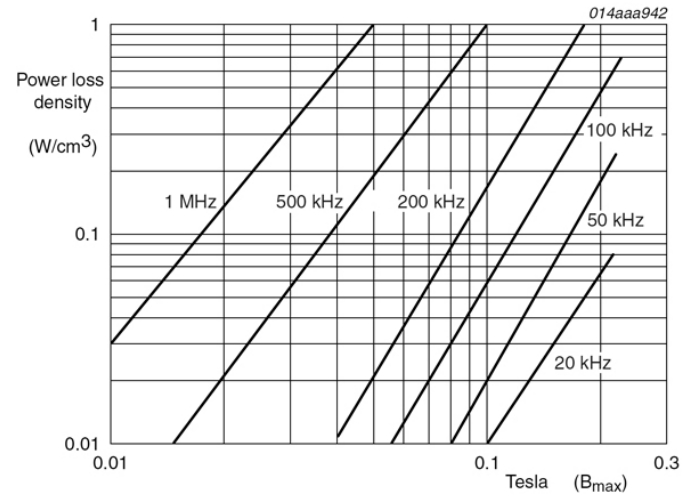
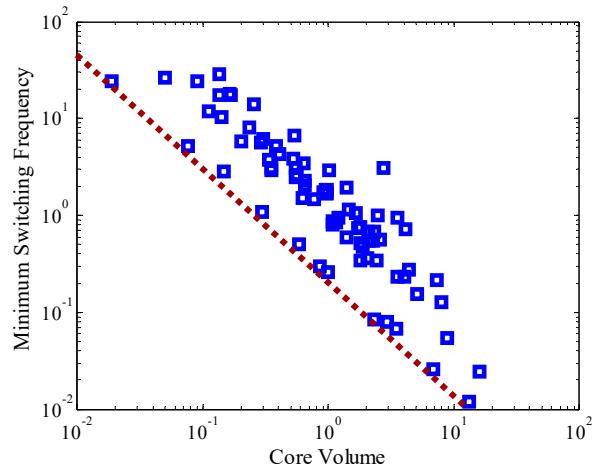


(a)

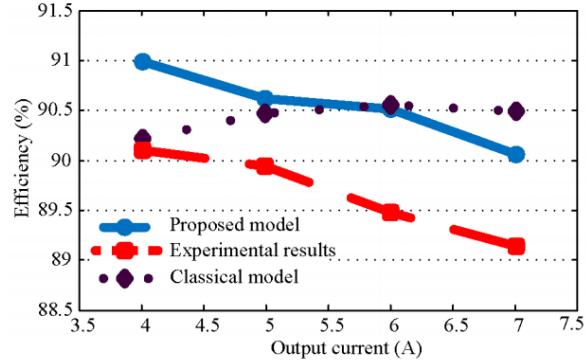
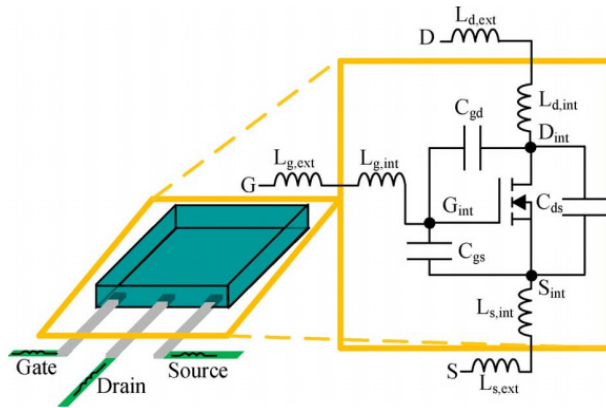


(b)

Limitations: Magnetics Design



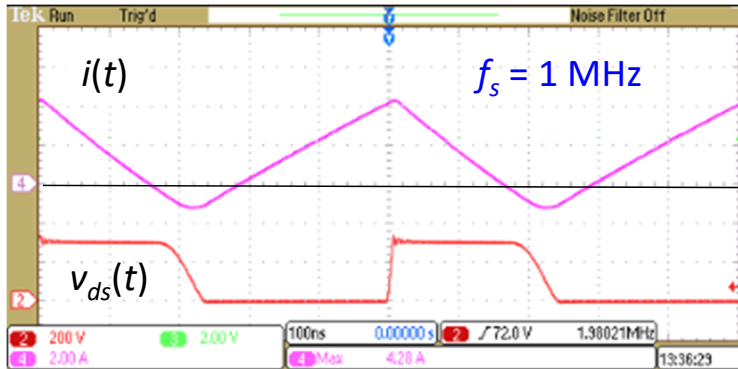
Limitations: Circuit Modeling



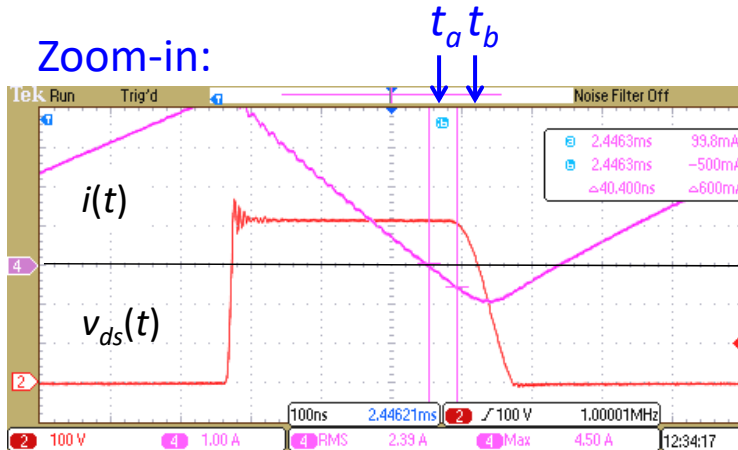
150-to-400V, 150W Boost

EXPERIMENTAL EXAMPLE

ZVS with Si diode



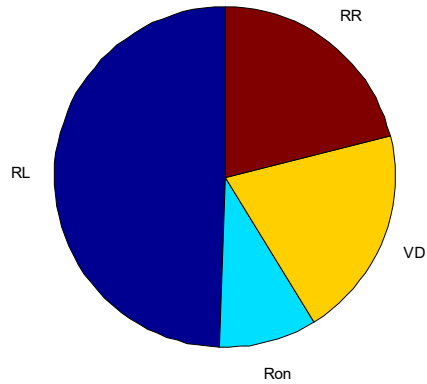
Zoom-in:



- ZVS turn-ON
 - Eliminated losses due to C_{sw} discharge during turn-ON transient
 - Eliminated losses due to MOSFET di_F/dt during turn-ON transient
- Diode reverse recovery still impacts the waveforms and losses
- Increased current ripple
 - Increased conduction losses (by >30%)
 - Increased dv_{ds}/dt upon turn-OFF, MOSFET turn-OFF speed is more important

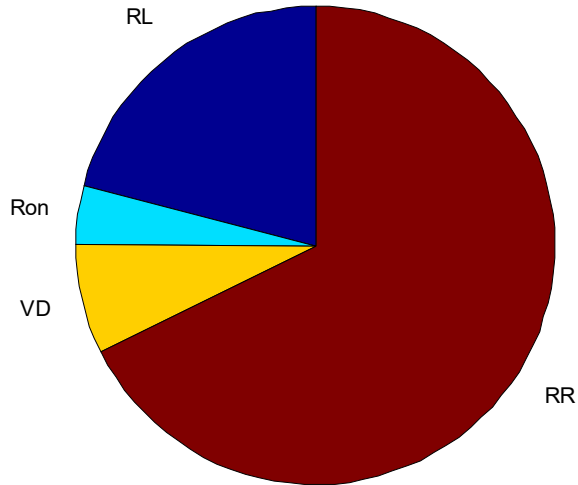
Loss Breakdown: Soft-Switched Si Boost

$f_s = 100 \text{ kHz}$
 $P_{loss} = 5.7 \text{ W}, \eta = 98.1\%$



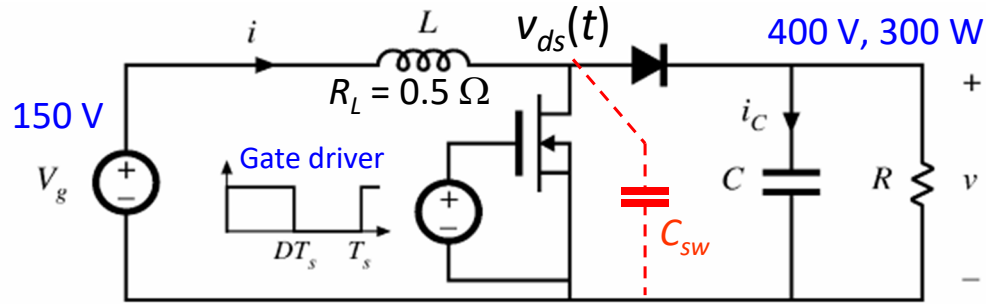
Reverse-recovery:
21% of the total loss

$f_s = 1 \text{ MHz}$
 $P_{loss} = 17.7 \text{ W}, \eta = 94.4\%$
Experiment: $\eta = 95.1\%$

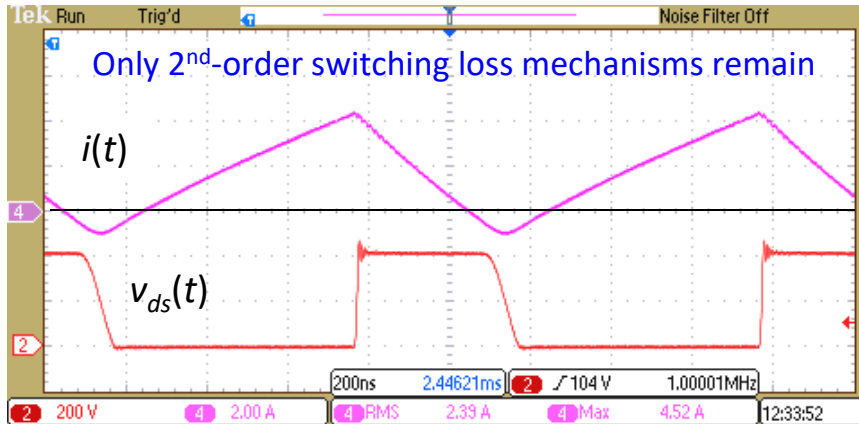


Reverse-recovery:
68% of the total loss

Soft-switched SiC diode



SiC diode, “soft-switched” operation



MOSFET

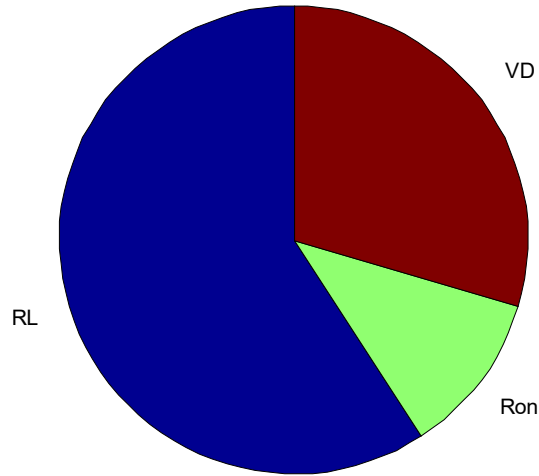
- $di_T/dt = 200 \text{ A}/\mu\text{s}$
- $C_{ds,eq} = 45 \text{ pF}$
- $R_{on} = 0.15 \Omega$

SiC diode

- $t_{rr} = 0, Q_{rr} = 0$
- $2C_{d,Req} - C_{d,eq} = 64 \text{ pF}$
- $V_D = 1.8 \text{ V}$

Soft-switched Boost with SiC diode

Conduction losses only, 2nd-order switching losses not included in the model



100 kHz or 1 MHz
98.5% efficiency
 $P_{loss} = 4.5 \text{ W}$

Experiments:

98.7% at 1 MHz
98.0% at 2 MHz

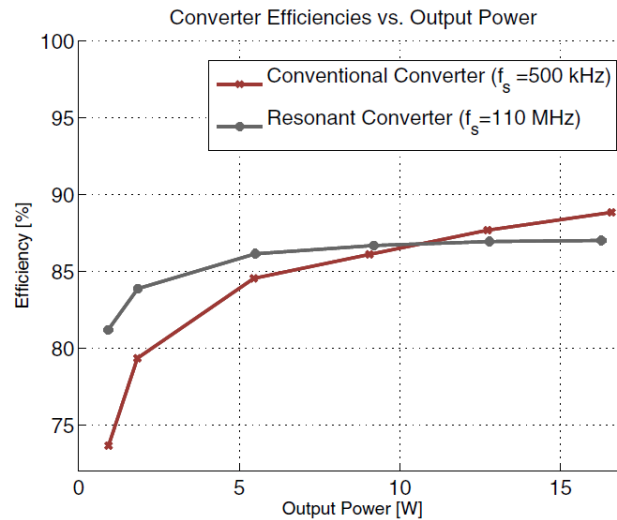
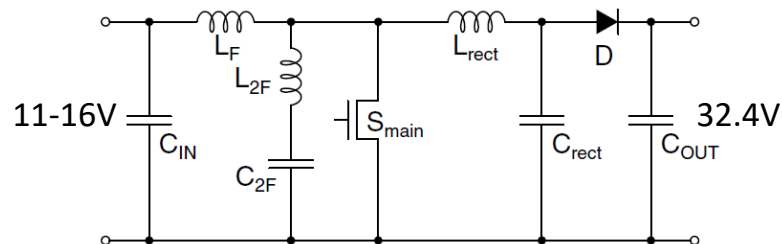
Power supply technology limits become dominated by:

- Magnetics
- 2nd-order switching loss mechanisms, e.g. gate-drive losses, parasitic inductances (layout and packaging)
- Gate-drive circuitry and controllers to support high-frequency operation

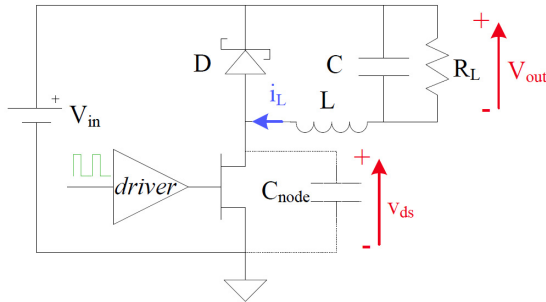
VHF power electronics [11]

Component	Resonant Design	
	Value	Type
L_F	33 nH	Coilcraft 1812SMS
L_{2F}	12.5 nH	Coilcraft A04TG
L_{rect}	22 nH	1812SMS
C_{2F}	39 pF	ATC100A
C_{rect}	10 pF	ATC100A
C_{out}	75 μ F	Multilayer Ceramics
C_{in}	22 μ F	Multilayer Ceramics
S_{main}		Freescale MRF6S9060
D		Fairchild S310

Component	Conventional Design	
	Value	Type
L_{boost}	10 μ H	Coilcraft D03316T-103ML
C_{out}	75 μ F	Multilayer Ceramics
C_{in}	22 μ F	Multilayer Ceramics
S_{main}		LT1371HV
D		Fairchild S310



WBG Devices



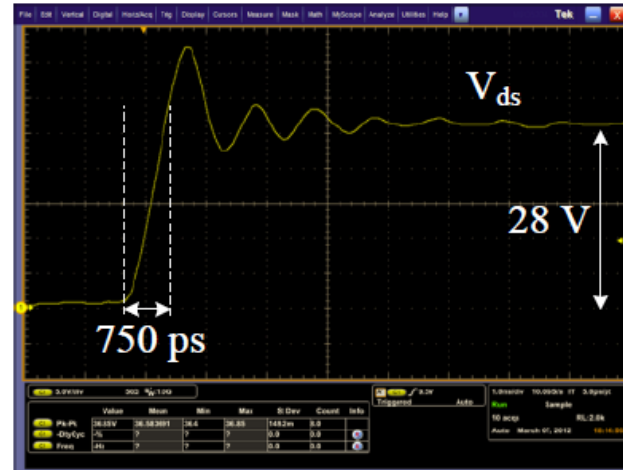
Standard hard-switched PWM operation at 50 MHz
 dv_{ds}/dt dominated by probe (4 pF) capacitance

TriQuint TGF2023-02
12W, DC-to-18 GHz
RF/microwave HEMT

FOM for switching applications

$$C_{ds}R_{on} \approx 1 \Omega\text{pF}$$

$$Q_gR_{on} \approx 10 \Omega\text{pC}$$



Emerging GaN HEMT devices may enable completely new RF-based design approaches in power electronics

Topics Covered

- High Frequency Power Conversion
 - Switching losses and device selection
 - Nonlinear device capacitances
 - Resonance in power electronics
 - Soft switching (ZVS and ZCS)
- Resonant Converters
 - State-plane analysis
 - Resonant converter topologies
 - Sinusoidal analysis
 - AC-modeling and frequency modulation
- Non-resonant soft switching converters
 - State-plane analysis
 - Constant frequency control
 - Resonant switches
 - Modeling and Simulation
 - Discrete time models
- Switched capacitor converters
 - SSL and FSL operation
 - Charge vector modeling
 - Soft-charging operation
- Applications and practical issues of high frequency converters

HARD SWITCHING ANALYSIS

Synchronous Switching

