

Closed-Form Solution

$$\gamma = \frac{F}{\pi} 2M_1$$

$$\frac{\pi}{F} = \alpha + \beta$$

$$M_1 = \frac{2 \tan \frac{\alpha}{2} \tan \frac{\beta}{2}}{1 - \tan \frac{\alpha}{2} \tan \frac{\beta}{2}}$$

$$\gamma = \frac{F}{\pi} 4 \frac{\tan \frac{\alpha}{2} \tan \frac{\beta}{2}}{1 - \tan \frac{\alpha}{2} \tan \frac{\beta}{2}}$$

$$\alpha = \frac{\pi}{F} - \beta$$

$$\gamma = \frac{F}{\pi} 4 \frac{\tan \left(\frac{\pi}{2F} - \frac{\beta}{2} \right) \tan \left(\frac{\beta}{2} \right)}{1 - \tan \left(\frac{\pi}{2F} - \frac{\beta}{2} \right) \tan \frac{\beta}{2}}$$

$$\gamma = f(F, \beta)$$

Control

$$\begin{cases} \alpha = 2 \tan^{-1} \left(\frac{M_1}{J_1} \right) \\ \beta = 2 \tan^{-1} \left(\frac{J_1}{2 + M_1} \right) \end{cases}$$

$$M_1 = \tan \left(\frac{\alpha}{2} \right) J_1$$

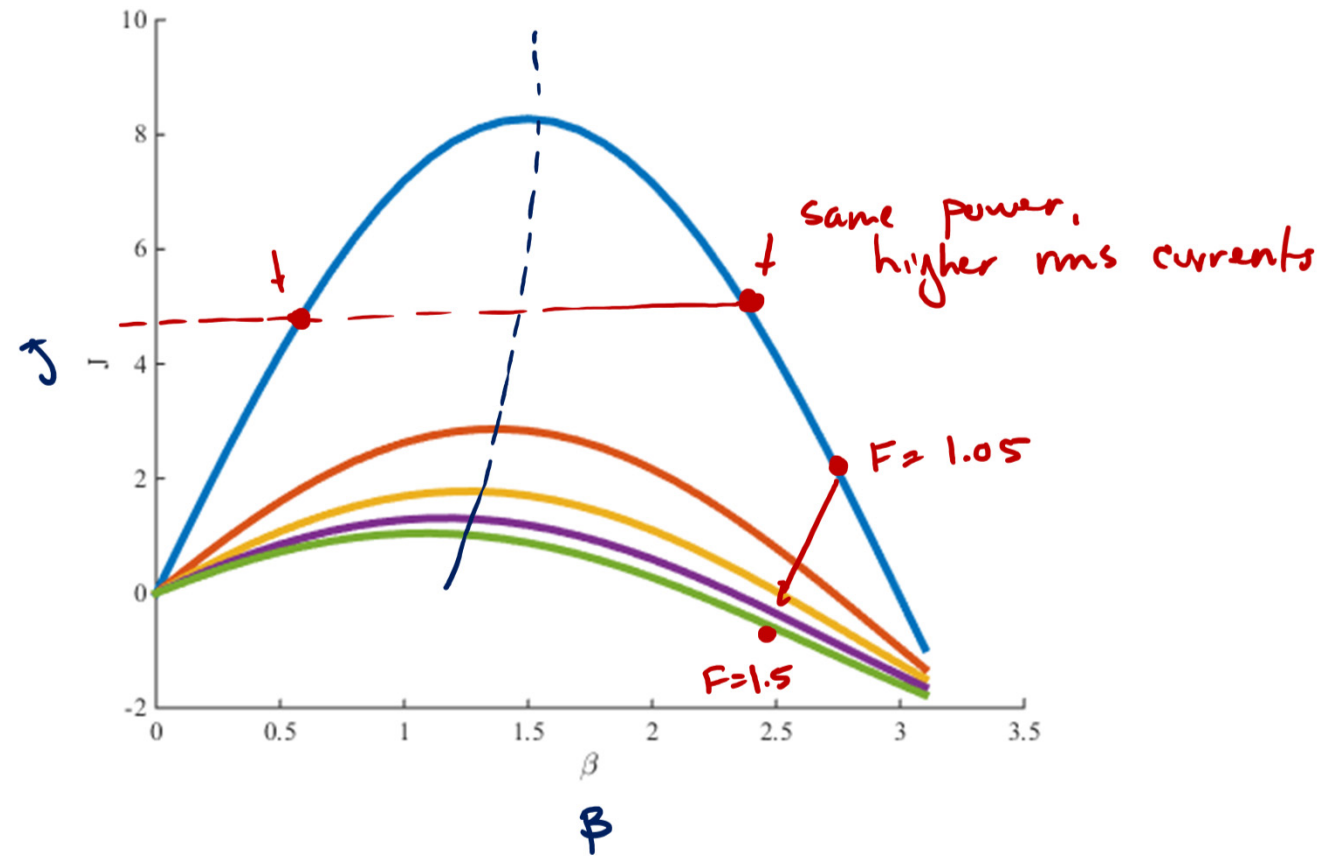
$$J_1 = \tan \left(\frac{\beta}{2} \right) (2 + \tan \frac{\alpha}{2} J_1)$$

$$J_1 = \frac{2 \tan \frac{\beta}{2}}{1 - \tan \frac{\beta}{2} \tan \frac{\alpha}{2}}$$

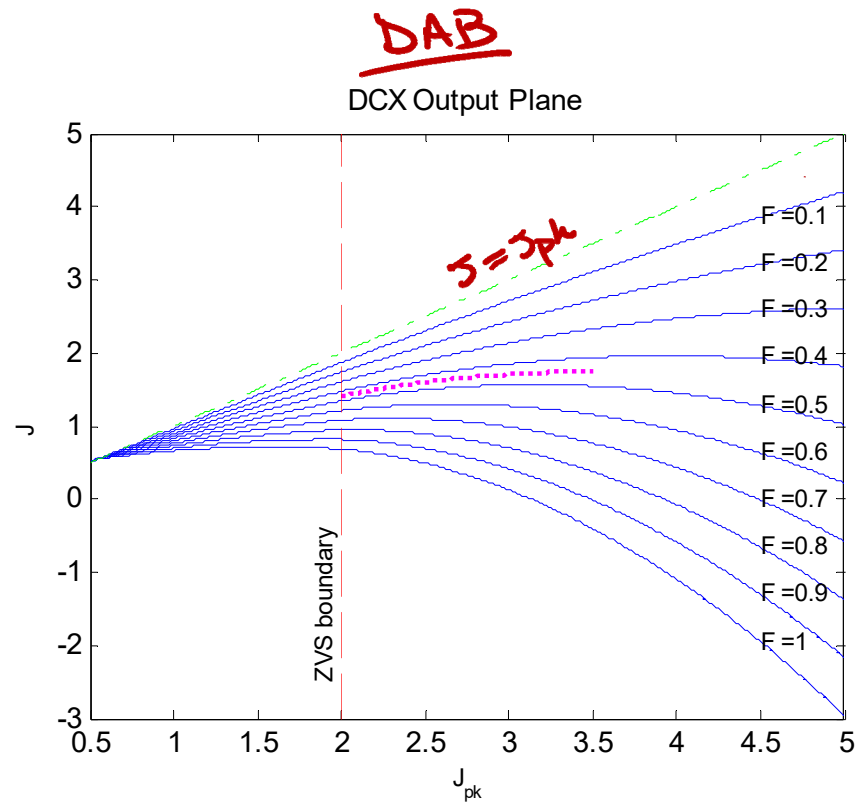
SRC Control Trajectory

$$F = \frac{f_s}{f_0} \geq 1 \text{ for this SRC mode operation}$$

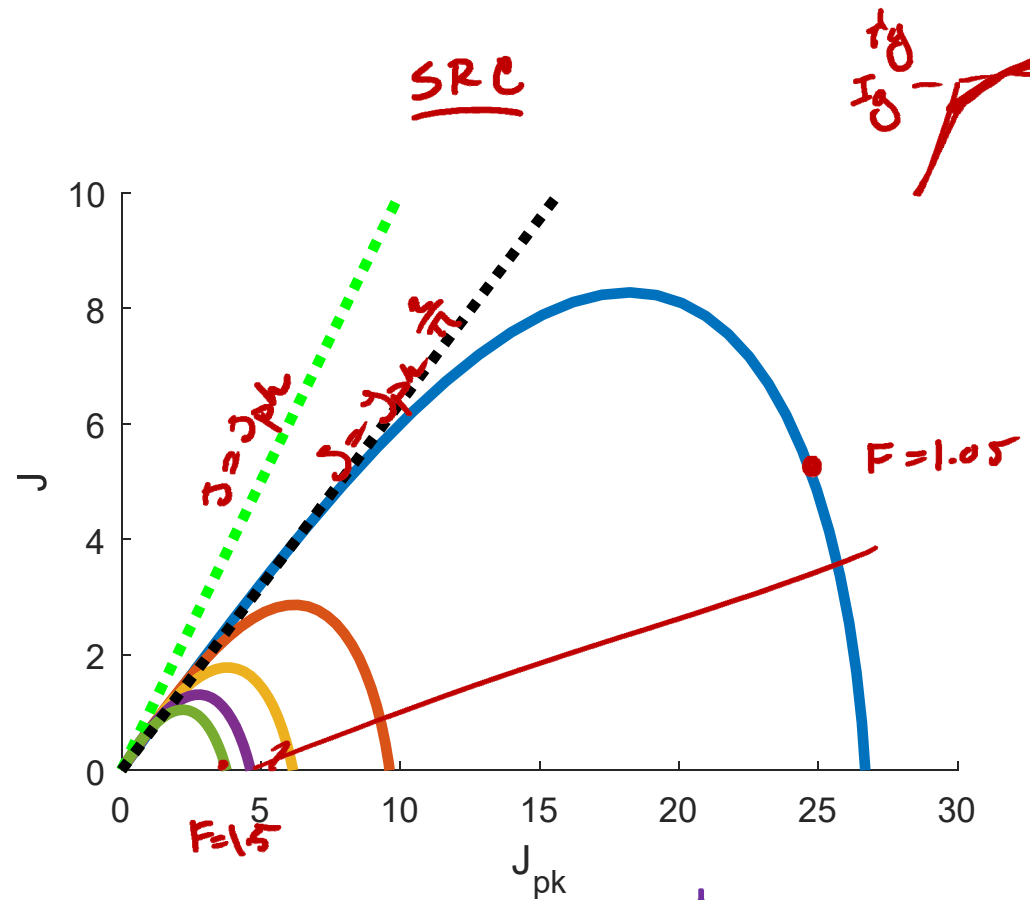
↳ gives possibility of ZVS



SRC Current Stress



$$\omega \mid \omega_0 = \frac{1}{\sqrt{L_e C_p}}$$

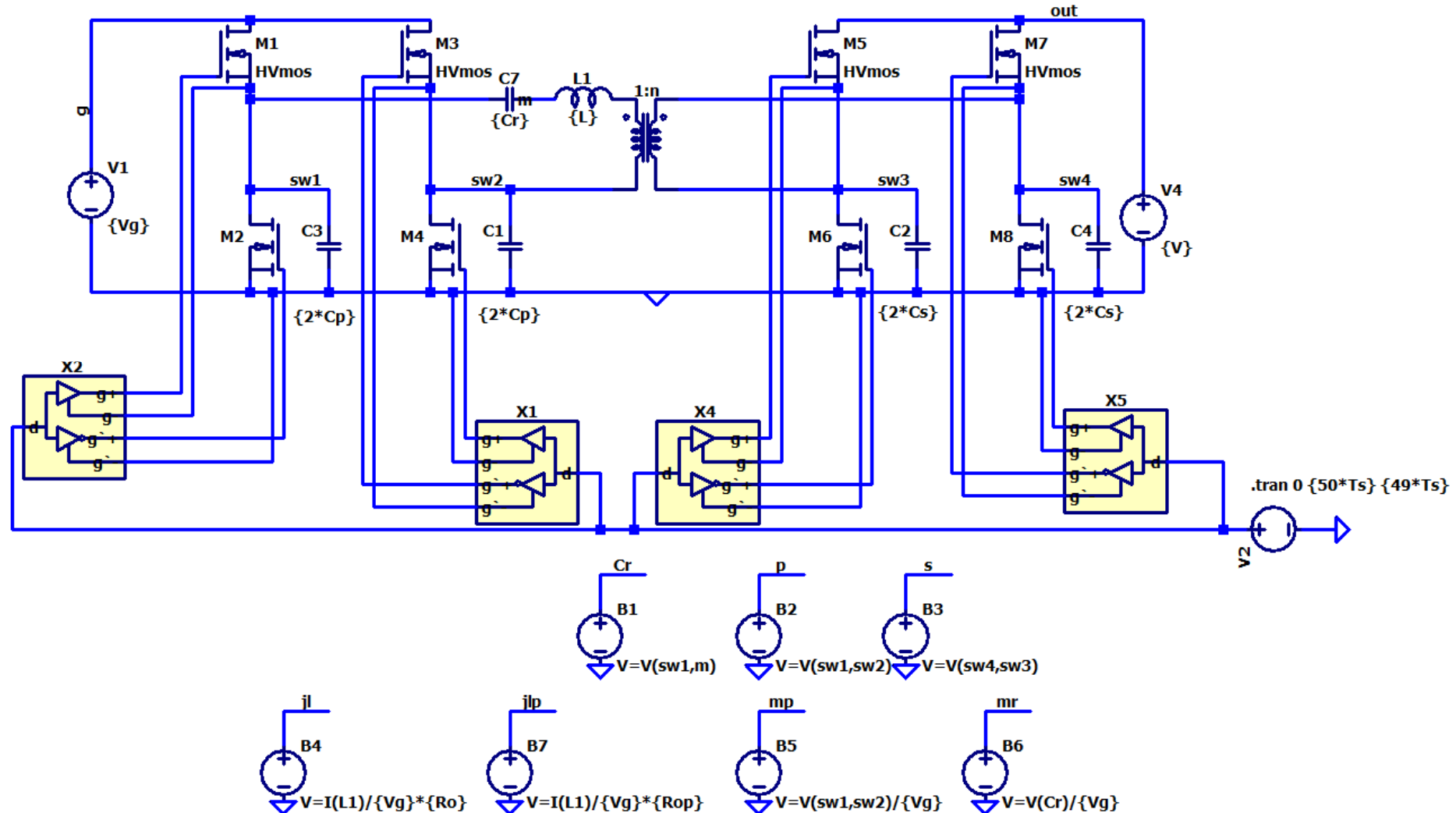


$$\omega \mid \omega_0 = \frac{1}{\sqrt{L_e C_r}}$$

$C_p \neq C_s$ neglected

Example Simulation

```
.param Cr={150n} Ro={{(L/Cr)**.5} td=70n phi={Ts/2+150n} Rop={{(L/Cp)**.5}
.param fs=750k Ts={1/fs} Vg=100 V={Vg} C={100u} Cp=200p Cs={Cp} L={10u}
```



SRC Simulation

$$I_{out} = 2A$$

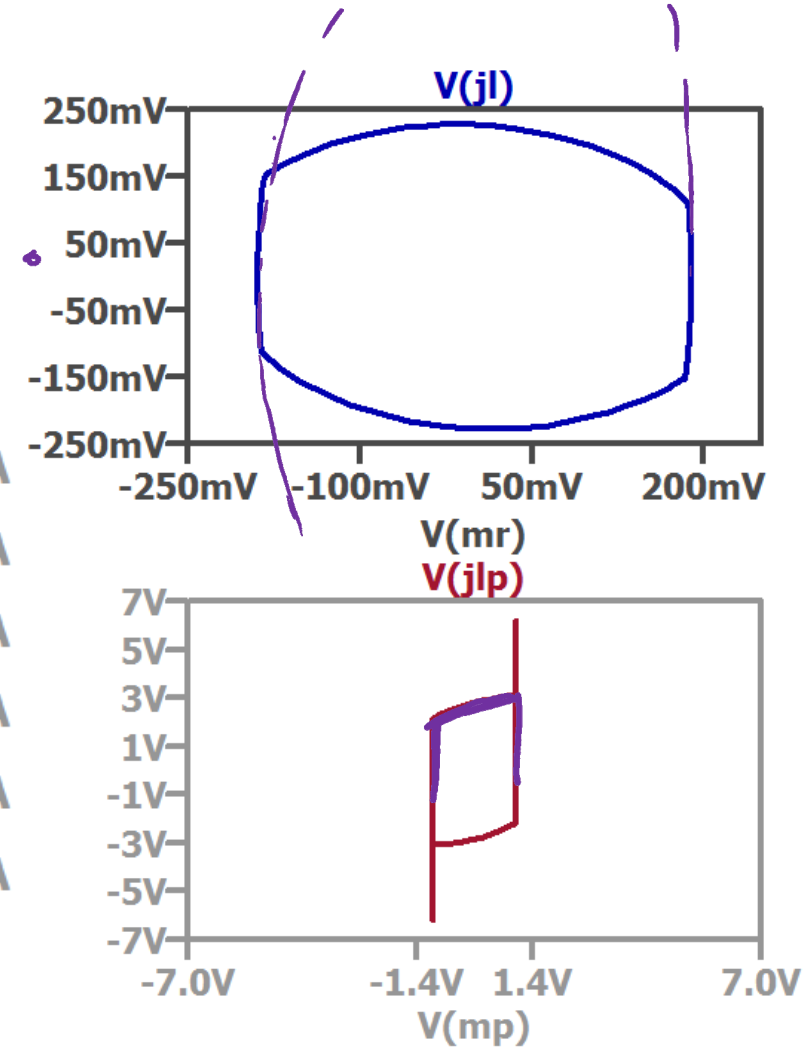
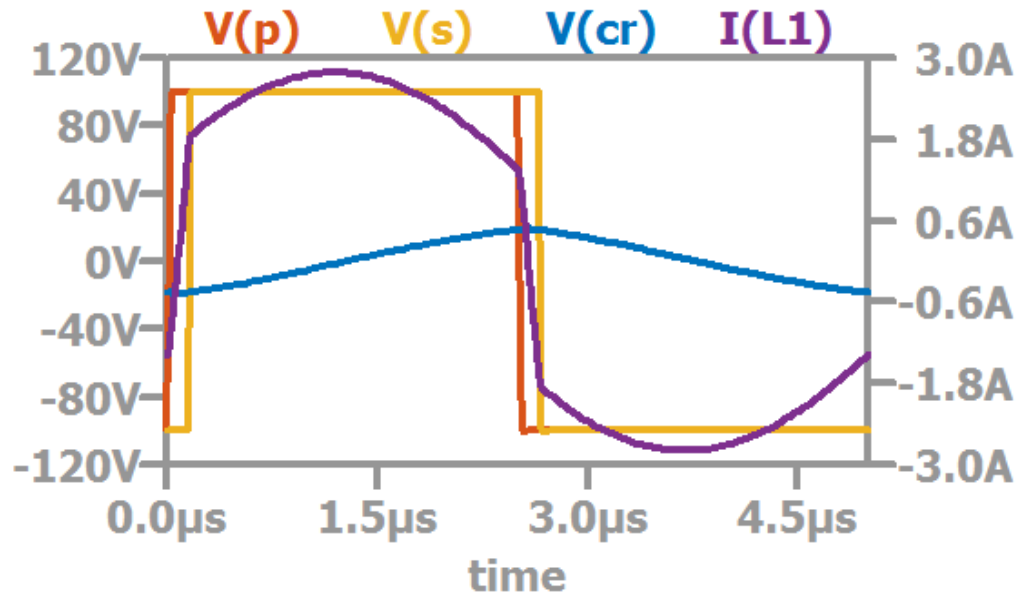
$$f_s = 200kHz$$

$$f_o = 130kHz$$

$$V_g = 100V$$

$$V_{out} = 100V$$

$$\Rightarrow \frac{f_s}{f_o} > \phi$$



SRC Simulation

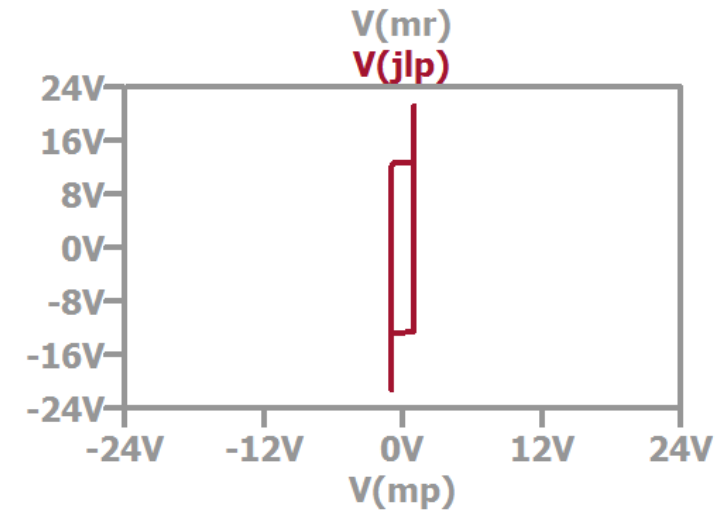
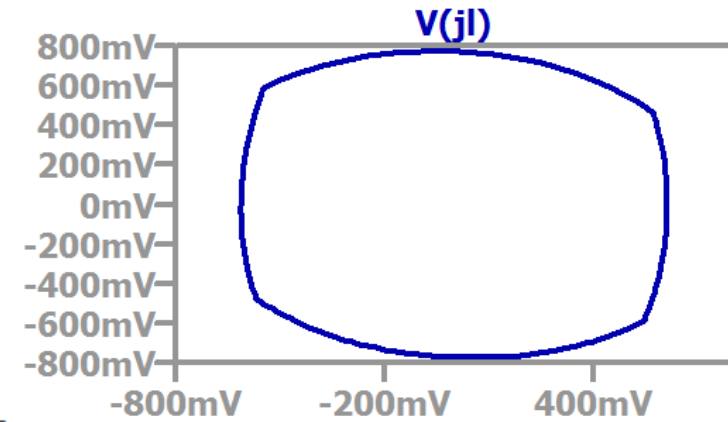
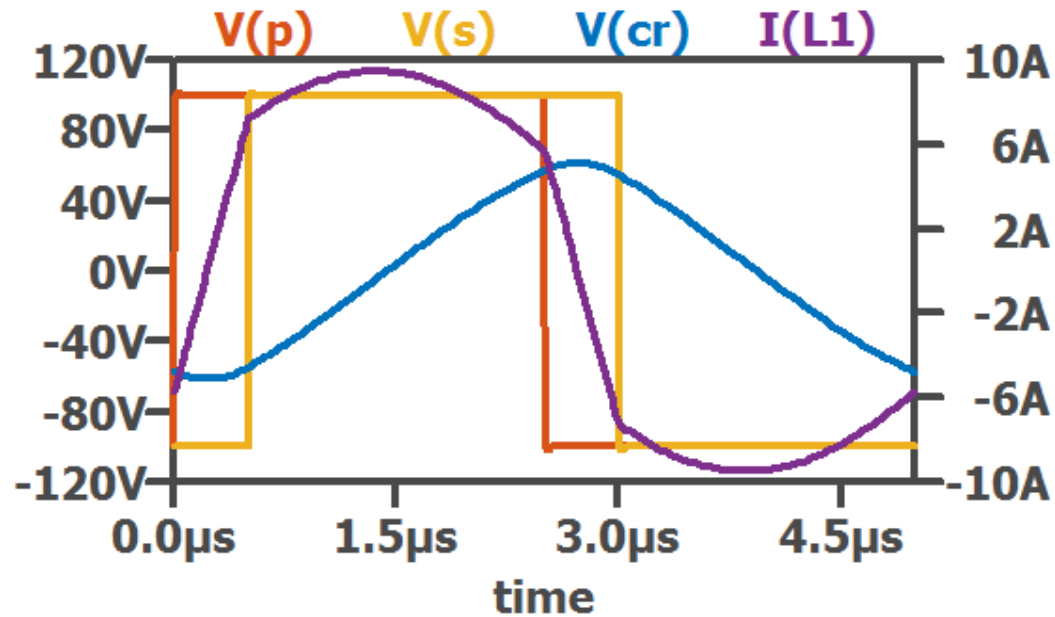
$$I_{out} = 6.5A$$

$$f_s = 200kHz$$

$$f_o = 130kHz$$

$$V_g = 100V$$

$$V_{out} = 100V$$



SRC Simulation

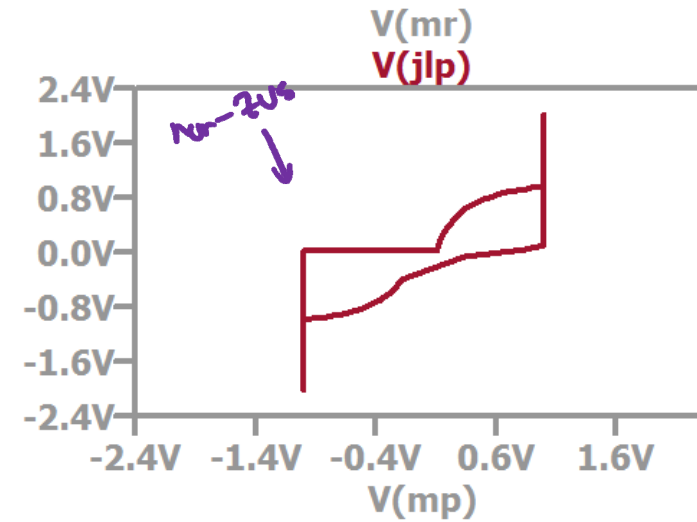
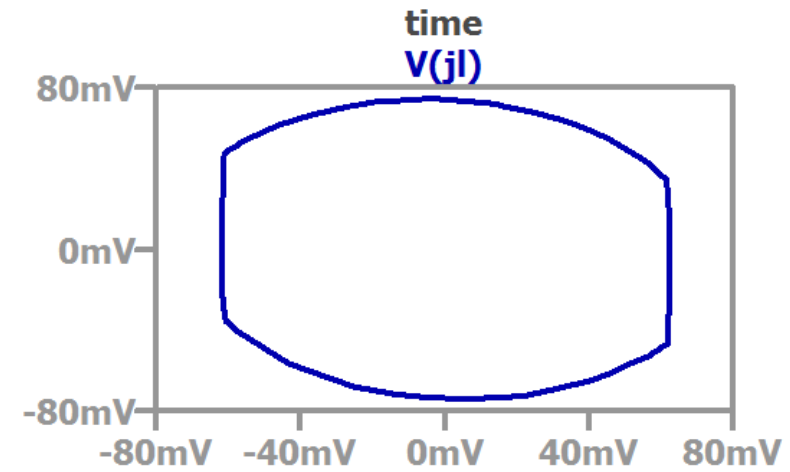
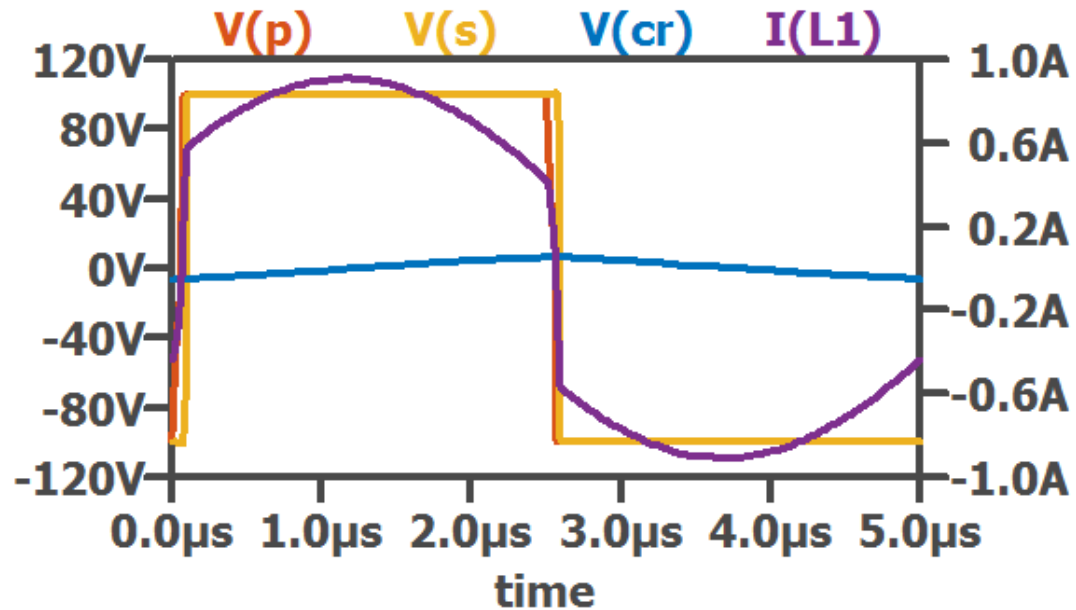
$$I_{out} = 500\text{mA}$$

$$f_s = 200\text{kHz}$$

$$f_o = 130\text{kHz}$$

$$V_g = 100\text{V}$$

$$V_{out} = 100\text{V}$$



SRC Simulation

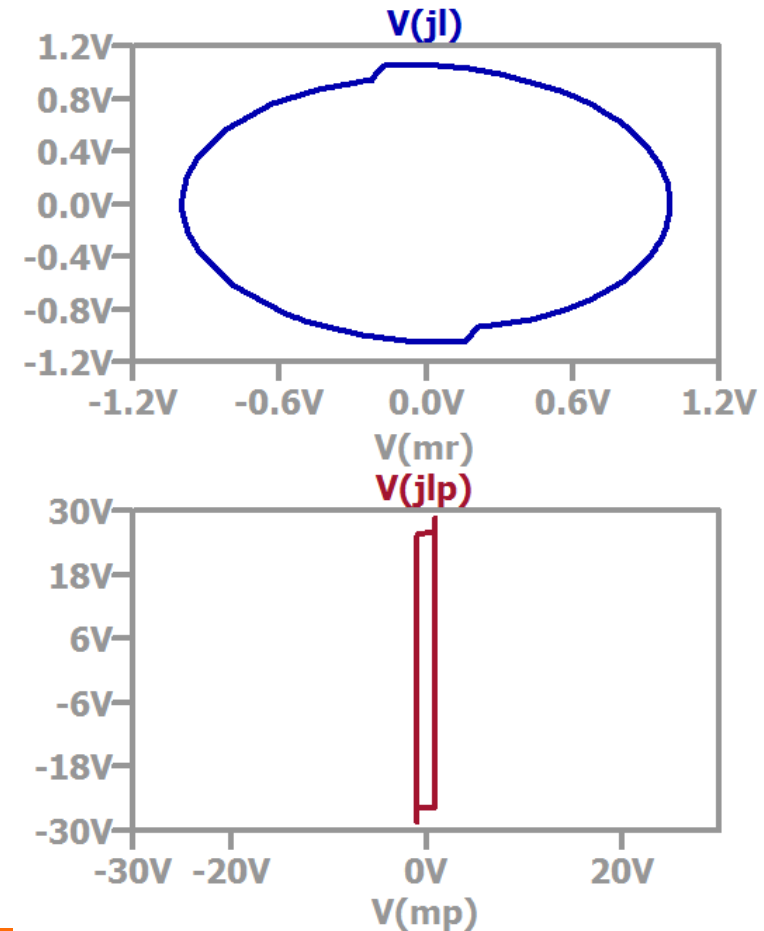
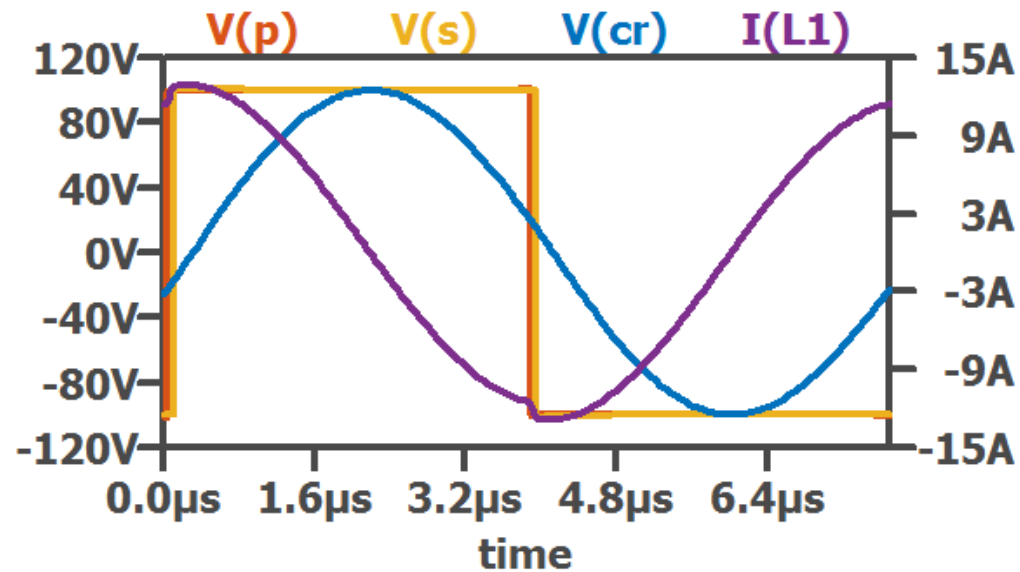
$$I_{out} = 1.2A$$

$$f_s = 130kHz \quad \left. \vphantom{f_s} \right\} F=1$$

$$f_o = 130kHz$$

$$V_g = 100V$$

$$V_{out} = 100V$$



SRC Simulation

all cases
 $n=1$

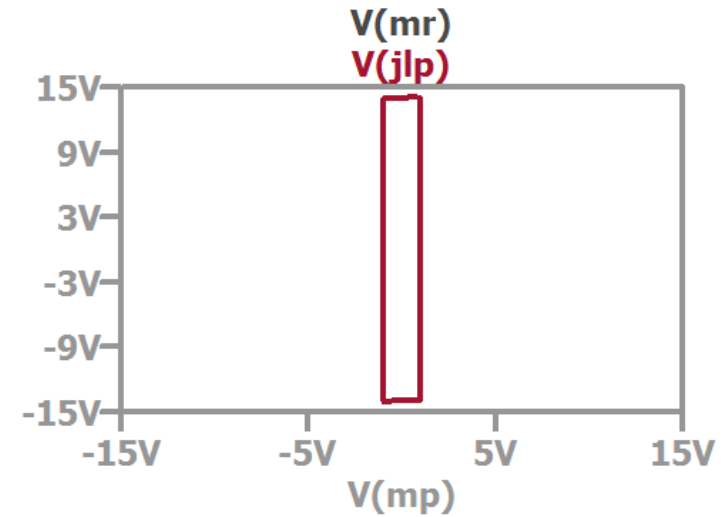
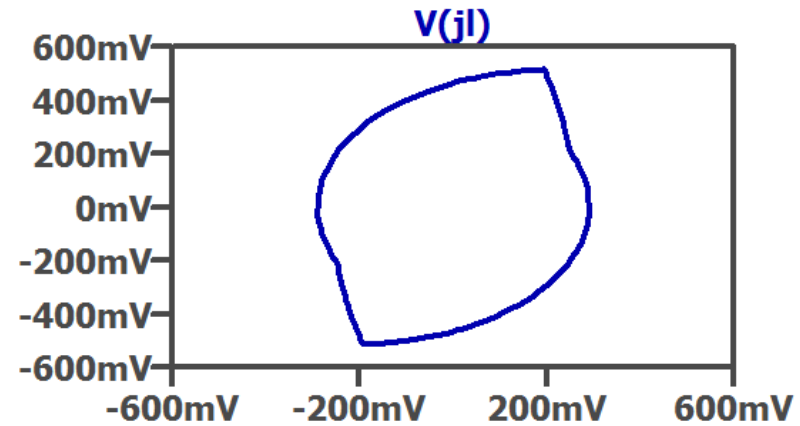
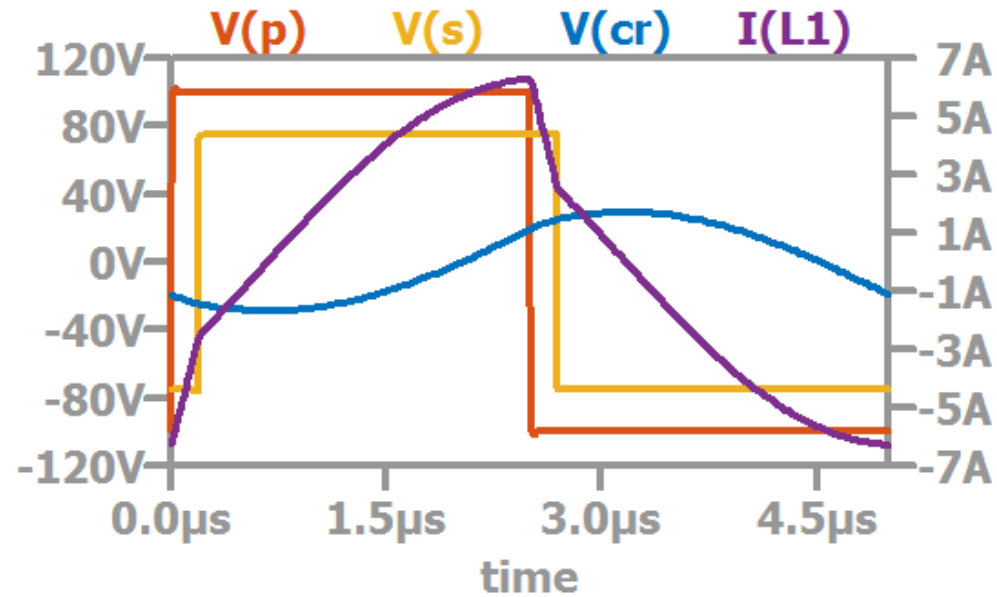
$$I_{out} = 3A$$

$$f_s = 200kHz$$

$$f_o = 130kHz$$

$$V_g = 100V$$

$$V_{out} = 75V$$



SRC Simulation

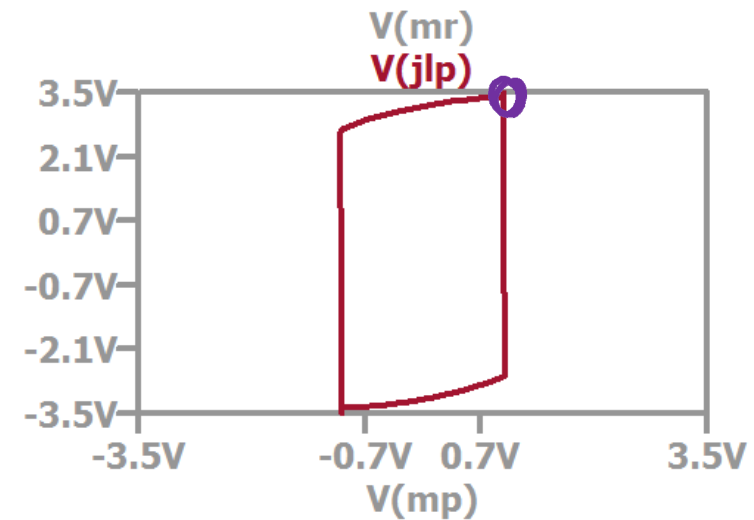
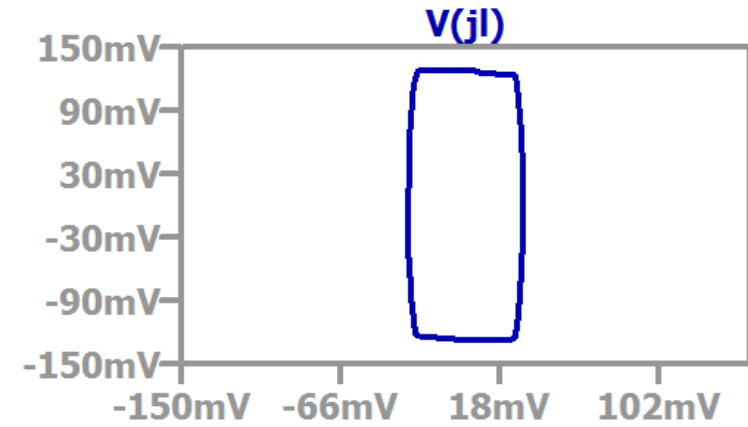
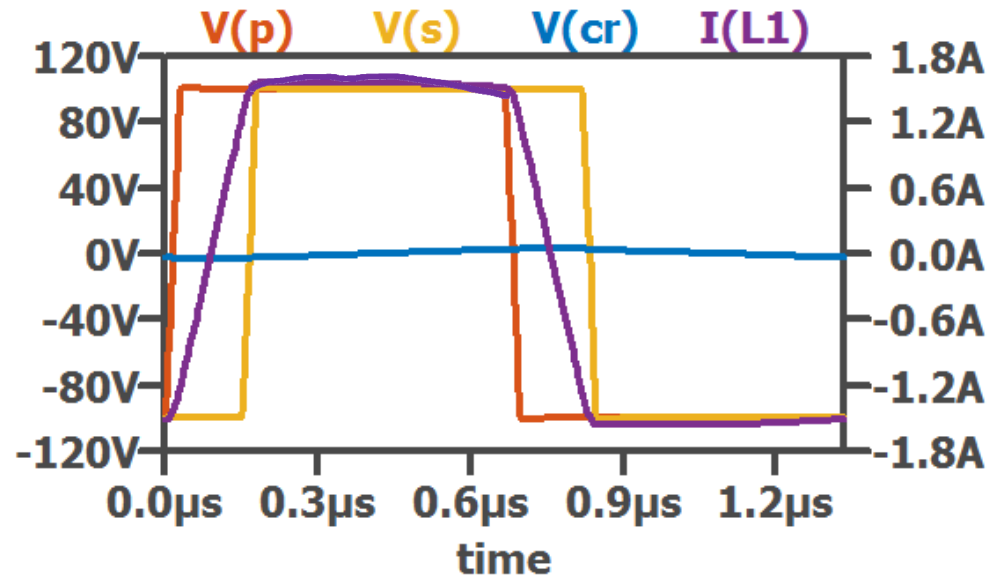
$$I_{out} = 1A$$

$$f_s = 750kHz \quad \left. \vphantom{f_s} \right\} F \gg f$$

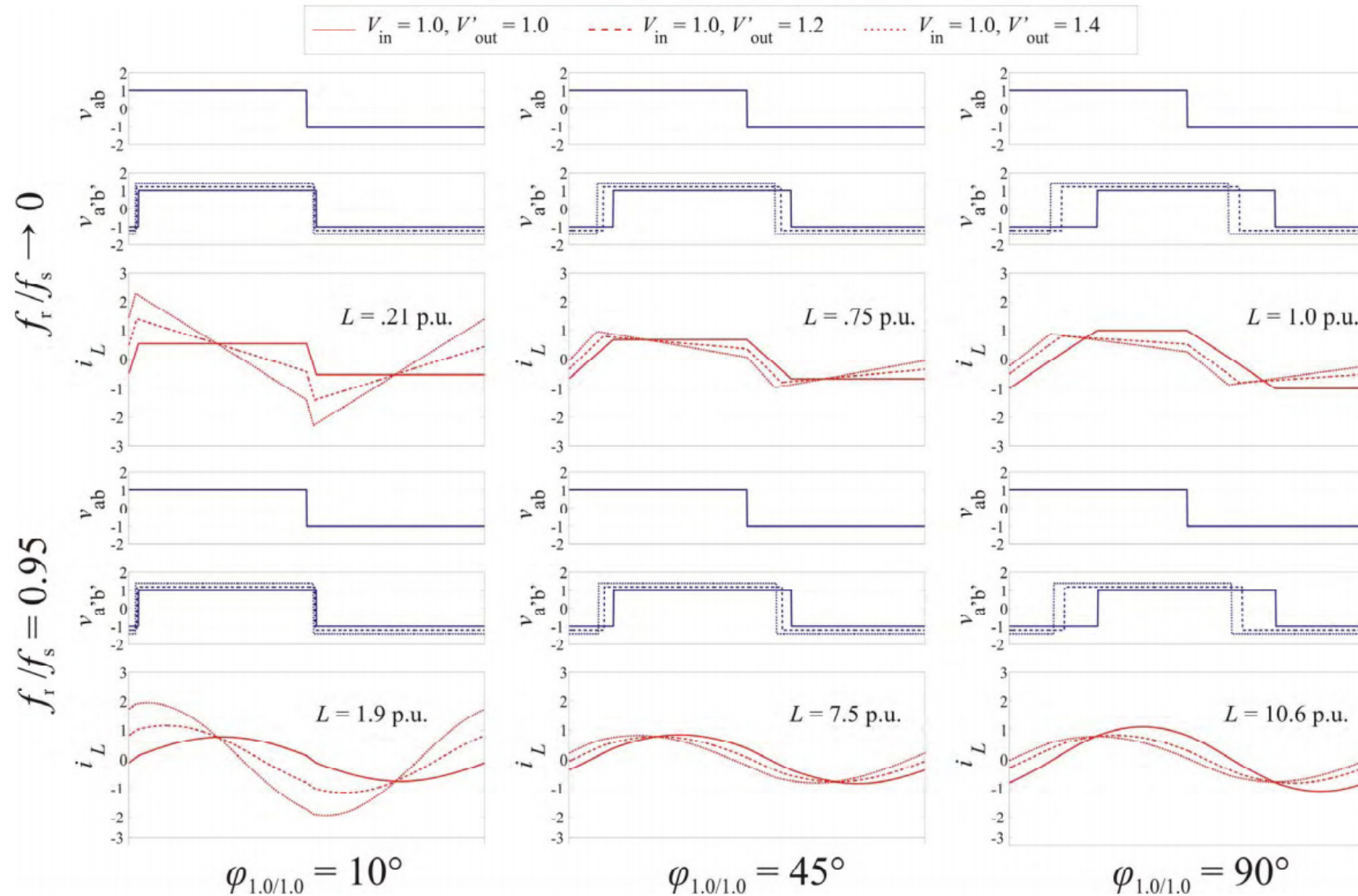
$$f_o = 130kHz$$

$$V_g = 100V$$

$$V_{out} = 100V$$



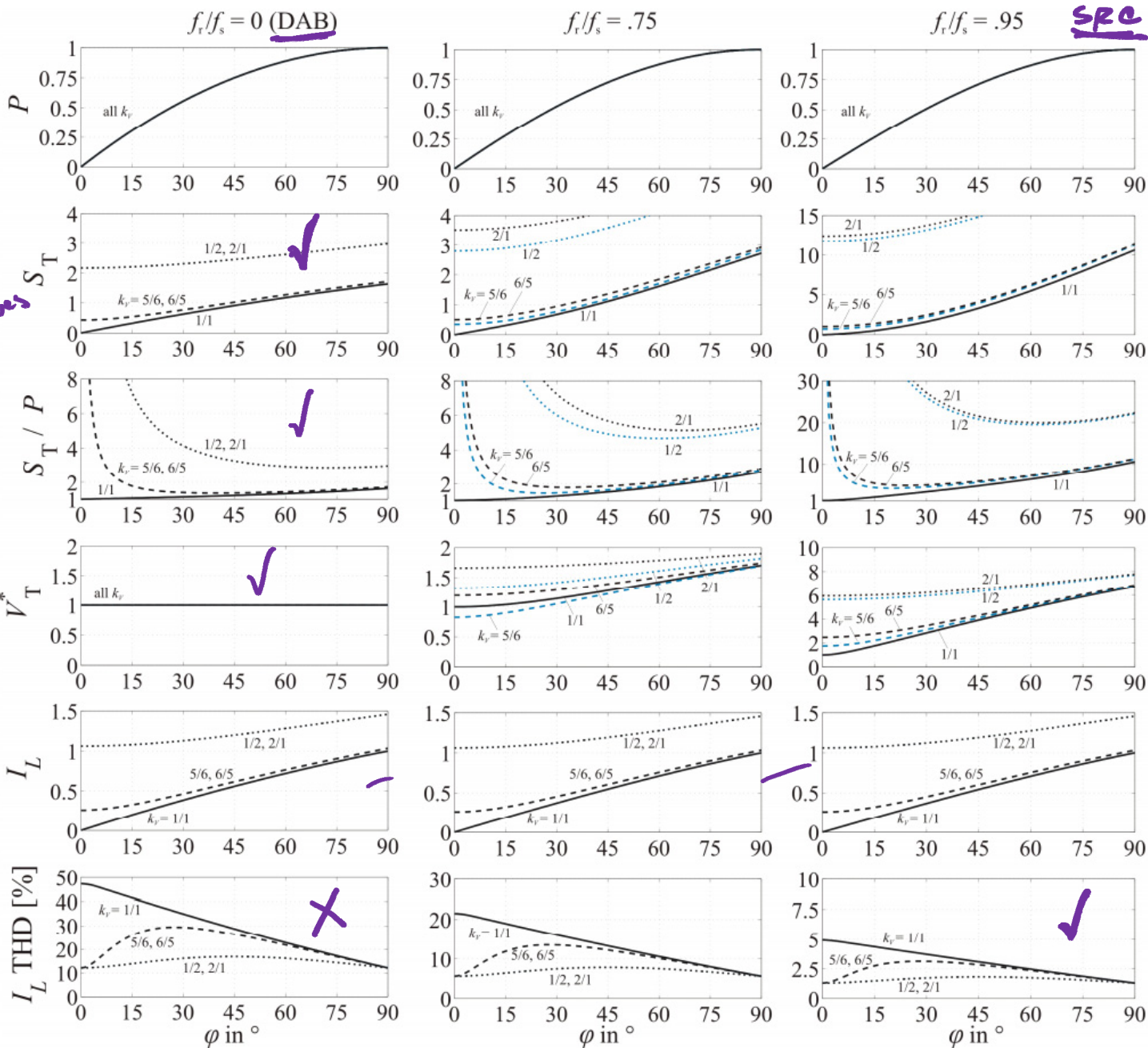
DAB vs SRC



Part
 $S_T = V_T \cdot I_T$
 V_T, I_T are rms values

XF voltage

Rms



DAB vs SRC: Conclusions

DAB

- + Smaller resonant tank
- + Smaller RMS currents
- + Wider Soft-switching range

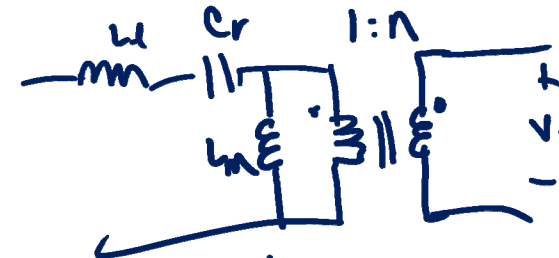
SRC

- + Can be designed with larger XF inductance
- + Lower AC winding losses
- + Reduced device turn-off losses



modify

LLE tank → SRC with extended ZVS range



↳ let L_m reduce from ∞