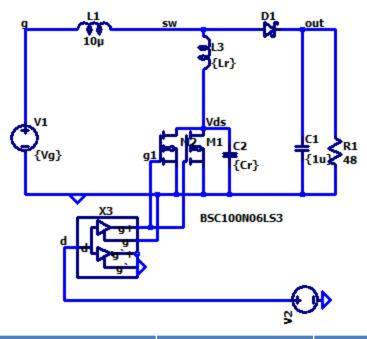
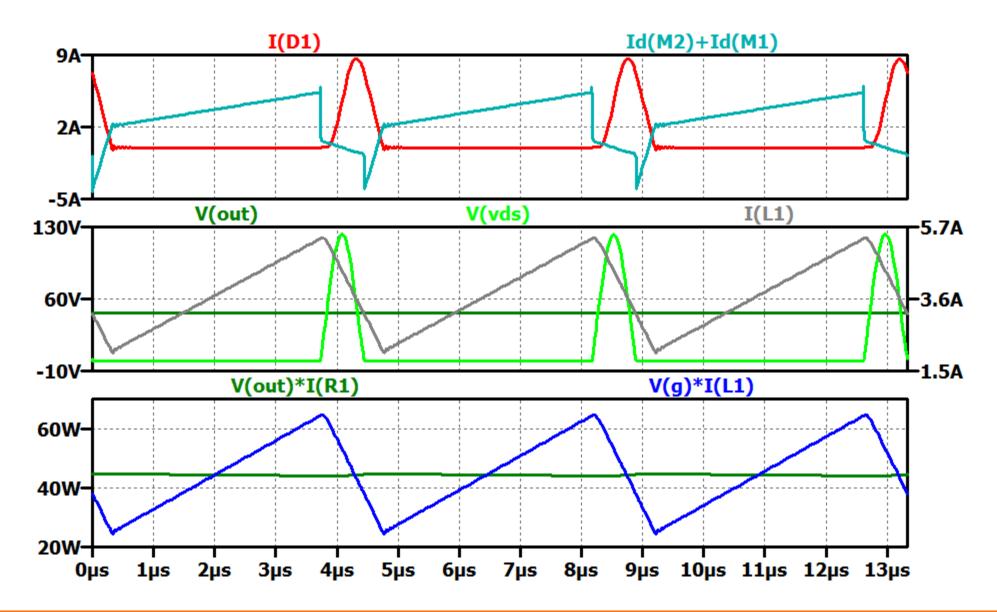
# **Resonant Operation**

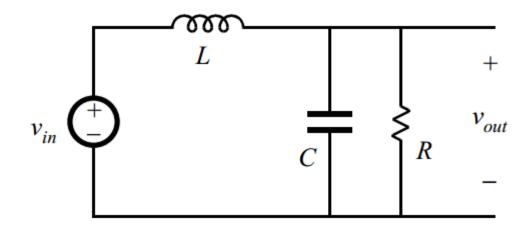


| Switching | L            | C <sub>out</sub> | $ f_{s} $ | Diode       | η (Sim) |
|-----------|--------------|------------------|-----------|-------------|---------|
| Hard      | 22uH         | 22uF             | 202k      | Si (FR)     | 93.9%   |
| Hard      | 22uH         | 22uF             | 202k      | Si Schottky | 95.8%   |
| Soft      | 4.65uH       | 22uF             | 202k      | Si Schottky | 98.4%   |
| Soft      | 710nH        | 4.4uF            | 1 MHz     | Si Schottky | 98.2%   |
| Soft      | 710nH        | 4.4uF            | 1 MHz     | MOSFET      | 99.6%   |
| Resonant  | 10uH + 2.4uH | 1uF + 10nF       | 225 kHz   | Si Schottky | 98.6%   |
| Resonant  | 10uH + 2.4uH | 1uF + 10nF       | 225 kHz   | MOSFET      | 99.96%  |

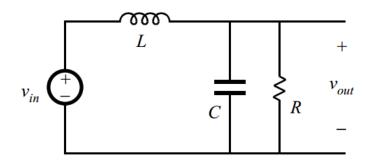
### **Resonant Boost Converter**



# **Resonant Circuits**



# **Resonant Circuit Analysis**

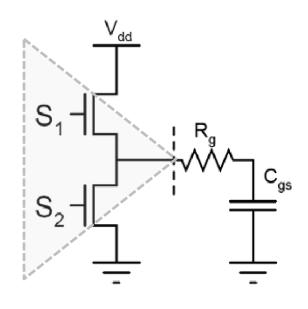


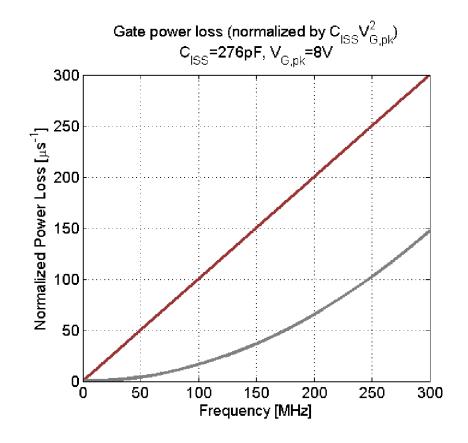


# **Soft Switching**

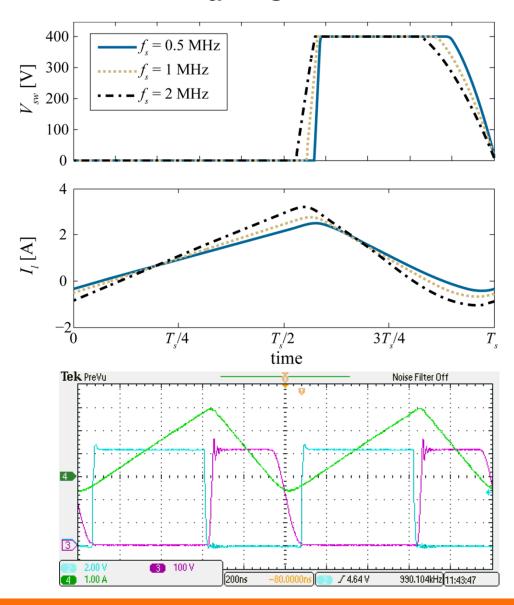
- Advantages
  - Reduced switching loss
  - Possible operation at higher switching frequency
  - Lower EMI
- Disadvantages
  - Increased current and/or voltage stresses due to circulating current
  - Higher peak and rms current values
  - Complexity of analysis and modeling

## **Limitations: Gate Drive**

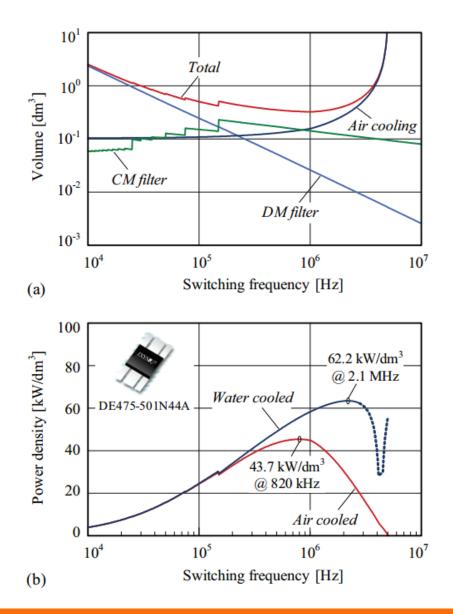




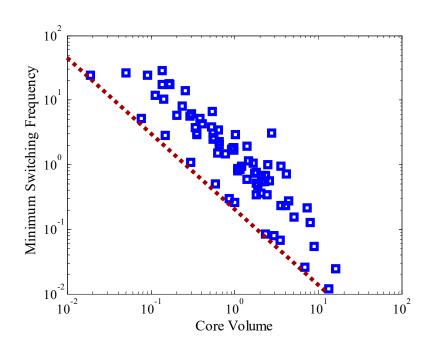
# Limitations: $t_d/T_s$

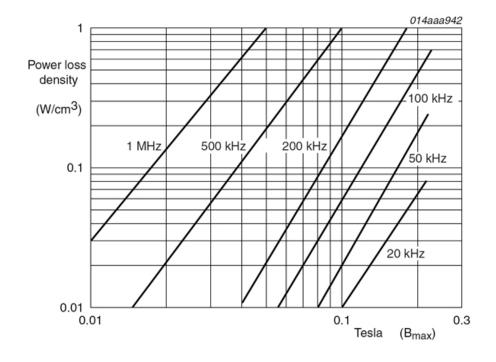


## **Limitations: Thermal**

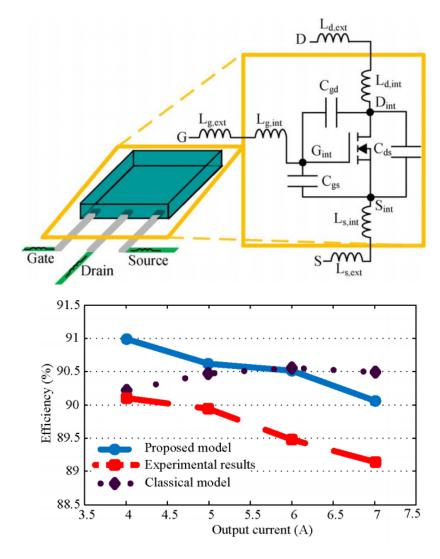


# Limitations: Magnetics Design





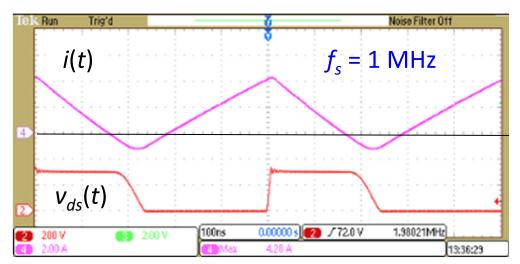
# **Limitations: Circuit Modeling**

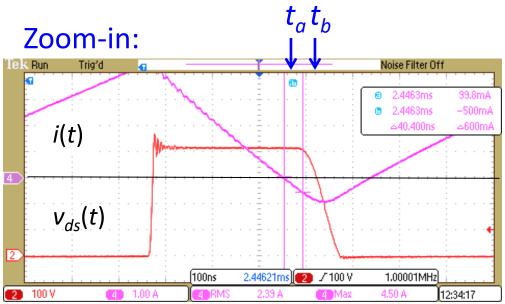


150-to-400V, 150W Boost

### **EXPERIMENTAL EXAMPLE**

### **ZVS** with Si diode



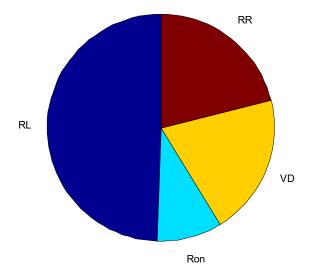


#### ZVS turn-ON

- Eliminated losses due to C<sub>sw</sub> discharge during turn-ON transient
- Eliminated losses due to MOSFET di<sub>F</sub>/dt during turn-ON transient
- Diode reverse recovery still impacts the waveforms and losses
- Increased current ripple
  - Increased conduction losses (by >30%)
  - Increased  $dv_{ds}/dt$  upon turn-OFF, MOSFET turn-OFF speed is more important

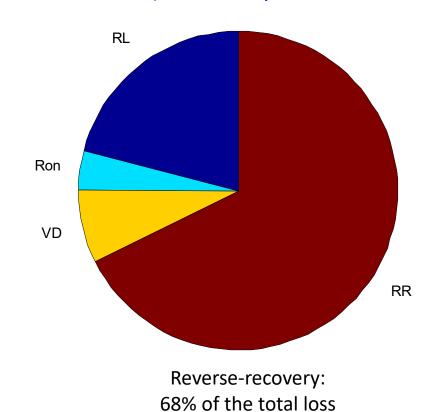
### Loss Breakdown: Soft-Switched Si Boost

$$f_s$$
 = 100 kHz  
 $P_{loss}$  = 5.7 W,  $\eta$  = 98.1%

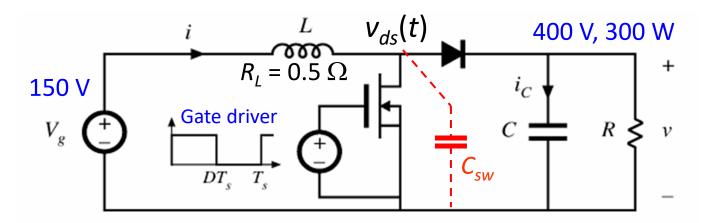


Reverse-recovery: 21% of the total loss

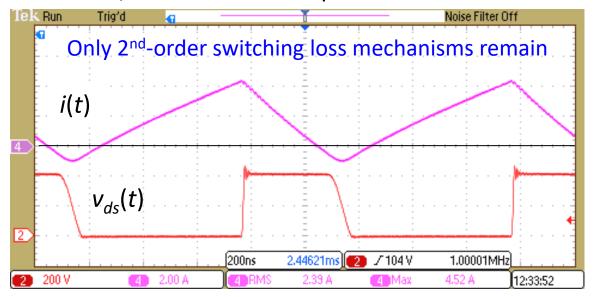
$$f_s$$
 = 1 MHz  
 $P_{loss}$  = 17.7 W,  $\eta$  = 94.4 %  
Experiment:  $\eta$  = 95.1 %



### Soft-switched SiC diode



#### SiC diode, "soft-switched" operation



 $f_s = 1 \text{ MHz}$ 

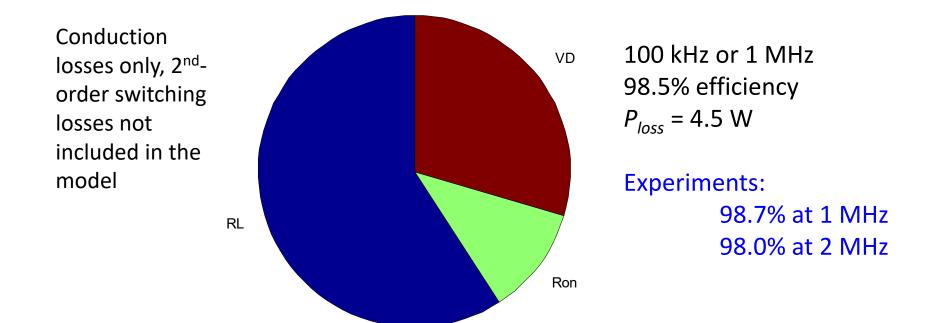
#### **MOSFET**

- $di_F/dt = 200 \text{ A/}\mu\text{s}$
- $C_{ds,eq} = 45 \text{ pF}$
- $R_{on} = 0.15 \Omega$

#### SiC diode

- $t_{rr} = 0$ ,  $Q_{rr} = 0$
- $2C_{d,Qeq}$ - $C_{d,eq}$  = 64 pF
- $V_D = 1.8 \text{ V}$

### Soft-switched Boost with SiC diode

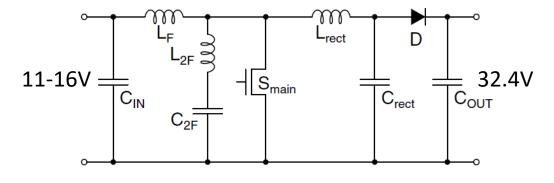


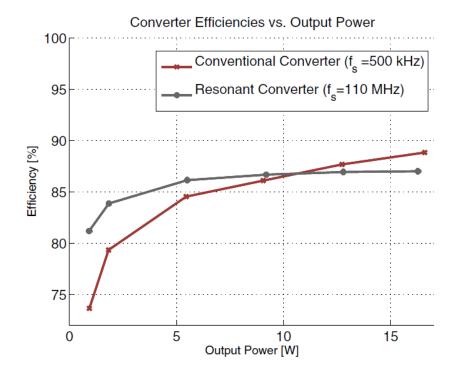
### Power supply technology limits become dominated by:

- Magnetics
- 2<sup>nd</sup>-order switching loss mechanisms, e.g. gate-drive losses, parasitic inductances (layout and packaging)
- Gate-drive circuitry and controllers to support high-frequency operation

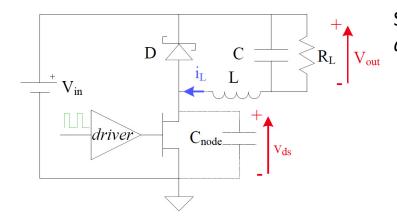
# VHF power electronics [11]

| Resonant Design     |            |                         |  |  |  |
|---------------------|------------|-------------------------|--|--|--|
| Component           | Value      | Туре                    |  |  |  |
| $L_F$               | 33 nH      | Coilcraft 1812SMS       |  |  |  |
| $L_{2F}$            | 12.5 nH    | Coilcraft A04TG         |  |  |  |
| $L_{rect}$          | 22 nH      | 1812SMS                 |  |  |  |
| $C_{2F}$            | 39 pF      | ATC100A                 |  |  |  |
| $C_{rect}$          | 10 pF      | ATC100A                 |  |  |  |
| $C_{out}$           | $75~\mu F$ | Multilayer Ceramics     |  |  |  |
| $C_{in}$            | $22 \mu F$ | Multilayer Ceramics     |  |  |  |
| $S_{main}$          |            | Freescale MRF6S9060     |  |  |  |
| D                   |            | Fairchild S310          |  |  |  |
| Conventional Design |            |                         |  |  |  |
| Component           | Value      |                         |  |  |  |
| $L_{boost}$         | 10 μH      | Coilcraft D03316T-103ML |  |  |  |
| $C_{out}$           | $75~\mu F$ | Multilayer Ceramics     |  |  |  |
| $C_{in}$            | $22 \mu F$ | Multilayer Ceramics     |  |  |  |
| $S_{main}$          | •          | LT1371HV                |  |  |  |
| D                   |            | Fairchild S310          |  |  |  |





### **WBG Devices**

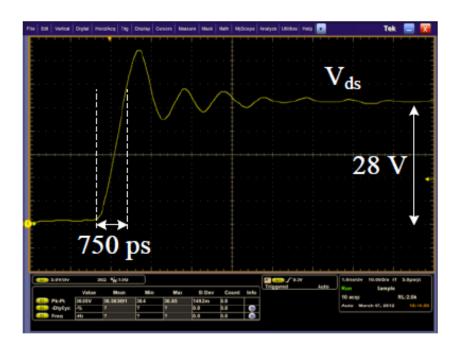


TriQuint TGF2023-02 12W, DC-to-18 GHz RF/microwave HEMT

FOM for switching applications

$$C_{ds}R_{on} \approx 1 \ \Omega pF$$
  
 $Q_{q}R_{on} \approx 10 \ \Omega pC$ 

Standard hard-switched PWM operation at 50 MHz  $dv_{ds}/dt$  dominated by probe (4 pF) capacitance



Emerging GaN HEMT devices may enable completely new RF-based design approaches in power electronics

# **Topics Covered**

#### Course Topics

- High Frequency Power Conversion
  - Switching losses and device selection
  - Resonance in power electronics
  - Soft switching (ZVS and ZCS)
  - Magnetics design
- Non-resonant soft switching converters
  - Constant frequency control
  - State-plane analysis
  - Resonant switches
  - Modeling and Simulation
  - Discrete time models
- Resonant Converters
  - Resonant converter topologies
  - Sinusoidal analysis
  - AC-modeling and frequency modulation
  - State-plane analysis
- Applications and practical issues of high frequency converters