Consider a pair of wires **ideal** wires)

Length $<< \lambda$

Voltage along a cable can vary!

Length $>> \lambda$, say, infinitely long

Voltage $v(z) \sim E(z)D$

We can actually get to this wave behavior by using circuit theory, w/o going into details of the EM fields!
There is capacitance between any two pieces of conductors. A pair of plates, wires, etc., or the core and shields of a coax cable.

\[ C = C' \Delta z \]

\[ \Delta z \]: capacitance per length

A piece of wire is actually an inductor.

\[ B \propto i \]

\[ \text{When } i \text{ changes with } t, \text{ so does } B \]

\[ \frac{di}{dt} \]

\[ B \times i \]

\[ \vec{E} \times \frac{\partial B}{\partial t} \Rightarrow \vec{v} \times \frac{di}{dt} \]

\[ \vec{v} = L \frac{di}{dt} \]

Similarly, a pair of coupled wires.

\[ L' \]

\[ L' \text{ is inductance per length} \]

Voltage \( \vec{v} \) around the loop!
To make things simple, we first consider a pair of *ideal* wires. No resistance, no shunt (leakage).

Pay close attention. We take a different approach than does the book. Now, zoom in on one segment:

\[ i(z, t) \quad L' \Delta z \quad \Delta u \quad C' \Delta z \quad v(z, t) \]

\[ \Delta z \]

\[ v(z+\Delta z, t) \]
\[ \Delta v = u(z+\Delta z, x) - u(z, x) = -L' \Delta z \frac{\partial i}{\partial z} \]

\[ \frac{\partial v}{\partial z} = \lim_{\Delta z \to 0} \frac{\Delta v}{\Delta z} = -L' \frac{\partial i}{\partial z} \]

\[ \frac{\partial^2 v}{\partial z^2} = -L' \frac{\partial^2 i}{\partial z \partial x} \]

\[ \frac{\partial^2 v}{\partial x^2} = -L' \frac{\partial^2 i}{\partial x^2} \]

Inductor

Capacitor

Take derivatives with regard to \( z, t \)
Partial differential equations

Do these 2 equations look familiar to you?
What are they?

Let \( v_p = \frac{1}{\sqrt{L'C'}} \), we have

\[
\frac{\partial^2 v}{\partial z^2} = \frac{1}{v_p^2} \frac{\partial^2 v}{\partial x^2}
\]

\( v = f(v_p t - z) \) is the general solution to this equation.

Do it on your own: verify this.
Coaxial cable

- Carries f’s up to 1GHz

Power transmission line

- 11 kV, 18 kV, 23 kV, 23.5 kV output (CLP power)
- 12.5 kV to 22 kV output (HEC)

https://en.wikipedia.org/wiki/Coaxial_cable
Let’s say we have a magic way to measure and record the instantaneous voltage between the inner and outer conductors of the coax cable, as a function of time, at any location along the cable. The cable carries a high frequency (tens to hundreds MHz) signal.

You do such measurements at two locations 0.3 m apart. Will the two waveforms be different (in general)? If so, describe the difference. Explain the reason behind your answers.

We can also measure and record the instantaneous voltage between the two wires of a power transmission line at arbitrary locations.

You do such measurements at two locations 0.3 m apart. Will the two waveforms be different? If so, describe the difference. Explain the reason behind your answers.

We stopped here on Thu 8/26/2021.
Let \( v_p = \frac{1}{\sqrt{LC'}} \), we have \( \frac{\partial^2 v}{\partial z^2} = \frac{1}{v_p^2} \frac{\partial^2 v}{\partial x^2} \).

\( v = f(v_p t - z) \) is the general solution to this equation.

This is the wave equation!
More strictly, the lossless, dispersionless, linear wave equation. Assume: no resistance, no leakage; \( v_p \) independent of frequency; \( v_p \) independent of voltage \( v \)

\[ \frac{\partial^2 i}{\partial z^2} = L'C' \frac{\partial^2 i}{\partial x^2} \]

The equation for \( i \) is in the same form – formally the same.
Therefore, formally same solution.
Is this amazing?
We arrived at the wave equation from circuit theory, regardless of frequency. Why does this approach work?

One more agreement, for co-ax cables:

\[ l' = \frac{\mu}{\pi} \ln \left[ \frac{D}{d} + \sqrt{(\frac{D}{d})^2 - 1} \right] \]

\[ c' = \frac{\pi \varepsilon}{\ln \left[ \frac{D}{d} + \sqrt{(\frac{D}{d})^2 - 1} \right]} \]

\[ \therefore \quad \frac{1}{V_p} = \frac{1}{\sqrt{l'c'}} = \frac{1}{\sqrt{\mu \varepsilon}} \]

Consistent with EM theory! Check this offline for other transmission lines.

See Table 2-1, pp. 45 in 7/E, pp. 53 in 6/E

(There will be homework problems for you to learn about other types of transmission lines, as well as non-ideal co-ax cables)
\[
\frac{\partial^2 v}{\partial z^2} = \frac{1}{v_p^2} \frac{\partial^2 v}{\partial x^2}
\]

(\text{the equation for } i \text{ is in the same form – formally the same.})

\( v = f(v_p t - z) \) is the general solution to this equation.

What are the single frequency, simple harmonic solutions?

Single frequency, simple harmonic solutions:

\[
v(z, t) = |V_0^+| \cos(\omega t - \beta z + \phi_0^+)
\]

\[
i(z, t) = |I_0^+| \cos(\omega t - \beta z + \phi_0^+) \quad \text{(formally the same equation, thus formally the same solution.)}
\]

Here, \( V_0^+ \) and \( I_0^+ \) are “complex amplitudes” that we will talk about later. For the waves, they are not the phasors of the waves. We will talk about the distinction.

\(|V_0^+| \) and \(|I_0^+| \) are the \textbf{real amplitudes}, or simply amplitudes.

We have not shown \textbf{the voltage and current waves are in phase}. But they are. You can take this as a conclusion for now. Or, if you are interested, \textbf{read the proof next page}. 
Here we show that the voltage and current waves are in phase with each other:

\[ v(z,t) = |V_0^+| \cos(\omega t - \beta z + \phi_{v0}^+) \]
\[ i(z,t) = |I_0^+| \cos(\omega t - \beta z + \phi_{i0}^+) \]

\[ \frac{\partial v}{\partial z} = \beta |V_0^+| \sin(\omega t - \beta z + \phi_{v0}^+) \]
\[ \frac{\partial i}{\partial t} = -\omega |I_0^+| \sin(\omega t - \beta z + \phi_{i0}^+) \]

Recall that

For this to hold for any arbitrary \( z \), we must have \( \phi_{v0}^+ = \phi_{i0}^+ \equiv \phi_0^+ \)

So, in phase!

We also get a by-product:

\[ \frac{|V_0^+|}{|I_0^+|} = \frac{\omega L'}{\beta} = v_p L' \]

Unit: \( \frac{m \ H}{s \ m} = H/s = \Omega \)

These conclusions are important!

Anywhere, any time \( v(z,t)/i(z,t) = \text{constant} \)
Define \( \frac{|V_{0}^+|}{|I_{0}^+|} = \frac{\omega L'}{\beta} = \nu_p L' \equiv Z_0 \) \hspace{1cm} (\text{\(Z_0\) is real, i.e., purely resistive})

Consider:

\[ i(z,t) \]

\[ Z_0 \hspace{1cm} v(z,t) \] (Infinitely long)

\[ \]

There is no way to tell the difference just by measuring \( v \) and \( i \).

Energy propagating away vs. energy dissipated

Analogy: laser beam going to infinity or hitting a totally black wall

You may also use

\[ \frac{\partial i}{\partial z} = \lim_{\Delta z \rightarrow 0} \frac{\Delta i}{\Delta z} = -C' \frac{\partial v}{\partial t} \]

Doing the derivatives in a similar way as in last page, you will also see the voltage and current waves are in phase.

You will have a similar “by-product” about the \( \nu/i \) ratio.

It may look different, but you should be able to show they are equal.

Do it on your own. Hint: use

\[ \nu_p = \frac{1}{\sqrt{L' C'}} \]

Use scratch paper!
Now you may work on HW2: P1, P2

Some Clarifications

• Class notes and other information on course website
  • All class notes, homework, homework answers, some quiz answers (after the quiz, of course).
  • Read the notes, in conjunction with the textbook sections indicated in the schedule (also on website), before you do homework
  • The notes contain math derivations that I do not go over in detail and tell you to go over offline.
  • The notes also contain contents that I call “the extra mile,” for you to ponder upon.

• Homework
  • Do it on your own before checking the answer sheets.
  • Homework problems are for your exercise. Effort level needed to achieve same learning outcome differs by individual. Therefore homework is not graded.

• Quizzes
  • You will do well on quizzes if you do the above. Example: Quiz 1.
  • Graded (generously). Not a “gotcha” thing. Done with purposes.
  • Will give answers right after in-class quizzes. Primary purpose is to make sure you are prepared for the content to be covered in class.

• Project
  • On going.
  • Take notes, save results. You will better understand the results later; you can go back to any step and do/observe more when your understanding deepens.
  • Contact UGTA for CAD tool help.
The solution copied:

\[ v^+(z, t) = |V_0^+| \cos(\omega t - \beta z + \phi_0^+) \]

\[ i^+(z, t) = |I_0^+| \cos(\omega t - \beta z + \phi_0^+) \]

In what direction do these waves propagate?
Waves propagating the other way are also solutions to the same equations:

\[ v^{-}(z,t) = |V_{0}^{-}| \cos(\omega t + \beta z + \phi_{0}^{-}) \]

\[ i^{-}(z,t) = |I_{0}^{-}| \cos(\omega t + \beta z + \phi_{0}^{-}) \]

The superscript + or − signifies propagation direction: \( +z \) or \( -z \).

Of course, any linear combinations of waves in opposite directions are also solutions:

\[ v(z,t) = |V_{0}^{+}| \cos(\omega t - \beta z + \phi_{0}^{+}) + |V_{0}^{-}| \cos(\omega t + \beta z + \phi_{0}^{-}) \]

\[ i(z,t) = |I_{0}^{+}| \cos(\omega t - \beta z + \phi_{0}^{+}) + |I_{0}^{-}| \cos(\omega t + \beta z + \phi_{0}^{-}) \]

They may represent combinations of incident and reflected waves.

Recall that we have a mathematical tool to
1. Avoid the pain of dealing trigonometric functions, and
2. Turn partial differential equations to ordinary differential equations by putting aside the known time variation
Express waves with phasors

\[ v(z,t) = |V_0^+| \cos(\omega t - \beta z + \phi_0^+) + |V_0^-| \cos(\omega t + \beta z + \phi_0^-) \]

\[ \tilde{V} = \tilde{V}^+ + \tilde{V}^- = V_0^+ e^{-j\beta z} + V_0^- e^{j\beta z} \]

Where do the phases go?

Recall the details how we convert a time-domain function to a phasor:

By adding an “imaginary partner”

\[ v(z,t) \rightarrow |V_0^+| e^{j(\omega t - \beta z + \phi_0^+)} + |V_0^-| e^{j(\omega t + \beta z + \phi_0^-)} = [(|V_0^+| e^{j\phi_0^+}) e^{-j\beta z} + (|V_0^-| e^{j\phi_0^-}) e^{j\beta z}] e^{j\omega t} \]

This is not the phasor yet.

Throw away the known time variation \( e^{j\omega t} \)

and define the complex amplitudes \( V_0^+ = |V_0^+| e^{j\phi_0^+} \) and \( V_0^- = |V_0^-| e^{j\phi_0^-} \)

We get the phasor:

\[ \tilde{V} = \tilde{V}^+ + \tilde{V}^- = V_0^+ e^{-j\beta z} + V_0^- e^{j\beta z} \]

Positive going

Negative going

Notice sign and direction
Express waves with phasors

The current wave is similar

\[ i(z, t) = I_0^+ \cos(\omega t - \beta z + \phi_0^+) + I_0^- \cos(\omega t + \beta z + \phi_0^-) \]

This tool makes our life much easier when we deal with a more complicated situation.

Here's the more complicated situation:

No wires are ideal.
Any wire has some resistance.

\[ R' \quad \Delta z \]

Resistance per length

There is always some shunt conductance between two wires

\[ G' \quad \Delta z \]

Shunt conductance per length

Notice that \( R' \) and \( G' \) describes two different things. \( R' \neq 1/G' \)
Analyze the circuit in the phasor way

$$\frac{d\tilde{V}}{dz} = \lim_{\Delta z \to 0} \frac{\Delta \tilde{V}}{\Delta z} = -(R' + j\omega L')\tilde{I}$$

$$\frac{d\tilde{I}}{dz} = \lim_{\Delta z \to 0} \frac{\Delta \tilde{I}}{\Delta z} = -(G' + j\omega C')\tilde{V}$$

Take derivatives on one equation and insert it into the other, you get

$$\frac{d^2 \tilde{V}}{dz^2} - (R' + j\omega L') (G' + j\omega C') \tilde{V}(z) = 0$$

and a formally same equation for the current.

This is an ordinary differential equation. Because we used phasors.

We have arrived at this equation just by circuit analysis using phasors.

You could also first do the circuit analysis in the time domain, arriving at partial differential equations, and then convert quantities to phasors and arrive at the same ordinary differential equations, as done in the book (Sections 2-3 & 2-4).

We stopped here on Thu 2/4/2021.
The partial differential equations for the general, more complicated situation are, well, too complicated. We don’t even bother to tackle them. Let’s look at the simpler ordinary differential equation:

\[ \frac{d^2 \tilde{V}}{dz^2} - (R' + j\omega L') (G' + j\omega C') \tilde{V}(z) = 0 \]

Before solving this equation, let’s first have a digression back to the ideal case

\[ R' = 0 \quad \text{and} \quad G' = 0 \]

\[ \frac{d^2 \tilde{V}}{dz^2} + \omega^2 L' C' \tilde{V} = 0 \quad \Rightarrow \quad \tilde{V}(z) = V_0 e^{\pm j\omega \sqrt{L'C'} z} \]

Recall that

\[ \frac{\omega}{\beta} = \nu_p = \frac{1}{\sqrt{L'C'}} \quad \Rightarrow \quad \beta = \omega \sqrt{L'C'} \]

we have \( \tilde{V} = V_0 e^{\pm j\beta z} \)

Notice that these are actually two solutions. What are the difference between the two solutions?
Waves propagating in two opposite directions: \( \vec{V} = \vec{V}^+ + \vec{V}^- = V_0^+ e^{-j\beta z} + V_0^- e^{j\beta z} \)

No surprise. The solutions we got earlier for the ideal case.

Now, back to the more complicated, general case

\[\frac{d^2 \vec{V}}{dz^2} - (R' + j\omega L')(G' + j\omega C') \vec{V}(z) = 0\]

Let \( \gamma^2 = (R' + j\omega L')(G' + j\omega C') \)

we can write \( \frac{d^2 \vec{V}}{dz^2} - \gamma^2 \vec{V}(z) = 0 \)

Compare this to the ideal case \( \frac{d^2 \vec{V}}{dz^2} + \omega^2 L'C' \vec{V} = 0 \)

These two equations are “formally” the same, except \(-\gamma^2\) is complex.

\( \beta^2 \rightarrow -\gamma^2 \) thus \(-j\beta \rightarrow -\gamma\) and \( j\beta \rightarrow \gamma \)

So, the solutions are \( \vec{V} = V_0^e^{-j\gamma z} + V_0^- e^{j\gamma z} \)

What kind of waves are they?
\[ \tilde{V} = V_0^+ e^{-\gamma z} + V_0^- e^{\gamma z} \]

What kind of waves are they?

Let \( \gamma = \alpha + j \beta \) (we are doing nothing. Any complex number can be written as this), we have the first solution

\[ \tilde{V}^+ = V_0^+ e^{-\gamma z} = V_0^+ e^{-(\alpha + j \beta)z} = V_0^+ e^{-\alpha z} e^{-j \beta z} \]

What kind of wave is this?

Similarly,

\[ \tilde{I}^+ = I_0^+ e^{-\gamma z} = I_0^+ e^{-(\alpha + j \beta)z} = I_0^+ e^{-\alpha z} e^{-j \beta z} \]

Why do the waves attenuate when there is resistance or shunt leakage? (Why is there no attenuation when the wire is made of a perfect conductor and the medium between them is a perfect insulator)?

Recall that, in circuit theory, reactive versus resistive..., ...

How to express the decaying wave propagating in the \(-z\) direction?
Again, there can be waves going the other way.

\[
\tilde{V} = V_0^+ e^{-\alpha z} e^{-j\beta z} + V_0^- e^{\alpha z} e^{j\beta z} \quad \text{sign}
\]

\[
\tilde{I} = I_0^+ e^{-\alpha z} e^{-j\beta z} + I_0^- e^{\alpha z} e^{j\beta z} \quad \text{sign}
\]

Again, we discuss the most important concept of the first half of the semester:

\[
\tilde{V} = V_0^+ e^{-\gamma z} + V_0^- e^{\gamma z}
\]

Take derivatives

\[
\frac{d\tilde{V}}{dz} = -\gamma V_0^+ e^{-\gamma z} + \gamma V_0^- e^{\gamma z}
\]

From circuit analysis

\[
\left(\frac{d\tilde{V}}{dz}\right) = \lim_{\Delta z \to 0} \frac{\Delta \tilde{V}}{\Delta z} = -(R' + j\omega L')\tilde{I} = -(R' + j\omega L')I_0^+ e^{-\alpha z} e^{-j\beta z} - (R' + j\omega L')I_0^- e^{\alpha z} e^{j\beta z}
\]

For the identity to hold for all \( z \), we must have the following:

For the \( e^{-\gamma z} \) term:

\[
\gamma V_0^+ = (R' + j\omega L')I_0^+
\]

\[
\Rightarrow \quad \frac{V_0^+}{I_0^+} = \frac{R' + j\omega L'}{\gamma} = \frac{R' + j\omega L'}{\sqrt{(R' + j\omega L')(G' + j\omega C')}} = \sqrt{\frac{R' + j\omega L'}{G' + j\omega C'}}
\]
For the $e^{\gamma z}$ term: $\gamma V_0^- = -(R' + j\omega L')I_0^-$

$$\Rightarrow \frac{V_0^-}{I_0^-} = -\frac{R' + j\omega L'}{\gamma} = -\frac{R' + j\omega L'}{\sqrt{(R' + j\omega L')(G' + j\omega C')}} = -\frac{\sqrt{R' + j\omega L'}}{\sqrt{G' + j\omega C'}}$$

Notice negative signs. Just because of sign convention (see circuit diagram)

Define $Z_0 \equiv \sqrt{\frac{R' + j\omega L'}{G' + j\omega C'}}$

the characteristic impedance

Complex and explicitly dependent on frequency in the general (lossy) case.
For the wave traveling towards \(+z\),
\[
\tilde{V}^+ = V_0^+ e^{-\gamma z} \\
\tilde{I}^+ = I_0^+ e^{-\gamma z}
\]
At any \(z\), \(\frac{\tilde{V}^+(z)}{\tilde{I}^+(z)} = \frac{V_0^+}{I_0^+} = Z_0\)

For the wave traveling towards \(-z\),
\[
\tilde{V}^- = V^- e^{\gamma z} \\
\tilde{I}^- = I_0^- e^{\gamma z}
\]
At any \(z\), \(\frac{\tilde{V}^-(z)}{\tilde{I}^-(z)} = \frac{V_0^-}{I_0^-} = -Z_0\)

Again, notice this negative sign.

These relations are \textit{separately} held by the two waves in opposite directions.

In general, \(Z_0 \equiv \sqrt{\frac{R' + j\omega L'}{G' + j\omega C'}}\) is complex and \textit{explicitly} dependent on frequency.

Are \(V_0^+\) and \(I_0^+\) in phase in the general case?

For the \textit{lossless} transmission line, \(R' = 0\) and \(G' = 0\),
\[
Z_0 = \sqrt{\frac{L'}{C'}}
\]
Real. No \textit{explicit} frequency dependence.
Take-home messages

• Voltage $v$ and current $i$ follow the same differential equation
• Therefore solutions in same form
• Therefore there is a constant ratio between their amplitudes and there is a constant shift between their phases for harmonic waves going in one direction
• In the phasor form, the complex amplitude ratio is $\pm Z_0$
• Being a voltage/current ratio, $Z_0$ has the dimension of impedance
• In general (lossy case), $Z_0$ is complex and explicitly depends on $\omega$
• In the lossless case, $Z_0$ is real w/o explicit frequency dependence
• $Z_0$ being real means the voltage and the current are in phase. It also means the equivalent circuit for a (semi-)infinitely long transmission line is simply a resistor with a resistance value $Z_0$ – see next page.

At this point, review textbook up to Section 2-4. Finish P1 through P6 of HW2.
Ribbon twin lead: (used to be) used to connect a television receiving antenna to a home television set.

The inductors (and resistors in lossy lines) are on only one side. Which side is which wire???
The cables

Coaxial cable

Ribbon twin lead: (used to be) used to connect a television receiving antenna to a home television set.

\[ Z_0 = 75 \, \Omega \]

https://www.moonraker.eu/antennas/antenna-hardware/ribbon-feeder/75-m-75-ohm-twin-feeder

\[ Z_0 = 300 \, \Omega \]


Question:

How to vary the \( Z_0 \) of the transmission line of a given construction?

Hint: Consider the simple lossless case

\[ Z_0 = \sqrt{\frac{L'}{C'}} \]

and use Table 2-1 in Textbook.
Project

Circuit simulations to transition you from lumped element-based circuit theory

Part 1

Generator: 1 V step, rise time = 0.1 ns. Internal impedance 50 Ω.

Plot the two voltages $V_1$ and $V_2$ for the above two cases.

Hint: You may make mistakes. Do a sanity check by a “back of an envelope” analysis. At the very least, find out the steady state. Does the simulation give you more or less what you expect?

Ongoing project. Stay tuned for next steps.
Project

Part 2

50 Ω
0.3 nH
0.12 pF

50 Ω

Part 1

Generator: 1 V step, rise time = 0.1 ns. Internal impedance 50 Ω.
Plot the two voltages $V_1$ and $V_2$ for the above two cases.
What have you got?

Now, do the same simulations for rise time = 1 ps.
Notice that you might need to set MaxTimeStep & StopTime. Try different values for these and see what difference you make by changing them.
Also, adjust the scales of the plots to show details.
Do not forget to do a sanity check.
Compare the results to those of Part 1. Similarities and differences?
Do the results make sense to you?

Ongoing project. Stay tuned for next steps.

We stopped here on Tue 2/9/2021.
There is no way to tell the difference just by measuring $v$ and $i$.
Energy propagating away vs. energy dissipated
Analogy: laser beam going to infinity or hitting a totally black wall

**Impedance match**

By the way, transmission line (thick line) versus “wire wires” (thin lines)

The same as the infinitely long line!

We want impedance match! (Reasons?)
Now, let’s look at a transmission line with a source and a load.

If $Z_L = Z_0$, impedance matched. All energy delivered to load. Good!

(we can view this from the vantage point of equivalent circuits)

What if $Z_L \neq Z_0$?

The load says $\frac{\mathcal{V}(0)}{\mathcal{I}(0)} = \frac{\mathcal{V}_L}{\mathcal{I}_L} = Z_L$

If there were only the incident wave, $\frac{\mathcal{V}^+(0)}{\mathcal{I}^+(0)} = \frac{V_0^+}{I_0^+} = Z_0$

Something has to happen to resolve this “conflict.” That something is reflection.

Sign due to convention

By definition, $Z_L = \frac{\mathcal{V}_L}{\mathcal{I}_L} = \left(\frac{V_0^+ + V_0^-}{V_0^+ - V_0^-}\right) Z_0$

Solve it and we have $V_0^- = \frac{Z_L - Z_0}{Z_L + Z_0} V_0^+$

Now, we just focused on the load. Will talk about the line and generator later.
If \( Z_L \neq Z_0 \), there has to be a reflected wave.

\[
V_0^- = \frac{Z_L - Z_0}{Z_L + Z_0} V_0^+
\]

The load does not get all energy carried by the incident wave.

**Where does the rest of the energy go?**

Consider analogy: laser beam hitting wall not totally black/dark.

Define the voltage reflection coefficient

\[
\Gamma \equiv \frac{V_0^-}{V_0^+} = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{Z_L - 1}{Z_L + Z_0}
\]

\[
\frac{Z_L}{Z_0} = \frac{1 + \Gamma}{1 - \Gamma}
\]

- One-to-one mapping between \( \Gamma \) and \( Z_L/Z_0 \)
- The ratio \( Z_L/Z_0 \) more important than \( Z_L \) itself
Therefore we define the normalized load impedance $z_L = \frac{Z_L}{Z_0}$

Thus,

\[
\Gamma \equiv \frac{V_0^-}{V_0^+} = \frac{z_L - 1}{z_L + 1} \equiv \frac{1 + \Gamma}{1 - \Gamma}
\]

Notice the one-to-one mapping. This is very important!

For the current

\[
\frac{I_0^-}{I_0^+} = -\frac{V_0^-}{V_0^+} = -\Gamma
\]

Where does the negative sign come from?

\[
Z_0 = \sqrt{\frac{L'}{C'}} \text{ is real for a lossless line, but} \\
Z_0 \equiv \sqrt{\frac{R' + j\omega L'}{G' + j\omega C'}} \text{ is complex in general.}
\]

$Z_L$ is complex in general. Thus, $\Gamma$ is complex in general.

Read the textbook: Section 2-6 overview, 2-6.1
Quiz 2

Find the time-domain sinusoidal functions corresponding to the following phasors. (\(z\) is position. \(Y_0^+\) and \(Y_0^-\) are real and positive.) Make sure you follow conventions adopted in this course.

\[
\tilde{Y}_1(z) = Y_0^+ e^{-j\beta z}
\]

\[
\tilde{Y}_2(z) = Y_0^- e^{i\beta z}
\]

\[
\tilde{Y}(z) = -2jY_0^+ \sin(\beta z)
\]

Find the phasor for the following function of position \(z\) and time \(t\). (\(z\) is position. \(V_0^+\) is real and positive)

\[
v(z, t) = 2V_0^+ \cos(\beta z) \cos(\omega t)
\]