

# Frequency Sampling Structures

# Specifying Frequency Response

Set the frequency response of an FIR filter at  $M$  equally-spaced points  $\Omega_k = 2\pi k / M$ ,  $k = 0, 1, 2, \dots, M - 1$  and find the impulse response  $h[n]$ .

Frequency response and impulse response are related by

$$H(e^{j\Omega}) = \sum_{n=0}^{M-1} h[n] e^{-j\Omega n}$$

and it follows that

$$H(e^{j\Omega_k}) = H(e^{j2\pi k/M}) = \sum_{n=0}^{M-1} h[n] e^{-j2\pi kn/M}, \quad k = 0, 1, 2, \dots, M - 1$$

This is the DFT of  $h[n]$ .

# Specifying Frequency Response

Since  $H(e^{j2\pi k/M})$  is the DFT of  $h[n]$ ,  $h[n]$  must be the inverse DFT of  $H(e^{j2\pi k/M})$ .

$$h[n] = \frac{1}{M} \sum_{k=0}^{M-1} H(e^{j2\pi k/M}) e^{j2\pi kn/M}, \quad n = 0, 1, 2, \dots, M-1$$

The transfer function and impulse response are related by

$$H(z) = \sum_{n=0}^{M-1} h[n] z^{-n} = \frac{1}{M} \sum_{n=0}^{M-1} \sum_{k=0}^{M-1} H(e^{j2\pi k/M}) e^{j2\pi kn/M} z^{-n}.$$

Exchanging the order of summation,

$$H(z) = \frac{1}{M} \sum_{k=0}^{M-1} H(e^{j2\pi k/M}) \sum_{n=0}^{M-1} e^{j2\pi kn/M} z^{-n}$$

# Specifying Frequency Response

Using the formula for summing a geometric series,

$$H(z) = \frac{1}{M} \sum_{k=0}^{M-1} H(e^{j2\pi k/M}) \frac{1 - z^{-M} e^{j2\pi k/M}}{1 - z^{-1} e^{j2\pi k/M}} = \frac{1 - z^{-M}}{M} \sum_{k=0}^{M-1} \frac{H(e^{j2\pi k/M})}{1 - z^{-1} e^{j2\pi k/M}}$$

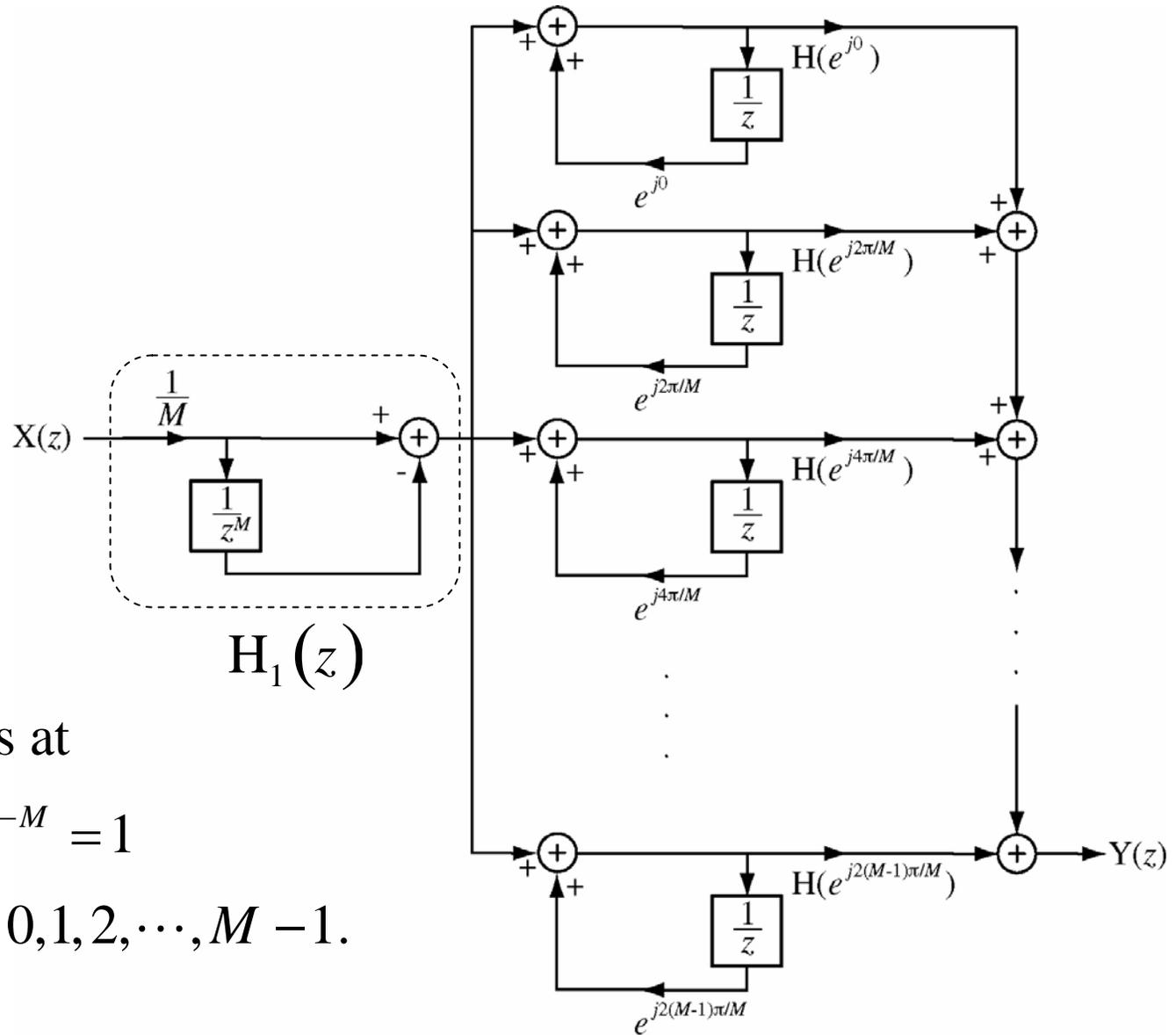
We can think of this as the cascade of two filters, one with transfer function

$$H_1(z) = \frac{1 - z^{-M}}{M}$$

and one with transfer function

$$H_2(z) = \sum_{k=0}^{M-1} \frac{H(e^{j2\pi k/M})}{1 - z^{-1} e^{j2\pi k/M}} .$$

# Specifying Frequency Response



$H_1(z)$  has zeros at

$$1 - z^{-M} = 0 \Rightarrow z^{-M} = 1$$

$$z = e^{j2\pi q/M}, \quad q = 0, 1, 2, \dots, M-1.$$

# Specifying Frequency Response

$H_2(z)$  is the sum of the transfer functions of  $M$  subsystems, each of which has a pole where

$$1 - z^{-1} e^{j2\pi k/M} = 0 \Rightarrow z^{-1} e^{j2\pi k/M} = 1 \Rightarrow z = e^{j2\pi k/M}, \quad k = 0, 1, 2, \dots, M-1$$

So the transfer function can be written as

$$H(z) = \underbrace{\frac{1}{M} \left[ \prod_{q=0}^{M-1} 1 - z^{-1} e^{j2\pi q/M} \right]}_{H_1(z)} \underbrace{\sum_{k=0}^{M-1} \frac{H(e^{j2\pi k/M})}{1 - z^{-1} e^{j2\pi k/M}}}_{H_2(z)}$$

or

$$H(e^{j2\pi p/M}) = \frac{1}{M} \sum_{k=0}^{M-1} \frac{\prod_{q=0}^{M-1} 1 - e^{-j2\pi(p-q)/M}}{1 - e^{-j2\pi(p-k)/M}} H(e^{j2\pi k/M}), \quad 0 \leq p < M$$

# Specifying Frequency Response

The poles of  $H_2(z)$  are at the same locations as the zeros of  $H_1(z)$ . So for any particular zero of  $H_1(z)$ , all the terms in the summation are zero except the one for which the pole and zero cancel. Therefore

$$H(e^{j2\pi p/M}) = \frac{H(e^{j2\pi p/M})}{M} \prod_{\substack{q=0 \\ q \neq p}}^{M-1} 1 - e^{-j2\pi(p-q)/M}, \quad 0 \leq p < M$$

This result implies that

$$\prod_{\substack{q=0 \\ q \neq p}}^{M-1} 1 - e^{-j2\pi(p-q)/M} = M, \quad 0 \leq p < M$$

# Specifying Frequency Response

The poles and zeros could theoretically be anywhere on the unit circle, but for practical designs they must occur in complex conjugate pairs and

$$H\left(e^{j2\pi k/M}\right) = H^*\left(e^{-j2\pi k/M}\right) = H^*\left(e^{j2\pi(M-k)/M}\right)$$

# Specifying Frequency Response

Taking advantage of the complex-conjugate symmetry, for  $M$  even,

$$H_2(z) = \sum_{k=0}^{M-1} \frac{H(e^{j2\pi k/M})}{1 - z^{-1} e^{j2\pi k/M}} = \frac{H(e^{j0})}{1 - z^{-1}} + \sum_{k=1}^{M/2-1} \frac{H(e^{j2\pi k/M})}{1 - z^{-1} e^{j2\pi k/M}} + \frac{H(e^{j2\pi(M-k)/M})}{1 - z^{-1} e^{j2\pi(M-k)/M}}$$

$$H_2(z) = \frac{H(e^{j0})}{1 - z^{-1}} + \sum_{k=1}^{M/2-1} \frac{A(k) - B(k)z^{-1}}{1 - 2\cos(2\pi k/M)z^{-1} + z^{-2}}$$

$$\text{where } A(k) = H(e^{j2\pi k/M}) + H(e^{j2\pi(M-k)/M})$$

$$\text{and } B(k) = e^{-j2\pi k/M} H(e^{j2\pi k/M}) + e^{j2\pi k/M} H(e^{j2\pi(M-k)/M})$$

Similarly, for  $M$  odd,

$$H_2(z) = \frac{H(e^{j0})}{1 - z^{-1}} + \frac{H(e^{j\pi})}{1 + z^{-1}} + \sum_{k=1}^{(M-1)/2} \frac{A(k) - B(k)z^{-1}}{1 - 2\cos(2\pi k/M)z^{-1} + z^{-2}}$$

# Example

Design a filter whose frequency response goes through these points.

$k$	0	1	2	3	4	5	6	7
$H(e^{j2\pi k/M})$	0	1	$j$	0	0	0	$-j$	1

$$H(z) = \frac{1-z^{-M}}{M} \sum_{k=0}^{M-1} \frac{H(e^{j2\pi k/M})}{1-z^{-1}e^{j2\pi k/M}}$$

$$H(z) = \frac{1-z^{-8}}{8} \left[ \frac{1}{1-z^{-1}e^{j2\pi/8}} + \frac{j}{1-z^{-1}e^{j4\pi/8}} + \frac{-j}{1-z^{-1}e^{j12\pi/8}} + \frac{1}{1-z^{-1}e^{j14\pi/8}} \right]$$

# Example

Taking advantage of the periodicity of  $e^{j2\pi k/8}$

$$H(z) = \frac{1-z^{-8}}{8} \left[ \frac{1}{1-z^{-1}e^{j2\pi/8}} + \frac{1}{1-z^{-1}e^{-j2\pi/8}} + \frac{j}{1-z^{-1}e^{j4\pi/8}} + \frac{-j}{1-z^{-1}e^{-j4\pi/8}} \right]$$

or

$$H(z) = \frac{1-z^{-8}}{8} \left[ \frac{2-2z^{-1}\cos(\pi/4)}{1-2z^{-1}\cos(\pi/4)+z^{-2}} - \frac{2z^{-1}\sin(\pi/2)}{1-2z^{-1}\cos(\pi/2)+z^{-2}} \right]$$

and the frequency response is

$$H(e^{j\Omega}) = \frac{1-e^{-j8\Omega}}{8} \left[ \frac{2-2e^{-j\Omega}\cos(\pi/4)}{1-2e^{-j\Omega}\cos(\pi/4)+e^{-j2\Omega}} - \frac{2e^{-j\Omega}\sin(\pi/2)}{1-2e^{-j\Omega}\cos(\pi/2)+e^{-j2\Omega}} \right]$$

The impulse response is

$$h[n] = \left\{ \begin{array}{l} 0.25, -0.0732, 0, 0.0732, \\ \uparrow \\ -0.25, -0.4268, 0, 0.4268 \end{array} \right\} \xleftrightarrow{\mathcal{DFT}} H(e^{j2\pi k/M}) = \{0, 1, j, 0, 0, 0, -j, 1\}$$